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LEANDER RECORD OF MINISTER ADMITS

MAGNETISCHE UND METEOROLOGISCHE

# BEOBACHTUNGEN

AN DER

K. K. STERNWARTE ZU PRAG IM JAHRE 1905.

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66. Jahrgang

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# MAGNETISCHE UND METEOROLOGISCHE BEOBACHTUNGEN

AN DER

## K. K. STERNWARTE ZU PRAG IM JAHRE 1905.

Auf öffentliche Kosten herausgegeben

Professor Dr. L. WEINEK,

Direktor der k. k. Sternwarte in Prag-

66. Jahrgang.



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### Vorwort.

Der vorliegende Band enthält die im Jahre 1905 an der k. k. Sternwarte zu Prag angestellten magnetischen und meteorologischen Beobachtungen mit ihren Reduktionen und bildet den 66. Jahrgang in der Reihenfolge dieser Publikationen.

Wie bereits im Vorworte zum 64 und 65. Jahrgange in Aussicht gestellt und begründet wurde, sind mit Beginn des Jahres 1905 die Beobachtungen der magnetischen Horizontalintensität aufgelassen worden. Insofern fehlen auch die betreflenden Rubriken in dieser Veröffentlichung. Die magnetischen Deklinationsbeobachtungen werden jedoch in gleicher Weise wie frither weitergeführt. Im Monate Juli erfuhren dieselben eine längere Unterbrechung, welche durch mehrmaliges Reißen das Aufhängefadens und eine dadurch notwendig gewordene Anderung der Aufhängevorrichtung, sowie neuerliche Justierung des Instrumentes verursacht war.

Den, in den Zusammenstellungen für Luftdruck angeführten, Barometerständen wurden, wie im Vorjahre, die Ablesungen des Normalbarometers Greiner & Gesisler 501 zu Grunde gelegt, diese aber auf den Aufhängungsort des vordem benütten Fortinischen Barometers Tonnolet 831 d. i. auf die Sechöhz 1972. Meter bezogen, wodurch die Einheitlichkeit in der Reduktion des Luftdruckes in Bezug auf die früheren Jahre gewahrt blieb. Sämtliche meteorologischen Instrumente funktionierten, kleine leicht behobene Störungen ausgenommen, während des ganzen Jahres zufriedenstellend.

Die Reduktion der magnetisch-meteorologischen Beobachtungen war in folgender Weise verteilt. Herr Adjunkt Dr. Artur Scheller besorgte die absoluten magnetischen Deklinationsbeobachtungen am Laurenzerberge, an denen sich gelegentlich auch der erste Assistent, Herr Josef Dörr, beteiligte, und deren Reduktion, sowie diejenige der täglichen Variationsbeobachtungen. Herr Dörr bearbeitete die Thermographen-Aufzeichnungen für das ganze Jahr und machte die Zusammenstellung der direkten Messungen des Dunstdruckes, der relativen Feuchtigkeit, der Windrichtung, der Bewölkung und des Wolkenzuges. Der zweite Assistent, Herr Anton Kaiser, besorgte die Bearbeitung der Barographen-Aufzeichnungen für das ganze Jahr, ebenso die Reduktion der Windautogramme und der Hydrometeore.

An dem täglichen magnetischen und meteorologischen Dienste beteiligte sich außer dem Adjunkten und den beiden Assistenten auch der Sternwartendiener, Herr Josef Hlavaty.

PRAG, im April 1966.

L. Weinek.

## GEOGRAPHISCHE LAGE DER PRAGER STERNWARTE.

Länge,	Òs	tli	ch	,	or	1	Gr	ec	nv	vio	:h						0	٠	57	41		_	14	25
		7			,		Pa	ris	8						٠	٠	0		48	30	, «	-	13	5
•		,			,		Be	rli	n			٠	٠	٠	٠		c		4	6		-	ŧ	3
Breite																							. 50	5
Sechal	e														٠					19	7-	2	Me	ter.

#### RESULTATE AUS DEN MAGNETISCHEN BEOBACHTUNGEN.

INSTRUMENTE UND BEORACHTUNGSSTUNDEN. Die absoluten magnetischen Beobachtungen wurden im eisenfreien Observatorium am Abhange des Laurenzerberges angestellt. Zur Bestimmung der Deklination kam der magnetische Theodolit Edelmann in Verwendung. - Die Variations-Beobachtungen geschahen um 196, 26 und 96, wobei zur Ableitung der Tagesmittel die Formel:

 $\frac{1}{3} \left(19^3 + 2^5 + 9^4\right)$  benützt wurde. Wie in allen vorhergehenden Jahren erfolgte die Lesung der Deklination um 18 Min. nach den bezeichneten Stunden. BEOBACHTUNGEN DER DEKLINATION MIT DEM EDELMANNSCHEN THEODOLITEN (III). - BERECHNUNG

DER DEKLINATION AUS DEN ANGABEN DES VARIATIONSINSTRUMENTES. Die Torsion des Fadens des Edelmannschen Theodoliten wurde auf bekannte Weise mit Hilfe eines Torsionsstabes ermittelt und in Rechnung gebracht. Der Kollimationssehler des Magnetspiegels wurde bei jeder einzelnen Bestimmung der Deklinstion durch Umkehren des Magnetes eliminiert. Auf Seite s bedeuten a und b die beiden Lagen des Magnetgehäuses. - Als Mire diente die Spitze des im labre 1880 neu hergestellten Helmes des Altstädter Wasserturmes, deren Azimut zu 86° 24'.77 angenommen worden ist. (Siehe: Astronomische Beobachtungen an der k. k. Sternwarte zu Prag im Jahre 1854. Seite 56). Bei nebligem Wetter wurde dagegen der Helm des Karmeliter-Kirchturmes als Mire B benützt. Die Azimutdifferenz gegen die ersterwähnte Mire A beträgt: Mire A - Mire B == 14° 6:64. (Siehe Vorwort zum 63. Jahreang).

Die folgende Zusammenstellung gibt die Werte für den Skalenteil o des Variationsinstrumentes:

1905			für den enteil o	1905	Skalenteil Mittel	0
Januar Januar	27 28	8 8	17.22 18.91	Januar 27 u. 28	8" 18.0	6
April April April	7 10	8 8 8	21.60 19.71 20.35	April 9	8 20.5	5
Juni Juni	3	8	21.71	Juni 2 u. 3	8 21.7	9
Juli August	31	8	14.29	Juli 31 u. Aug. 1	8 14.7	0
September September September September	12	8 8 8	19.97 18.05 18.25 16.73	September 13	8 18.2	5
November November November	21 27 29	8 8	13.68 14.23 13.65	November 26	8 13.8	5

Der Wert für den Skalenteil o in der letzten Kolumne dieser Tafel diente zur Berechnung der Deklination aus den Angaben des Variations-Instrumentes mittelst der Formel:

Deklination =  $D_4 + o'_1 soll3 n_1$ 

worin Do die Deklination des Skalenteiles o und n die Lesung in Skalenteilen bedeutet. Die Anderung von Do zwischen je zwei in der Tafel enthaltenen Angaben wurde der Zeit proportional angenommen. Die nach dieser Formel berechneten Deklinationen jedes Tages, serner die Tages- und Monatsmittel der Deklination sind auf Seite 2 u. f. zusammengestellt,

MONATSMITTEL DER DEKLINATION UND DIE DARAUS ABGELEITETE TÄGLICHE VARIATION IM JAHRE 1905.

1905	198	27	94	Mittel	Tägliche Variation
Januar	8 41.84	8 45.66	8 40, 10	8 42.63	5.27
Februar	42.74	48.44	42.77	44.66	5.70
März	42.20	50.00	43.60	45.30	7.89
April	41.37	49.94	44.06	45.12	8.57
Mai	36.37	46,96	40.89	41.41	10.59
Juni	39.38	49.58	43.95	44 28	10.20
Juli	37.91	48,49	43.14	12 98	10.58
August	39,12	50,06	44.19	44.37	10,04
September	41.12	49.29	44.04	44.82	8.17
Oktober	40.52	47,29	41.70	43.13	6.68
November	39.12	43.98	38.25	40.45	5.73
Dezember	39.11	41.73	38.91	39.92	2.82
Jahr	8 40.07	8 47.62	8 42.17	8 43.27	7.76

REDUZIERTE VARIATIONS-BEOBACHTUNGEN DER DEKLINATION IM JAHRE 1905.

2

		JANU	AR		Г	EBRUAR		
Тад	194	3,	gh gh	Tages- mittel	19 <sup>b</sup>	21	9'	Tage
,	8 30.2	8 41.1	8 39.2	8 39.8	8 42.5	8 17.9	8 43.4	8 44
2		41.0	38.7	39.4	42.0	45.8	43.0	44
3	38.3	42.0	38.5 31.8	39.6	39-3	47.9	34.1 42.7	40
5	39.0	41.3	22.3	34.4	42.6	44.9	40.1	42
6	39.3	42.1	38.3	39.9	42.1	47.1	41.9	43
7 8	39.5	46.9	43.7 43.8	43.4	41.7	49.9	43.4	45
8	43.7	46.4	43.6	44.6	41.7	48.2	40.0	43
1ó	43-7	46.0	41.8	43.8	42.6	50.5	44-4	45
11	44-1	48.5	42.4	45.0	43.9	49.7 50.5	44 · 4 43 · 4	46 45
12	44-7 43-4	46.8	43.7	44.8	43.7 43.1	49.6	43.4	45
14	43-4	47.1	34.8	41.8	41.8	47.5	43.5	44
15	42.7	45.1	43.0	43.6	42.9		44.0	45
16	41.8	46.1	42.6	43.5	42.5	45.9	43.0	44
17	41.7	45.4	39.8	42.3	42.9	48.0	43.8	44
19	42.2	45.6	37.6	41.5	43.0	46.6	44.0	44
21	43.0	47.0	41.6	43.9	43.7	49.4	44.2	45
22	43.0	49.8	40.6	44.5	44.1	48.8	36.8	43
23	42.4	45.3	41.9	43.2 43.2	44.5	49.8	44.2	45
25	43.0	46.1	42.4	43.8	44.0	48.9	44.4	45
26	42.9	45.7	43.0	43.9	43.8	48.4	44.5	45
27	41.2	46.5	41.7	43.1	43.9 43.0	50.5	43·7 45·3	46
29	42.9	47.7	40.5	43.7	43.0	***	13.5	,
30	42.4 41.0	46.5	43.7	44.2			i	
Mittel	8 41.84	8 45.66	8 40.39	8 42.63	8 42.74	8 48.44	8 42.77	8 44
		MA	RZ		A	PRIL		
,	8 44.7	8 48.9	8 41.9	8 45.2	8 36.2	8 50.5	8 44.8	8 43
2	43.9	48.6	41.6	44.7	45-S 41.8	52.5	45.8	47
3	41.4	47.9	40.2	43.2	41.8	49.4 51.1	43-7	45 45
5	42.6	51.9	41.6	45-4	39.4	50.7	43.6	44
6	42.7	49.6	43.6	45.3	41.1	49.4	41.9	44
7 8	42.5	52.7	39.9	45.0 46.2	41.8	52.4	44.5	46
9	43.0	51.8	45.2	46.7	40.9	49.5	43.1	44
10	43.0	50.7	45.1	46.3	42.0	51.9	45-2	46
11	42.9 42.3	49.8	44.7	45.8	42.6 41.4	51.4	45.4	46 46
13	41.3	49.8	43.9	45.0	44.2	51.1	44.7	46
14	42.2 42.3	49.0 50.7	44.5	45.2	41.5	52.0	45.3	46
16	40.6	49.9	42.1	44.2	41.5	\$0.6	45.0	45
17	41.7	48.4	42.9	44.3	42.6	48.3	45.4	45
18	40.9	48.8	44.8	44.8 44.6	41.4 42.2	49.7	44.8	45 45
20	41.1	49.6	43.9	44.9	42.0	51.9	44.5	46
21	41.6	49.5	44.5 44.8	45.2	41.9	53.2	46.0	47
22	41.4	50.1		45.4	41.7	50.0	45.6	45
23	41.6	50.4	43-7	45.2 45.6	42.0	49.4	45.7	45
25	42.3	51.6	45.1	46.3	42.3	46.2	43.8	44
26	41.7	50.1	44.5 42.1	45.4	43.3	49.9	41.6	44
27 28	42.8 42.1	51.3	42.1	45.4 45.2	39.5	43-7	41.3 41.8	42
29	43.1	52.3	46.0	47.8	39.6	44.3	40.1	41
30	42.0	50.9	44.8	45.9 45.8	35-5	48.9	39.7	41
Mittel	8 42.20	8 50.09	8 43,60	8 45.30	8 41.37	8 49.94	8 44.06	8 45

		Mai		1905		Juni		
Tag	194	24	94	Tages- mittel	194	2h	94	Tages- mittel
1 2	8° 36.1 36.6	8 48.1	8 40.9	8 41.7 41.4	8° 35.4 37.5	8° 47.0 47.1	8 41.2 41.2	8 41.2
3	36.0 36.3	40.8	39.9	40.9	49.9	46.9 49.8	41.4 40.6	46.1 42.1
5	35.9	46.3	39.9	40.7	35.9 39.5	47.0	42.9	43.1
6 7	35.6	48.1 45.4 46.1	39.8 40.1	41.2 39.7	38.8 39-3	50. 5 44. 8	43.6	44.3
8	35-4	45.5	39.9 40.6	40.5	39.4 38.4	51.3	45.4 45.0	45.4
10	36.5	46.6	41.0	41.4	41.7	49.4 50.7	44.7	45.3
12	36.3	46.9	41.6	41.6	39.2 38.9	47.6 47.3	43.7 44.8	43.5
14	36.6	43.5	41.3	40.5	39.5	48.7	45.0 45.2	44.4
16	38.5	46.5	41.9	42.3	40.4	48.7 51.8	44.5	44.5
17 18	37.4 36.3 39.1	45.7 47.8	42.2	41.8 41.7 42.8	38.1 40.0	50.8 49.8	43.6 44.5 44.8	44.5 45-1 44.3
20	39.1	49.5 47.8	39-7 41-3	42.5	37-7 41.7	49.6	43.4	44-9
21	36.2 36.5	47.6	40.6	41.5	38.7 39.1	53-5	44.7 45.6	45.6
23 24	36.9 37.8	47.3	40.8	41.7	44.8 38.8	51.8 49.5	44.3 44.1	44.1
25 26	37.7	46.8	42.3	42.3	37 · 7 37 · 5	50.7	43.9 44.6	44.4
27 28	35.6 34.5	53.1 47.2	40.0 40.3	42.9 40.7	38.1 39.7	49.4 52.2	44.0 43.7	43.8
29 30	35·5 35·2	47.9 48.9	40.9	41.4 41.3	37·7 37·4	50.7	43.7 44.4 45.1	44.3
31	35.3	47.2	41.2	41.2	37.4	30.3	*5	44.,
Mittel	8 36.37	8 46.96	8 40.89	8 41.41	8 39.38	8 49.58	8 43.95 <sup>4</sup> )	8 44.1
		juli	**)		Aud	GUST		
1 2	8 38.4 38.2	8 52.2	8 45.3	8 45.3 38.2	8 36.4 33.3	8 49-7 46-8	8 43.1 48.5	8 43.1
3	18,0	50.3 51.0	43-3 43-5	46.8 44.5	37.8 35.4	49.4 46.3	41.0	42.
5	40.8	51.7	43.9	45.5	35-9	48.6	41.8	42.1
7	36.7 38.8	51.5 49.7	43.7 43.4	44.0 44.0	35.8 40.2	49.5	42.9	42.7 43.3 44.6
8 9 10	37-1	51.1	44.6	44.3	40.9 36.6	49.9 48.9 48.1	43.1	42.8
11	_		_	_	39.0 41.9	51.1	44.0	43.7
13	=	=	=	=	39·5 37·9	51.8	45.1	45.5
14	=	_	=	=	41.4 39.7	52.2 52.3	44.2 44.1	45.9
16 17	· -	=	Ξ	=	39.0	50.4 52.3	43.5 44.0	41.3 45.3
18	=	=	=	=	39.2	52.2 51.3	44.3	45.1 45.4
20	-	=	_	_	36.5	49.4	45-4 44.8	43.6
21	37·5 35·8	47.1	41.4	42.0	39.1 39.1	50.3 49.0	44.8 45.8	44.7 44.6
23	41.1	49.2 48.6	42.2 41.0	42.4 43.6	40.5	49.0	45-5 44-4	45.8
25 26	37·5 38.3	47-3	41.9	42.2	41.1	49.0	44.8	45.7
27 28	36.8	48.1	42.5 48.5	42.5	40.6	49.5	44.9 45.8	45.0
29 30	43.4 32.9	42.8	39.0	41.7 37.9	40.7	50.5	45.2 43.5	45.5
31	33.8	45.7	45.0	42.5	40.5	50.0	44.5	45.0
Mittel	8 37.91	8 48.49	8 43.14	8 42.98	8 39.12***)	8 50.06	8 44.19	8 44.

		SEPTE	MEER	1905	Окт	TOBER		
Tag	194	24	gh	Tages- mittel	194	24	9h	Tages mittel
	8 41.0	6° 50, 1	8 44.8	8 45.3	8 40.4	8 48.9	8 41.5	8° 43.6
2	40.3	50.0	45.0	45.1	40.0	49.2	8 41.5 43.8	44.3
3	41,2 39.0	57.1	45.0	47.5 44.3	41.9	49.1	43.8	45.0
5	42.2	55-3	45.2	47.6	40.9	49.4	44.2	44.8
6	41.0 39.4	50.7	45-4	45-7 45-3	40.1 42.4	52.5 47.6	43.0	45.2
8 9	41.7	52.7	46.9	47.1	42.0 42.1	46.2 46.6	40.7	43.0
10	40.8	54.0	43.5	45.0	41.2	47-3	43.0	43-9
11	41.0	41.8	40.6	41.1	40,1	47 - 4	41.2	42.5
13	37 · 3 38 · 3	45.8	41.1	41.4	40.0	48.7	42.6	43.8
14	37.9 38.3	48.1	41.9 45.6	42.6	41.9	47.2 46.7	42.6	43.9
15	41.3	50.0	45.8	44.3	41.1	47.4	43.6 42.8	43.5
17	41.6	50.8	45.5	46.0	41.1	47.7	39.5	42.8
18	42.1	51.3 48.2	45.4 38.9	46.3	40.7	47.1	42.3	43.4
20	47.5 40.8	48.1	45.6	44.8	40.8	47.9	42.6	43.8
21	42.7	49.5	45.9	46.0	40.9	47.9 46.0	41.9	43.4
23	42.3	48.0	44.0	46.5 44.8	37.6	45.2	41.1	41.3
24	41.6	48.1	43.7	44.3 43.0	40.4 39.4	44-3	41 · 3 38 · 8	42.0
26	43.8	50.0	42.4	45.4	41.3	45.6	37.5	41.5
27	42.0	46.1	40.1	42.7	38.6	44-5	40.9 40.1	41.3
29	41.5	47.0	44.1	44.2	38.6	42.6	39.8	40.3
30	40.9	46.8	46.4	44-7	38.8	44 3	40.5	41.2
Mittel	8 41.12	8 49.29	8 44.04	8 44.82	8 40.52	8 47.20	8 41.70	8 43.1
		Nove	MBER		DEZ	EMBER		
	8 39.7	8 45.7	8 40.2	8 41.9	8 38.0	8 41.3	8 39.0	8 39.4
3	38.9	45.0	42.1	42.0	38.7 38.7	42.2	39.2	40.0
4 5	39.9	47 - 1 45 - 4	38.7	41.9 42.3	38.5	46.1	38.2	40.9 39.9
6	19.3	47.7	41.2	42.7	37.7	40.9	39.4	39.3
7 8	40.7	43.9	39.6	41.4	39.3	41.3	39.8	19.8
9	39.7	45.5	40,5	41.2	38.9	41.6	39.4 38.8	39.8
10	40.9	42.7	40.9	41.5	39-5	42.1	39.7	40.4
11	39.6	45.3	40.8	41.9 36.3	39.3	42.8 42.7	40.1 39.0	40.7
13	37.8	47.7	39.8	41.8	41.0 38.7	41.6	37.0	39.9
15	38.4	42.4	24.0	34.9	39.0	40.4	39.5	39.6
16	37 - 3	43-7	36.3	39.1	39.6	41.7	40.0	40.4
17	37.9 38.3 38.8	42.6	38.0	39.5	39.5 39.3	42.0	39.0 39.7	40.2
19	38.8	41.7	38.4	39.5 39.6 40.3	39.6 39.0	41.2 42.3	37.6	39.5
21	39.3	43.7	39.5	40.3	38.4	40.9	35.8	39.0
22	38.2	43.2	38.8	49.1	39.2	40.3	39.5	39.7
23	38.2 38.5	43.4	36.0 38.5	39.2	38.9	41.9	39.5	40.2
25	39.2	47.5	38.7	41.8	39.1	41.8	39.4	40.1
26 27	40.0 39.0	41.2	38.4	39.9	39.2	41.6 41.6	39.1	40.0
28	38.9	42.1	18.4	39.8	39.3	44.3	36.5	40.0
30	39-3 39-1	42.7	38.8	40.3	39.4	42.9	39.0 36.3	40.4 39.4
31		****	,,,,		38.5	41.9	38.3	39.6
		8 43.98	8 38,25	8 40.45	8 39.11		8 38.91	8 39.9

Mittl. Zeit		Lesung	VarInstr. Stalen- teile	Benb Dekl, and Dekl, f.d Skalen- teil a	Mittl. Zeit		Lesung	VarInstr Skalen- teile	Beoh. Dekl. und Dekl. (d.Skalen- teil o	Mittl. Zeit		Lesung	Var Instr Skalen- teile	Beob Dek und Dek f.d.Skaler teil o
1905	Januar :	17. (♀), Seh	eller u.	Dörr.		1905 Apr	ril 11. (♂),	Schotter			1905	Juti 31. (©	, Dörr.	
21 13 18 21 25 27 29 33 41 46 52 59	a b b a Mire A a +360 a -360 a 3 max (a) +360 (a) +360 (a) -360	220 2.72 134 43.61 135 0.60 135 0.50 134 42.65 220 2.59 134 37.44 134 47.29 134 41.37 128 45.12 127 5.06 130 10.87 130 11.58	48.4 48.5 48.5 48.5 48.5 48.5 48.5 48.7 48.8 48.4 45.1	S 41.51 8 17-24 8 41.28 8 16.98	55 22 0 4 7 10	a b b a Mire A a + 360 a - 360 a a since b a (a) + 360 a) - 360	134 40.97 134 51.62 134 45.77 130 30.07 129 5.85	42.5 43.4 42.4 42.5 42.7 42.9 43.3 43.6 44.2 45.1		25 28 31 42 48	Mire A  a b b a Mire A a +360 a -360 a -360 (a) +360 (b)	135 1.84 135 42.27 133 17.93 137 50.08	56.2 56.0 55.9 55.7 55.8 55.5 55.4 54.3 54.0 53.9	8 42.1 8 140 8 42.4 1 14.5
1905	Januar 2	18. (30, Sch	eller u.	Dörr.		1905 Ju	ni 2. (Ç),	Scheller.			1905 A	ugust I. (	3), Döri	r.
21 55 22 3 5 80 14 16 19 25 31 36 41	a b b a Mire B a + 360 a - 360 a (a) + 360 (a) - 360	135 0.50	48.7 49.0 49.3 49.8 50.3 50.1 50.1 50.6 51.3	8 43,11 8 1863 8 44.02 8 1919	21 10 15 18 22 26 29 32 50 50 22 5	Mire A  a +360 a -360 a -360 a  a  (a) +360 (a) +360 (a) -360	220 5.09 134 42.24 134 58.21 134 58.36 134 43.41 220 4.68 134 47.19 134 39.33 134 43.36 129 18.13 128 5.24 130 35.95 130 31.67	31.4 31.7 31.9 33.8 34.9 35.4	8 36.94 8 31.46 8 37.60 8 21.97	47 51 53 22 6	(a) - 360	135 26.86	49.2 50.1 50.6 51.2 51.6 52.1 52.3 53.0 54.5 55.0 55.5	8 40.0 8 15.1 8 40.6 8 15.1
	1905 Ap	ril 7. (?), !	Scheller.			1905 Ju	ni 3. (†), 9	Scheller.		16	05 Septe	mber 12. (	ქ), <b>D6</b> ი	r.***)
21 56 22 3 4 9 16 18 32 37 41 49	a -360 Meaning (a) (a) +360 (a) -360	220 8.54 134 47.24 135 5.80 135 5.70 134 49.36 220 8.61 134 43.30 134 56.17 134 49.57 130 43.86 128 54.40 132 21.09 128 57.08	44.1 45.0 45.1 45.9 46.4 46.9 47.3 48.9 49.4 50.8		12 15 19 24 30 33 43	a b b a Mire A a +360 a -300 a	134 57-45 135 6-64 135 1-71 131 3-27	33.6 34.3 34.6 34.8 34.9 36.5 36.9 38.2 39.3 40.1	8 38.74 8 21.71 8 39.40 8 12.01	1 46, 51, 54, 58, 19 1, 6, 9, 20, 28, 38, 47,	a -360 a Manufact (a) (a) +360	135 13.36 134 57.80 134 58.15 135 14.31 234 11.02 135 21.69 135 13.41 134 18.58 131 57.06 136 33.39 135 16.67	30.7 34.4 36.7 38.9 39.0 38.6 38.4 38.8 38.6 38.6	8 36.7 8 20.4 8 38.4 8 19-4
	1905 Apri	i 10 (C), 1	Scheller			1905 Ju	li 28. (?),	Dörr. **	,	19	05 Septe	mber 13. (	), Sche	ller.
20	(a) + 360	135 10.60 135 5.45 130 39.93 128 56.59	43.5 44.0 44.3 44.9 45.8 46.0 46.0 45.8 46.3		29 32 38 41 46 49 21 58 22 5	step (a) (a) +360	220 54.92 134 36.40 134 52.48 134 52.73 134 37.14 220 57.46 134 31.82 134 36.15 130 30.87 129 8.67 131 31.97	37.5 37.8 37.9 38.2 38.3 38.5 38.6 41.3 44.0		23 25 29 32 36 40 51 58	a -360 a Neerby (a) (a) +360	220 0.86 134 56.24 135 12.52 135 12.67 134 57.11 220 5.71 134 49.37 135 5.73 135 5.746 135 20.51 132 55.05 137 39.06	43.5 43.7 43.8 44.0 43.9 44.5 45.0 46.3 46.7	8 39-72 8 17-8 8 40-2 8 48-9

Mittl. Zeit		Lesung	VarInstr. Skalen teile	Brot. Dekl. and Dekl. L. d. Skalen- teil o	Mittl. Zeit		Lesung	Vac -Instr. Skalen teile	Beob. Dekl, and Dekl. f. den Skalen leil o
	1905 Sep	otember 13. (5)	, Dörr.			1905 Nover	mber 21. (♂), S	cheller.	
	Mire A	220 0.32				Mire B*)	234 8.31		
18 45	a b	134 54.24 135 10.60	40.8	8 38.59	21 33 37	a b	135 12.55 135 58.90	52.0 52.4	8 39.58 B 1342
51 54	b a	135 11.35	40.9 40.9	8 38.89 8 18.39	41 45	b a	135 59.31 135 14.36	53.6 53.6	8 40.66
	Mire A	220 0.10				Mire B	234 8.41		
58 19 2 5	a +360 a -360 a	134 46.11 134 1.21 134 53.54	40.8 40.8 40.4	1	49 52 56	a +360 a -360 a	135 4 18 135 22.93 135 14.46	52.9 53.6 54.5	
15	Massing (A)	134 13.06	40.0 39.7	1	22 8	(a) + 360	135 39.41	56 6 57-3	
23 30 18	(a) +360 (a) -360 (b)	132 5.32 136 15.77 135 15.72	4L3 40.8		17	(a) -360 (b)	137 38 35	57.6	
30	(a) -360 (b)	136 15.77 135 15.72	41.3 40.8		27	(b)	134 28.62	57-4	
30	(a) -360 (b)	136 15.77	41.3 40.8			(b)		57-4	
23 30 38	(a) -360 (b)	136 15.77 135 15.72 tomber 14. (4),	41.3 40.8		2 <del>7</del>	(b)	134 28.62	57-4	
23 30 38	(a) -360 (b) 1905 Sep	136 15.77 135 15.72 tcmber 14. (4), 219 58.24 134 54.44	41.3 40.8	8 39.87 8 39.80		(b)	134 28.62 ber 27. (©), Sc 220 0.85 134 56.32	57.4 cheller.	8 39.07 8 14.07
23 30 38 21 20 25 27	(a) — 360 (b) 1905 Sep Mire A a b	136 15.77 135 15.72 tember 14. (4), 219 58.24 134 54.44 135 10.66 135 9.91	41.3 40.8 Dorr. 45.5 46.0 46.3	8 39.87 8 11.10 8 39.67	27   2 34 40 43	(b)  1905 Novem  Mirc A  a b b	134 28.62 ber 27. (°), Se 220 0.85 134 56.32 135 11.70 135 12.16	57.4 cheller. 49.5 50.2 50.3	8 39.60
23 30 38 38	(a) — 360 (b) 1905 Sep Mire A a b	136 15.77 135 15.72 tember 14. (4), 219 58.24 134 54.44 135 10.06 135 9.91 134 53.99	41.3 40 8 Dörr. 45.5 46.0	8 39.87	27   2 34 40	(b)  1905 Novem  Mirc A  a  b	134 28.62 ber 27. (°), So 220 0.85 134 56.32 135 11.70	57.4 cheller. 49.5 50.2	8 14:07
23 30 38 21 20 25 27 33	(a) -360 (b)  1905 Sep  Mire A  a  b  b  a  Mire A  a +360	136 15-77 135 15-72 tcmber 14. (4), 219 58-24 134 54-44 135 10.06 135 9.91 134 33-99 219 58-44 138 46-19	41.3 40.8 Dorr. 45.5 46.0 46.3 46.7	8 39.87 8 11.10 8 39.67	27   2 34 40 43 48 52	Mire A  a b b a Mire A a b b a A a A b b a	134 28.62 ber 27. (©), Se 220 0.85 134 56.32 135 11.70 135 12.16 134 56.93 220 0.70 134 45.88	57.4 cheller. 49.8 50.2 50.3 50.5	8 39.60
23 30 38 21 20 25 27 33	(a) -360 (b)  1905 Sep  Mire A  a  b  b  a  Mire A  a +360  a -360	136 15.77 135 15.72 tomber 14. (4), 219 58.24 134 54.44 135 10.06 135 9.91 134 35.99 219 58.44 134 46.19	41.3 40.8 Dorr. 45.5 46.0 46.3 46.7 46.9 47.4	8 39.87 8 11.10 8 39.67	27 2 34 40 43 48 55 55	Mirc A  a b b a Mire A a + 360 a - 360	134 28.62 ber 27. (©), Sc 220 0.85 134 56.32 135 11.70 135 12.16 134 56.93 220 0.70 134 45.88 135 5.25	57.4 cheller. 49.5 50.2 50.3 50.5	8 39.60
23 30 38 21 20 25 27 33 35 40 42 52	Igos Sep  Mire A  a  b  a  Mire A  a + 360  a - 360  a - 360	136 15.77 135 15.72 157 157 157 157 157 157 157 157 157 157	41.3 40.8 Dorr. 45.5 46.0 46.3 46.7 46.9 47.4 47.6 48.6	8 39.87 8 11.10 8 39.67	27   27   27   34   40   43   48   52   55   59   22   8	Mirc A  a b b a Mire A a + 360 a - 360 Basses (a)	134 28.62 220 0.85 134 36.32 135 11.70 135 12.16 134 56 93 220 0.70 134 45.85 135 5.25 134 56.07 134 45.85 135 5.25 134 56.07 134 25.07	57.4 cheller. 49.5 50.2 50.3 50.5 50.4 50.5 50.5	8 39.60
23 30 38 21 20 25 27 33 35 40 42	(a) -360 (b)  1905 Sep  Mire A  a  b  b  a  Mire A  a +360  a -360	136 15.77 135 15.72 tcmber 14. (%), 219 58.24 134 54.44 135 10.06 135 9.91 134 53.99 219 38.44 134 46.19 134 2.52 134 33.94	41.3 40.8 Dorr. 45.5 46.0 46.3 46.7 46.9 47.4 47.6	8 39.87 8 11.10 8 39.67	27 2 34 40 43 48 52 55 59	Mirc A  a b b a Mire A a + 360 a - 360	134 28.62 ber 27. (©), Sc 220 0.85 134 56.32 135 11.70 134 56.93 220 0.70 134 45.88 135 5.25 134 56.07	57-4 cheller. 49.8 50.2 50.3 50.5	8 39.60



#### RESULTATE AUS DEN METEOROLOGISCHEN BEOBACHTUNGEN.

Im Jahre 1905 wurden die Ablesungen an den meteorologischen Instrumenten täglich um 7 Uhr morgens (19<sup>6</sup>), 2 Uhr nachmittags und 9 Uhr abends gemacht.

NORMALBAROMETER GREINER & GEISSLER 501. Dieses Heberbarometer aus Berlin ist seit Frühjahr 1876 auf der Stertwarte und befindet sich im 7. Stocke genau neben dem zweiten Normalbarometer, dem Heberbarometer spitra 1891 einer Seehöhe von 206,00 Meter. An alle Abiesunge dieses Instrumentie ist eine Stelenkorrektion von 4-0 in Millindert anzubringen

NORMALBAROMETER SPITRA 189. Vom Jahre 1902 angefangen werden an diesem Barometer, welches eine doppelte Skala. Pariser Linien und Millimeter hat, nicht mehr wie vordem die Pariser Linien abgelesen, und diese nach Reduktion auf o' in Millimeter verwandelt, sonderen die Millimeter abgelesen und die in K<sup>2</sup> angegebenen Barometertemperaturen in C<sup>2</sup> verwandelt. An den Ablesungen in Millimetern ist jedoch eine Korrektion von 1-0,58 Millimeter ansubenigen (wide Anhang des Jahreganges 1901). Filst die Zeit von 1875 Juni 27 jül 1885 Ajurl 12 ergels sich aus 13 Vergeleichungen:

Von 1896 Februar 8 bis 1896 September 18 aus 9 Vergleichungen:

Greiner 501 - Spitra 189 = + 0,29.

Von 1902 Januar 7 his 1902 März 22 aus 46 Vergleichungen:

Greiner 501 - Spitra 189 = +0.38.

STATIONSBAROMETER TONNELOT 831. Wie im vorigen Jahrgange mitgeteilt wurde, hatte sich in diesem Barometer Luft angesammelt. Nach seiner Instandsettung wurde es seit Jahrcsanfang bei allen Terminberobaritungen mit abgeiesen. Da jedoch das untere Glasgeflaß mehrere Syringe erhelte, mußte das Instrument am 6. Jani wieder außer Drente gestellt werden und wurde erst anch erfolgter diesbezüglicher Reparatur seit 4. November wieder regelnaßig abgelesen. Aus 168 Vergleichungen mit dem Normalbarometer Gereiner & Geisster 50 in der Zeit vom zo. November bis 31. Derenbere ergab sich die Different:

Tonnelot 831 — Greiner & Geissler 501 = + \*\*\*\*

Zu den taglichen Luhdruckbeobachtungen wurde wie im Vorjahre dan Normalburometer Greiner & Geissler 501 verwendet, die Ablesungen desselben (3. Stock) jedoch auf die Sechho von Tonnelot (1. Stock) d. 1, 1972 Meter reduziert.

BAROGRAPH VON KERLL Derselbe wir während des Jahres 1900 ununsterhechen in Tätigknit; die Aufseichnungen wirm aufriedenstellend. Der die Genausgleit des Autorigaphen siehe den Jahrgaug 1870, sotet XXX. Bei den auf Seite 13 bis 46 an-geführten autographischen Aufreichnungen sind für die Stunde 29 die Beobachtungen au Greiner & Geissler 30 (vgl. den worber-gehenden Aufschritt mitgeleit). Die Zahlen der Bürnen Kolumnen ind unter Zugrandledigung der Abeuungen des genannten Barometers den Aufzeichnungen des Autographen entnommen.

Alle Angaben der Barometerstände beziehen sich auf die Seehöhe 197.2 m (I. Stock).

MONATSMITTEL DER BAROMETERSTÄNDE FÜR DIE EINZELNEN STUNDEN.

1905				Lnft	lruck:	auf of r	duziert	in Milli	metern			
1905	125	144	162	184	20h	224	Oli	24	41	64	84	10,
Januar	750,99	750.79	750.81	750.76	750.99	751.30	751.20	750.65	750.63	750.40	751.01	751.15
Februar	48.87	48.84	48.55	48.38	48.50	48.56	48.50	48.00	47.95	48,17	48.35	48,41
Māra	42.38	42.37	42.15	42.20	42.49	42.65	47.55	42.25	42.08	42.25	42.55	42.79
April	41.61	41.39	41.23	41.41	41.76	41.89	41.68	41.20	40.95	40.94	41.24	41.41
Mai	46.40	46.33	46.22	46.39	46.66	46.66	46.47	46.03	45.71	45.61	45.89	46.30
Juni	44.23	44.11	44.00	44.28	44.46	44.34	44.07	43.47	13.23	43.18	43.41	43.94
Juli	45.26	45.12	45.09	45.19	45.43	45.48	45.20	44.80	44.51	44.51	44.72	45.22
August	44.19	44.16	44.23	44.47	44.74	44.90	44.66	44.26	43.87	43.60	44.04	44.20
September	45.07	44.91	44.77	44.83	45.16	45.41	45.17	44.73	44.42	44.36	44.71	44.78
Oktober	42,96	42.89	42.79	42.98	43.33	43.46	43,31	42.80	42.65	42.82	42,99	43.00
November	40.78	40.65	40.53	40.55	40.79	41.05	40.93	40.65	40.76	41.09	41.22	41.3
Dezember	51.64	51.56	\$1.50	51.40	51.60	52.05	51.99	51.63	51.63	51.66	51.74	51.8
Tahr	745.37	745.25	745.16	745.24	745.49	745.65	745.40	1745.04	744.87	744.93	745.16	745.3

THERMONITER, PSYCHKOMETER, Für die Abbesungen der Temperatur sind die beiden, in ½ Celsiusgrade geteiten Themometer flesk auf Unterken und auf II (seucht in Verwendang, Über die Korrektionen dreselben siche Jahren größ, S. XV. und Jahrgang 1850, S. XV. auf Jahrgang 1850, S. XV. und Jahrgang 1850, S. XV. und Germannen der Fehrer bei e' mit firste gräßenem Schnee bestätigen die Konstant der Xuljumktschlen der bestätigen die Konstant der Kuljumktschlen der Schnee bestätigen die Konstant der Kuljumktschlen Schnee bestätigen die Konstant der Kuljumktschlen der K

THERMOGRAPH VON RICHARD FRERES. Derselbe ist seit Anfang 1891 im Gebrauch und funktioniert im allgemeinen bei kleinen und mittleren Temperaturschwankungen in zufriedenstellender Weise.

MONATSMITTEL DER TEMPERATUR EÜR DIE EINZELNEN STUNDEN

1905				Lustte	mpera	tur in	Zente	simalg	raden			
1703	12h	14 <sup>1</sup>	16 <sup>b</sup>	18+	20 <sup>h</sup>	22h	0,1	24	44	64	86	101
lanuar	-2,82	_3.o8	-3.34	3.59	-3.41	_2,S1	-1.56	-0.71	-0.84	-1.45	-1.71	-2.1
Februar	1.53	1,32	1.15	1,08	1,20	1,98	3.15	3.95	3.64	2,98	2.30	1.8
Marz	*14.99	*) 4.59			4.50	6.25	7.91			*)7-74		9)5.7
April	5.94	5.33	4.96	4-53	5.68	7.58	8.98	9.69	9.79	0.01	7.52	6.6
Mai	11.88	11,04	10.30	10.47	12.61	14.97	16.42	17.40	17.48	16.87	14.86	13.1
luni	16.63	15.62	14.69	15,11	17.95	20.61	22.54	23,10	22.75	22.33	19.94	18.1
uli	18.58	17.05	17.32	17-53	19.87	22.23	23.55	24.35	24.53	23.38	21.25	19.2
August	16.89	16.29	15.71	15.59	7.22	19.72	21.46	22.42	22.10	20.90	18.89	17.4
September	13.25	12.76	12.25	12.13	13.18	15.24	16.87	17.88	17.50	16.12	14.63	13.6
Oktober	5.17	4.90	4.71	4,36	4.76	5.95	6.95	7,79	7,40	6.39	5.74	5.3
November	3.80	3.52	3,36	3.20	3.37	4.16	5.28	6,20	5-75	4.83	4.27	3.5
Dezember	2.02	1.94	1.85	1.78	1.89	2.25	2.73	3.09	2.95	2.53	2.23	1.9
lahr	8.15	7.68	7.26	7.18	8.23	9.84	11.19	11.98	11.82	10.97	9.71	8.7

BEWÖLKUNG; WOLKENZUG. Får die drei Beobachtungsstunden: 19\(^1\) (p\\*\ morgens), 2\(^1\) und 9\(^1\) ist die Wolkenform, die Ausdehaung des bewölkten Teiles des Himmels nach der Skala: o=\heliet, 10=\text{trib}, endlich der Zug der Wölken angegeben. In den Morgen- und Abendstunden ist letzterer nur dann olleit, wenn die Kichtung der Bewegung der Wölken trotz der Dunkefheit ganz unzweifelhaft zu erkennen war.

OSLER'S ANEMOMETER MIT WINDFAHNE (von Adie), Während des Jahres 1905 traten einzelne, in den betreffenden Monatstafeln ersichtliche Unterbrechungen in der Registrierung des Instrumentes ein.

ROBINSON'S ANEMOMETER MIT WINDRÄDERN (von Adie). Dieses Instrument registrierte das ganze Jahr hindurch sehr regelmäßig. Die mitgeteilte Richtung des Windes ist vom Osler, die Geschwindigkeit vom Robinson genommen.

1905				3	deter	in cine	r Sek	ande				
1905	124	14h	16b	189	30 <sub>p</sub>	22h	O/I	27	4"	66	89	10%
lanuar	3.44	3.25	3.10	3.07	3.59	3.92	3.90	4.10	3.50	3-35	3 - 47	3.4
Februar	2.84	2.63	2.73	2.59	2.81	3.28	3.32	3.49	3.19	2.93	2.58	2.8
Marz	2.12	1.88	1.53	1.35	1.75	2.49	2.91	3.09	2.83	2.10	1.90	1.8
April	2.49	1.95	2.01	2.35	3.05	3.52	3.71	3.69	3.72	3.22	2.58	2.3
Mai	1.24	1.31	1.36	1.49	2.05	2.55	2,60	2.86	2.58	2.30	1.49	1.3
uni	0.95	0.92	1.01	1.33 .	1,69	2.17	2.79	2.90	2.93	2.74	1.99	1.0
ան	1.38	1.40	1.52	1.63	2.09	2.57	2.71	2.85	2.59	2.35	1.67	1.3
August	1.50	1.63 1	1.48	1.39	1.89	2.31	2.51	2.55	2.53	2.10	1.49	1.2
september	1.62	1.59	8.63	1.56	1.81	2.14	2.57	2.58	2,09	1.76	1.54	1.4
Oktober	3.50	2.49	2,66	2.44	2.85	3-34	3.80	3-73	3.09	2.57	2.50	2.5
November	1.68	1.41	1.66	1.76	1.86	2.14	2.64	2.52	2.05	1.68	1.92	8.6
Dezember	1.97	2.02	1.90	1.98	2.27	2.39	2.44	2.53	1.80	1.68	2.04	8.8
ahr	1.98	1.87	1.88	1.91	2.31	2.74	2.99	3.07	2.77	2.42	2.10	1.9

RICHTUNG UND STÄRKE DES WINDES, (Skala 0-10.) Die Angaben beziehen sich auf die Schätzungen der Beobachter.

HÖHE DES NIEDERSCHLAGES. Die beiden Regenmenser der Sternwarte sind in einer Höhe von 80 Metern über dem Eruboden ausgeheitlich. Die Niederschäugsbibe wird um 7 h\tim rungen geneusen, bei stakten Regen auch mehrmals im Tage. — In der Jahresübersicht bezieht sich die Kolumne -Tage mit Niederschlägen auf diejenigen Tage, an welchen eine am Omlerometer geneusen Menge von Regen oder Schnee sich ergage, die Kolumne -Tage mit Niederschlägen 's \_\_ion'\* auf diejenigen Tage, an welchen eine am Omlerometer geneusen Menge von Regen oder Schnee sich ergage, die Kolumne -Tage mit Niederschlägen 's \_\_ion'\* auf diejenigen Tage, an welchen eine Schnee sich ergage, an welchen die Schnee sich ergen und die jenigen Tage, an welchen eine Schnee sich ergen und die jenigen Tage in Mit die geschlägen Tage, an welchen eine Schnee sich er und die jenigen Tage, an welchen eine Schnee sich er u Ombrometer gemessen worden.

Zur Bezeichnung der Form des Niederschlages, sowie anderweitiger Erscheinungen dienen nach dem Beschlusse des internationalen Meteorologenkongresses (Siehe Verhandlungen des internationalen Meteorologenkongresses, Seite 481 die folgenden Zeichen:

Regen	Nepel =	Gewitter	Monuring
Schnee	Tau		Mondhof
Hagel	Reif	Sonneuring	Regenbogen
Grauneln	Schneegestöber +	Sonnenhoi	Höhenrauch ∞

#### Übersicht der meteorologischen Beobachtungen im Jahre 1905.

			Luft	druck	in Millin	netern				Т	emper	aturi	n Ze	ntesimalgr	aden	
1905	Millerry	Höchster	Tag	Tiefster	Tog	Absolute Schwankung	Maxim.	Mistlerey Minera	Misslere	Hörbste	Tag	Tiefrie	Teg	Abeniute Schwastung	Marieres Maxim.	Mattere- Matte.
	- an	9-24				-	-			2.			_			
Januar .	750.93	762.3	2.	721.3	7.	41.0	754.43		-2.29		29.	-15.7	3	22.3	0.23	-4.4
Februar .	48.42	60.3	9.	34.0	27.	26.3	51.08	45.12	2.18	7.2	23.	- 7.S	14.	15.0	4.22	0.3
Marz	42.39	50.2	22.	34.1	28.	16.1	44.52	40.35	10.07	14.6	30.	- 0.6		15.2	1 8.96	33.3
April	41.39	50.7	1.	30.2	21.	20.5	43.92		7.14		29.	- 1.8	7.	21.0	10.58	3.9
Mai	46.22	54.7	28.	35.5	21.	21.2	47-77		13.96		30.	6.1	24	20.1	18.28	9.6
Juni	43.90	53.3	24.	34 - 3	7.	19.0	45-33		19.12		5.4 30.	7-5	84.	23.4	24.14	14.2
Juli	45.05	50.7	3. U. 4.	38.4	5.	12.3	46.67		20.82		2.	12.1	21.	22.6	25.66	16.4
August	44.28	53.0	13.	30.3	29	22.7	46.15		18.73	32.3	5.		29.4.35		22.04	14.9
September	44.86	53.0	18.	35.3	30.	17.7	46.70		14.62		12.	5.0	18.	21.5	18.20	18.4
Oktober .	43.01	53.1	26. u. 27.		5-	22.7	45.07	40.83	5.79		5.	- 1.6	25.	15.3	8.07	3.7
November	40.86	54.0	18.	25.1	14	28.9	43.90	37-70	4.30		6.	1.4	19.	15.2	6.44	2.0
Dezember	51.68	64.9	11. U. I2	28.7	30.	36.2	53.97	49.42	2.27	10.4	9.	- 6.6	31.	17.0	3.81	0.5
Jahr	745.25	764.9	11. U. 12. Dez.	721.3	7. Jan.	43.6	747 - 46	743.01	9.39	34-7	2. Juli	-15.7	Jan.	50.4	12.63	6.3
		4	Di	nstdr	uck in A	fillimetern		1			Feu	chtigk	cit	in Prozent	en	
1905	5	Mittle	erer Gr	ister	Tag	Kleinst	er Ta	rg	Mit	tlere	Größte	i	Tag	Kk	inste	Tag
lanuar				4.9	29.	0.8		2.	1	77	qS	1	8.		46	2.
Februar		1 4.		6.0	6.	2.3		4.		79	95	1	12.		53	20.
Marz		. 5.		8.1	38.	3.6		3.		74	96	1	17.		42	27.
April				9.4	12	2.5		9.		69	99		21.		33	Q.
Mai		. 7.		1.8	5-	4.5		5.	1 6	63	45		9.		27	30.
Iuni		10.		5.3	29.	5.1		2.		61	93		25.		25	4.
Tuli				8.0	2.	6.6		5.		64	49	1	20.	- 1	10	Q.
August		. 11.		6.7	4.	6.8		8.		70	100		6		35	24.
September		9.			11. U. 12			9		74	100		30.		33	19.
Oktober		. 5.		6.6	S. D. 13			6.		74	98		25.		45	
November .		. 5		8.4	5.	3.2		7.		52	100		21.		58	17.
Dezember		4		7.6	8. u. q.	2.4		3.		83	98		o. u.		61	07-

6.85 1) Mittel aus 29 Tagen. - 7) Mittel aus 30 Tagen.

18.9

z. Juli

4. Juni

6, 8ug., 31, Sept., 21, Fox.

1905	Bewöi	1			Α		hide		a g c					Höbe	der Nieder	rechi
1403	kung	Heuter	Teilweise bedeckt	Trüb	Nebelig	mit Nieder- sehlagen	and Nieder- schlagen	mil Regen	mil Schnee	mit Grampein	mit Hegel	mit Ge- wittern	mitWind 6-10	Summe	Gridte in \$4 St.	1
anuar	6.9		24	7	14	12	2	7	10	1			0	10.7	4.2	1
ebruar	8.3	0	18	10	17	12	5	9	6	i	0	ò	0	8.2	1.8	١,
årz	8.6	0	18	13	24	15	9	15	1		0	0	0	25.9	4.7	
pril	8.1	0	23	7	17	13	6	12	- 6	2			0	27.4	13.0	1
ai	17.5	0	24	7	16	10	7	10	0		0	i	0	33.8	11.9	
mi	7.0	0	27	3	12	14	6	14	0	ň	0	7	ı o	42.0	10.6	
di	7.1	0	28	3	8	14	16	14	0	0	0	á	0	61.1	19.7	
ugust	7.5		25	6	20	15	13	15	0		1 0	3	0	93.6	31.8	ш
ptember	7.9	1	17	12	24	10	1.3	10	0	, o	ľ	3	ı o	40.6	11.7	)
ktober	9.0	1 6	22	9	17	13	7 8	13			1 6		1	19.7	5.2	1
ovember	8.7		14	16	25	13	8	8	ĭ	0	0		0	30.9	10.3	1
ezember	8.9	0	10	21	23	111	4	9	5	0	1 6		0	18.3	8.1	
hr	8.0	1 1	250	#14	217	148	88	136	29	5	1	22	1	412.1	31.8	i
					1	140		1.30	-9	,				1	31.0	1
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1,903	· N	digkeit leter in a Se		ke (o)				N	NE	E	1 5	E	S	SW	w	N
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		2.94	1.0	07   2	4. U. :	21.		2		1 7		2	1	3	12	
årz		2.15	1.		-, -, u	-3.		6	l i	3		1	5	2	15	
		2.89	1.	00 1 6	u. 21.			,	1 2	1 3	- 1	i I	0	3	15	
ài		1.93	1.		. u. 6.			3	3	5	- 1	i	i	i	4	
mi		1.67	1.		, 4			7	1 1	4	i	3	2	3	8	
li		2.04	t.		8. u. ra			1		0		0	0	0	26	1
ugust		1.88	1 1		o. u. 30			1	0	0	- 1	ī	i 1	3	32	
ptember		1.86	1.						1 1	0	- 1	;	,	3	17	
ktober		2.88	2.	00 6	. 11. 15.			3	-1 i	, o	- 1	0	3	6	3.2	
ovember		1.94	1.		3.			l i		1		ĭ	1	2	7	
ezember		2.08	1.	57 0	. 16, 11	30.	1	8	0	0	- 1	1		4 1	6	
ezember	- 1	2.08	1.	11	., 16. u.	30.		-	-	-	+	1		4	_	_
Dezember	- 1	2.08	1.	11	., 16. ц.	30.		31	10	19	t	16	17	30	186	
ahr	• • •	2.33		58			ormalhőh	31	10	19	1	16	17	30	186	
Dezember . ,	Wass	2.33 erstan	d d. Mo	idau		im. (No		31 e = 18	5.931****	19		16	17	- 1	186	
Dezember	• • •	2.33 erstan	1.	idau		im. (No	ormalhöh (ster	31 e = 18	10	19		16	17	30	186	
inuar	Wass	2.33 erstan	d d. Me	idau		im. (No	ster	31 e = 18	5.931 mm	19		16	17	30	186	
lezember	Wass	2.33 erstan	d d. Mo	idau	in Zent	im. (No	ster	31 e = 18	5.931 mm	19		16	17	30	186	
lezember	Wass Mittlers	2.33 erstan	d d. Me	idau	in Zent	Tiel	ster . u. 15.	31 e = 18	5.931 Different	19		16	17	30	186	
ihr	Wass Mittlers 19.6 42.6 61.6	2.33 erstan	d d. Mo	idau ter	in Zent	Tiel	ster . u. 15,	31 e = 18	5.931 mm	19		16	17	30	186	
1905  anuar cebruar darz pril da l	Wass Mittlers 19.6 42.6 61.6 57.9	2.33 erstan	1 d d. Mc	idau ter	in Zent	Tiel	ster . u. 15. . u. 2. . u. 19.	31 e = 18	5.931**** Differen: 31 64 42 28 35	19		16	17	30	186	
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inuar bruar bruar bruar dar pril ai ai	Wass Mittlers 19.6 42.6 61.6 57.9 53.1	2.33 erstan erstan 35 at 92 , 80 , 74 , 40 ,	1. d d. Mo	idau ter	in Zent	im. (No	ster . u. 15, . u. 2, . u. 19.	31 e = 18	5.931*** bifferen: 31 64 42 28 35 27 36	19		16	17	30	186	
inuar cbruar dar dar dar dar dar dar dar dar dar d	Wass Mittlere 19.6 42.6 61.6 57.0 53.1 20.3	2.33 erstan 35 ac 92 , 80 , 74 , 74 , 40 ,	1. d d. Mo Höchs n 11. 7- 19. 1- u.	idau ter	-10 Zent	Tiel  6 am 4  8 1  8 1  8 1  8 1  8 1  8 1  8 1  8	ster . u. 15. . u. 2. . u. 19.	31 e = 18	5.931 64 42 28 35 27 36 85	19		16	17	30	186	
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inuar	Wass Mittlers 19.66 42.66 61.6 57.0 53.1 20.3 10.2 25.1 21.3 36.9	2.33 erstan 35 at 92 , 80 , 74 , 74 , 24 , 79 , 38 ,	1. d d. Mc Höchs  11. 7- 19. 1. u. 11. 17- 8. 5- 18.	idau ter	-10 Zent	im. (No. Tiel 6 am 4 8 = 1 1 6 5 7 18 8 7 18 5 7 18 6 7 18	ster . u. 15. . u. 2. . u. 19.	31 e=18	5.931**** bifferen: 31 64 42 28 35 27 36 85 27 37	19		16	17	30	186	
nuar 1905 nuar broar arz ari ari iii agust systember	Wass Mittlers 19.6 42.6 61.6 57.0 33.1 20.3 10.2 25.1 21.3 36.9	2.33 erstan 92 - 80 - 74 - 74 - 74 - 79 - 38 - 57 - 73 - 73	1. d d. Mc Höchs  11. 7- 19. 4- 4. 4. 11. 17- 17. 8. 5- 18. 12.	idau ter	-10 Zent	Tiel  5 am 4  8 = 1  5 - 18  6 a 13  6 - 13  6 - 26	ster . u. 15. . u. 2. . u. 19. . u. 19.	31 e=18	5.931 5 64 42 28 35 27 36 85 27 48	19		16	17	30	186	
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not an unit of the control of the co	Wass Mittlers 19.6 42.6 61.6 57.0 33.1 20.3 10.2 25.1 21.3 36.9	2.33 erstan 35 at 92 , 80 , 74 , 74 , 40 , 24 , 79 , 38 , 57 , 73 , 74 ,	1. d d. Mc Höchs  11. 7- 19. 4- 4. 4. 11. 17- 17. 8. 5- 18. 12.	sidau ter	-10 Zent -10 28 33 46 46 35 -12 -12 -12 26 26 26 26	Tiel  5 am 4  8 = 1  5 - 18  6 a 13  6 - 13  6 - 26	(ster	31 e=18	5.931 5 64 42 28 35 27 36 85 27 48	19		16	17	30	186	
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1905  1905  brotar cbroar ar brotar ar ar ar ar brotar ar ar ar ar brotar ar ar ar ar ar ar brotar ar ar ar brotar ar ar ar brotar ar a	Wass Mittlers 19.6 42.6 61.6 57.0 53.1 20.3 10.2 25.1 21.3 36.9 X NNE	2.33 erstan 35 at 92 - 80 - 74 - 74 - 74 - 74 - 74 - 74 - 74 - 7	1. d d. Med Höchs  11. 7- 19. 1. 11. 17. 8. 5. 18. 12. 11. 17. Feb Ve	sidau ridau ridau 2. 2. 2. 2. 2. 3. 5. 5. 5. 5. 5. 5. 5. 5. 5. 5. 5. 5. 5.	in Zent	SSW SW	ster  . u. 15 u. 15 u. 19 u. 19 u. 19 u. 7 u. 7 u. 7.	31 E = 18   D   D   D   D   D   D   D   D   D	5.931 mm. bifferen: 51 64 42 8 35 7 36 85 27 36 85 10 8 10 8	V NNW	Kalm	An	merk	unger	186	
1905  1905  1905  1905  1906  1907  1908  1908  1908  1908	Wass Mittlers 19.6 42.6 61.6 57.0 53.1 20.3 36.0 42.7 36.9	2.33 erstan  35 at 92 - 80 - 74 - 74 - 79 - 38 - 57 - 73 - 74 - 79 - 10 - 10 - 10 - 10 - 10 - 10 - 10 - 1	1. d d. Mc Höchs  11. 7- 19. 1. 17. 8. 17. 18. 18. 18. 18. 18. 18. 18. 18. 18. 18	oidau eter  2. SESES	in Zent	Tiel  Tiel  S am 4  S 1  S 2  1 3  3 3  3 2  2 1 3  5 2 6  6 am 4  T Wind  SSW SW	ster . u. 15, . u. 19, . u. 19	31 E = 18	55.931**** 51 64 42 28 35 27 36 85 27 48 48 108	V NNW	Kalın 6	An	merk	unger	186	
1905  1905  Innuar  christian  christian  ai  ai  ai  ai  ai  ai  ai  ai  ai	Wass Mittlered 19.6 42.6 61.6 57.9 53.1 20.3 10.2 25.1 21.3 36.9 45.0 42.7 36.9	2-33 erstan 35 at 92 , 80 , 74 , 74 , 74 , 79 , 85 , 74 , 79 , 79 , 73 , 74 , 74 , 75 , 75 , 75 , 75 , 76 , 76 , 76 , 76	1 1. d d. Mee Höchs  1 11. 7- 19. 1- 1- 17. 8. 5- 18. 12. 11. 1 7 Fct  Ve	oidau eidau eidau eidau eir z.	in Zent	Tiel  Tiel  S am 4  S 1  S 2  1 3  3 3  3 2  2 1 3  5 2 6  6 am 4  T Wind  SSW SW	ster  . u. 15 u. 2 u. 19	31 D D D D D D D D D D D D D D D D D D D	55.931**** 51.64 42.28 35.7 36.85 85.7 37.48 48 108	V NNW	Kaim 6 6 11	An	merk	unger	186	
loos loos loos loos loos loos loos loos	Wass Mittler 19.6 61.6 57.9 53.1 20.3 10.2 25.1 21.3 36.9 42.7 36.9	2-33 erstan orl 35 at  92 - 80 - 74 - 74 - 79 - 38 - 74 - 74 - 79 - 74 - 79 - 74 - 79 - 74 - 79 - 74 - 79 - 74 - 79 - 74 - 79 - 74 - 79 - 74 - 79 - 74 - 79 - 74 - 79 - 74 - 79 - 74 - 79 - 74 - 79 - 74 - 79 - 79	1. d d. Med Höchs  11. 7. 19. 1. u. 11. 17. 8. 5. 18. 12. 11. 17. Feb Ve	oidau eidau eidau eidau er 2. 2. 5 SE S	In Zent	Tiel  5 am 4  5 - 3  6 - 3  7 - 3  7 - 3  7 - 3  8 - 2  7 - 3  8 - 2  8 - 2  9 - 3  9 - 3  1 - 2  9 - 3  9 - 3  9 - 3  1 - 2  9 - 3  9	ster  u. 15, u. 2, u. 19, u. 19, u. 19, u. 7, u. 8, u. 7, u. 7, u. 8, u. 7, u. 7, u. 7, u. 8, u. 7, u. 7, u. 7, u. 8, u.	31 D	5.931**** 5.931*** 54 42 28 3.5 27 36 52 37 48 48 108	V NNW	Kalm 6 6	An	merk	unger	186	
1905  1905  indar cbroar dra dra dra dra dra dra dra dra dra d	Wass Mittlerr 19.6 61.6 62.6 61.6 657.9 10.2 251.1 20.3 10.2 251.1 36.9 8 45.0 8 10.2 25 12.3 36.9 8 10.2 25 12.3 36.9 8 10.2 25 12.3 36.9 8 10.2 25 12.3 36.9 8 10.2 25 12.3 36.9 8 10.2 25 12.3 36.9 8 10.2 25 12.3 10.2 10.2 10.2 10.2 10.2 10.2 10.2 10.2	2.33 erstan sr  35 at 92 - 80 - 74 - 74 - 79 - 73 - 74 - 79 - 79	1. d d. Med Höchs  11. 7- 19. 1- 1- 17. 8. 5- 12. 11. 1- 17. Fct  Ve	sidau sidau ter  2. SES	In Zent  -10 28 33 46 36 -12 -22 28 11 20 21 21 21 22 22 26 -11 20 22 22 26 -11 20 22 22 26 -11 20 22 22 26 -11 20 22 22 26 -11 20 22 22 26 -11 20 22 22 26 -11 20 22 22 26 -11 20 22 22 26 -11 20 22 22 26 -11 20 22 22 26 -11 20 22 22 26 -11 20 22 22 26 -11 20 22 22 26 -11 20 22 22 26 -11 20 22 22 26 27 27 28 28 28 28 28 28 28 28 28 28 28 28 28	Tiel  5 am 4  8 8 = 1  6 - 18  6 - 18  7 - 18  7 - 18  8 8 = 1  6 - 18  7 - 18  8 8 = 1  7 - 18  8 8 = 1  8 8 = 1  9 - 18  10 - 1	ster  u. 15, u. 2, u. 19, u. 19. l. u. 7- lan.  drichtu  W8W	31 D	5-931**** 5-931*** 51 64 42 28 35 27 36 85 27 48 48 108	V NNW	Kalm 6 6 6 11 7 7	An	merk	unger	186	
1905  1905  1905  1905  1905  1906  1906  1906  1906	Wass Mittler 19.6 42.6 61.6 57.9 51.1 20.3 36.9 42.7 36.9 NNNB 3 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	2.33 erstan gr   35 at   92   92   93   94   97   97   97   97   97   97   97	11. dd. Med Höchs  Höchs  11. 7- 19. 1. 11. 17. 8. 18. 12. 11. 17. Feb  Ve E E ESE  10. 3 5 4 4 9 4 5 1 1 9 4 4 10 7 7 4 10 7 7 10 10 10 10 10 10 10 10 10 10 10 10 10	ridau ridau errariar  2. 2. 3 SE S	-10   -10	Tiel  Tiel  5 am 4  8 8 1  1 8 8 7  1 1 8 8 7  1 1 1 8 8 7  1 1 1 8 7  2 2 8 8 8  3 3 6 6 am 4  4 13  6 14  4 13  6 15  3 2 6  3 3 6	ster . u. 15. u. 2. u. 19. u. 19. u. 19. u. 19. u. 7 u. 7 Jan.  drichtu  6 5 5 5 5 2 5 1	31 D D D D D D D D D D D D D D D D D D D	31 64 42 28 3.5 27 36 85 27 48 48 108 11 8 2 2 3 3 1 1 2 1 1 1 1 1 1 1 1 1 1 1 1 1	V NNW 5 4 4 6 6 4 6	Kalını 6 6 6 11 7 7 11 11 12 12 12 12 12 12 12 12 12 12 12	An	merk	unger	186	
1905  Indar  Locker  L	Wass Mittler 19.6 61.6 61.6 61.6 61.6 61.6 61.6 61.6	2.33 erstan 35 at  92 ,  80 ,  74 ,  74 ,  74 ,  74 ,  92 an    NE EN    1	1. d d. Mc Höchs  Höchs  11. 7. 19. 19. 11. 17. 8. 18. 12. 11. 17. Feb  Ve  Ve  E ESS  10. 3 5 4 4 5 1 1 9 4 4 10 7 11 0	sidau ter  2. SESES	in Zent  -10 28 33 44 45 33 11 12 22 26 11 11 11 11 11 11 11 11 11 11 11 11 11	Tiels (Nec Tiels ) Tiels (Nec Ti	ster . u. 15 u. 2 u. 19	31 E = 18 D D D D D D D D D D D D D D D D D D	5-931**** 5-931**** 51 42 28 35 27 36 85 27 48 48 108	V NNW 5 4 4 6 6 6 7	Kalın 6 6 6 11 7 11	An	merk	unger	186	
1905  1905  Indar  chraar  chraar  da  da  da  da  da  da  da  da  da	Wass Mittler  19.6 61.6 62.6 63.6 63.6 63.6 63.6 63.6 63.6 63	2.33 erstan gr 35 at 92 , 80 , 74 , 74 , 74 , 74 , 92 an	1. d d. Mc Höchs 11. 7. 19. 1. 17. 8. 12. 11. 17. 8. 12. 11. 17. Fct Ve Ve E E ESI		in Zent	Tiels (No. 1) Ti	ster . u. 15. u. 15. u. 19	31 D D D D D D D D D D D D D D D D D D D	5.931 *** 51	19 NNW 5 4 4 6 6 7 5 5	Kalm 6 6 6 11 7 11 12 22 11 22 22 12 22 22 22 22 22 22	An	merk	unger	186	
notar  1905  notar  not	Wass Mittler 19.6 61.6 61.6 61.6 61.6 61.6 61.6 61.6	2.33 erstan gr 35 ar ge 74 - 40 - 79 - 38 - 57 - 74 - 40 - 79 - 38 - 57 - 73 - 73 - 73 - 73 - 73 - 73 - 73	1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1	sidau ter  2. SES 6 9 9 8 0 1 4	in Zent  -16 -216 -33 -33 -33 -33 -44 -7 -46 -47 -47 -47 -47 -47 -47 -47 -47 -47 -47	Tiels (Nec Tiels )	ster  u. 15. u. 2. u. 19. u. 19. u. 19. u. 19. u. 7. Jan. drichtu  WSW	31 E = 18 U U U U U U U U U U U U U U U U U U	10 10 10 10 10 10 10 10 10 10 10 10 10 1	119 NNW   NNW   5 4 4 6 6 6 6 7 5 3 5 3	Kaim 6 6 6 11 7 7 11 12 21 12 21 18	An	merk	unger	186	
igos	Wass Mittler 19.6 62.6 62.6 61.6 62.6 62.6 62.6 62.6 62.6	2.33 erstan 35 at 80 92 - 74 - 74 - 74 - 73 - 73 - 73 - 73 - 74 - 73 - 73	1. d d. Mee Höchs 11. 7- 19. 1. 17. 8. 5- 18. 12. 11. 12. 12. 12. 12. 12. 12. 12. 12	vidau ter  2.  S SE S	in Zent	Tiels 5 am 4 12 16 5 5 am 4 12 16 16 16 16 16 16 16 16 16 16 16 16 16	ster . u. 15, . u. 15, . u. 19,	31	100 5-931 *** 51 42 28 3.55 27 36 85 27 37 48 48 108 108 11 6 2 2 3 3 1 1 2 2 3 3 1 1 1 2 2 3 3 3 3 1 1 1 1	V NNW	Kalm 6 6 6 11 7 11 12 22 11 22 22 12 22 22 22 22 22 22	An	merk	unger	186	
i 1905  andar broar broar fârz prel fârz fârz fârz fârz fârz fârz fârz fârz	Wassister 19.6. 42.6. 61	2.33 2.33 2.35 ar spr   35 ar spr   35 ar spr   35 ar spr   36 ar spr   37 ar	1. d d. Mc Höchs 1. 1. 7. 17. 18. 19. 18. 19. 19. 19. 19. 19. 19. 19. 19. 19. 19	2. sES	in Zent  -16 -216 -33 -33 -33 -33 -33 -33 -11 -22 -22 -23 -22 -33 -33 -33 -33 -33 -33	Ties	u. 15, u. 19, u. 19, u. 19, u. 19, u. 19, u. 19, u. 7, u. 19, u. 7, u. 19, u	31 31 E = 18 11 12 12 13 14 15 15 15 15 15 15 15 15 15 15 15 15 15	10 10 10 10 10 10 10 10 10 10 10 10 10 1	119 NNW NNW 5 4 4 6 6 6 7 5 3 3 2	Kaim 6 6 6 11 7 11 12 22 13 8 4	An	merk	unger	186	
igos	Wass Mittler 19.6 62.6 62.6 61.6 62.6 62.6 62.6 62.6 62.6	2.33 erstan 35 at 80 92 - 74 - 74 - 74 - 73 - 73 - 73 - 73 - 74 - 73 - 73	1. d d. Mee Höchs 11. 7- 19. 1. 17. 8. 5- 18. 12. 11. 12. 12. 12. 12. 12. 12. 12. 12	2. status   1   1   1   1   1   1   1   1   1	In Zent	Tiels 5 am 4 12 16 5 5 am 4 12 16 16 16 16 16 16 16 16 16 16 16 16 16	(ster   u. 15, 10, 2, 10, 2, 10, 10, 10, 10, 11, 1	31	100 5-931 *** 51 42 28 3.55 27 36 85 27 37 48 48 108 108 11 6 2 2 3 3 1 1 2 2 3 3 1 1 1 2 2 3 3 3 3 1 1 1 1	19 NNW NNW 4 4 6 6 7 5 3 3 3 3 7 7	Kaim 6 6 6 11 7 7 11 12 22 13 4 4 4 14	An	merk	unger	186	

<sup>&</sup>lt;sup>9</sup>) Nach den Aufseichnungen des Prager städtischen Wasserleitungs-Buresus,

# Fünftägige Mittel des Luftdruckes, der Temperatur, des Dunstdruckes und der relativen Feuchtigkeit.

	1905		Luftdr. Millim.	Temp. Celsius.				Relat. Feacht. Prox.	1905					Temp. Celsius.	Dunst- druck Millim.	
			Aufzeic	raphisthen hounges	A	us direktes	Ablesung	ro			Aus outog	ruphtrchet/ houngen	A	un direktes	Ablesung	en
lanuar		bis 5	751.67	- 8.20	751.23	- 7.50	2.1	73	Iuli s	bis o	745.61	20.98	745-55	20.97	11.1	61
Junioni	. 6	. 10		1.81		1.01	4.0	77	10	- 14	46.02	20.50	46.00	20.21	11.6	66
	11	. 15	\$1.16	- 1.70		- 1.82	3.2	78	15	. 10	44.21	19.37	44.34	18.73	11.1	66
	16	. 20	48.82	- 4.60	48.63	- 4.13	2.7	78	20	. 24	43.24	18,40	43.24	18.91	10.6	66
	21	. 25	56.11	- 3.31		- 2.90	2.9	77	25	. 29	41.40	20.45	44.55	20.45	12.0	69
	26	, 30	\$6.37	1.14	\$6.28	1.18	4.0	81	30	n 3	43.70	20.75	43.54	21.23	12.2	67
	31	- 4	44.45	3.10	44.07	3 - 33	4.2	73	Accompany	. 8		10.64				
Februar	٠.		55.83		\$6.05		4.8		August . 4		43.44	19.05	43.72	19.71	12.5	75
repruar	* 5	- 9	50.08	3.97	50.74	3.87	3.2	79	14	a 13	47.87	18,26	47.76	19.13	10.9	67
	15	e 14	50.14	2.73	49.72	3.08	4.7	52	19		45.05	19.34	45.87	19.57	10.8	66
	20	- 24	46.44	2.78	46.57	2.93	4.4	77	24	25	42.52	18.62	42.25	18.58	10.8	65
	25	- 1	39.48	3.16	39.12	3.43	4.5	80	20	. 2	39.97	14.62	39.44	14.57	8,6	71
	-25	9 4	39.40	- 1	39.12		-		-,					-		
Marz .	. 2	, 6	43.15	3.69	43.34	3.83	4.9	80	September 3	× 7	43.94	17.13	44.17	17.46	10.6	72
	7	. 11	40.97	- 5.13	40.73	5.10	5.0	77	8	n 12	46.57	19.35	40.87	19.51	11.7	71
	12	, 16	38.89	7.70	38.78	7.79	5.6	72	13	- 17	48.58	13.51	48.60	13.53	9.2	80
	17	. 21	43.26	- 1	43-55	6.72	5.6	78	18	n 22	49.95	11,66	46.80	11.85	6.4	64
	22	- 26	44.74	5.02	44.59	5.08	4 - 4	69	23	n 27	38.80	12.30	41.05	12.75	8.8	80 68
	27	- 31	44-74	9.23	44.52	9.49	6,1	69	28	, 2	30.00	12.07	38.74	11.93	7-9	
April .	. 1	. 5	43.86	6.86	43.58	7.02	4.5	61	Oktober, 3	p 7	36.50	8.77	36.86	8.83	5.7	68
	- 6	. 10	38.45	3.59	38.66	3.68	4.0	67	8	. 12	46.86	6.51	46.97	6.54	5.9	81
	11	+ 15	40.94	9.10	41.21	8.92	6.4	75	13	. 17	39.08	3.68	38.99	5.59	5.1	75
	16	n 20		5.00	40.17	5.07	4.9	75	18	. 22	40.38	3.61	46.29	3.84	4.5	75
	21	* 25	-	6.47	40.13	6.56	4.9	68	23	- 27	48.65	2.47	48.67	2.66	4.0	73
	26	+ 30	44.03	11.71	43.98	12.09	6.6	64	28	, 1	42.00	5.80	41.66	6.03	5.6	80
Mai		. 5	_	15.08	46.57	15.60	8.4	65	November 2	- 6	40.27	S. 49	40.23	9.00	6.5	76
	. 6	- 10	46.95	14.00		15.04	6.9	57	7	. 11	40.94	5.84	40.80	5.85	5.9	85
	11	- 15	47.21	12.20	47.16	12.40	2.1	68	12	- 16	10,62	2.56	10.47	2.56	4.6	82
	16	- 20	44.12	15.04	43.77	15-34	8.7	63	17	- 21	45.12	2.70	46.54	2.92	4.7	82
	21	. 25	40.20	10.41	40.55	10.47	5.8	61	22	. 26	44.73	2.86	44.44	3.13	4.8	84
	26	. 30	51.32	14.95	51.39	15.21	6.9	56	27	- 11	45.35	2.96	45.63	3.07	4.8	54
	31	. 4	47.06	20.66	46.98	21.01	9.4	54	Dezember 2	- 6:	52.24	1.66	51.95	1.68	4.4	84
uni .	. 5	. 0	40.34	19.63	40.24	19.97	19.2	60	Dezember 2	. 11	54.11	5.44	54.41	5.46	5.7	84
	10		42.31	14.57	42.38	14.65	6.7	55	12	. 16	54.25	3.51	53-73	3.67	4.7	79
	35	a 14	41.63	19.44	41.74	19.60	10.5	66	17	. 21	53.93	-0.30	54.04	-0.23	3.6	80
	20	. 24	48.71	18.60	48.67	18.76	9.9	63	22	26	53.28	3.27	53.06	3.27	4.8	82
	25	- 29	44.08	20.76	43.88	20.98	11.8	67	27	31	42.00	0.12	42.16	-0.01	4.0	86
	10	1 4	46,47	25.73		25.88	14.7	61	-,	- 31	72.00	0.12	72.10	-0.01	4.0	34)



## METEOROLOGISCHE BEOBACHTUNGEN

IM JAHRE 1905.

			a) D	irckte Ablese	ngen.			
_	Luftdrug	k auf o' reduz	iert in Millim.	= 700*** +	I	ufttempera	tur nach Cels	ius
Tag	19h	2 h	96	Tagesmittel	19 <sup>b</sup>	2 h	94	Tagesmitte
	52.6	110	10				4	
	61.4	56.1	59.9	56.20	- 13.4	- 12.0	- 13.7	- 13.03
*	01.4	61.4	60.8	61,20	- 15.5	- 11.6	- 13.2	- 13,43
3	57.8	54.3	58.4	54.50	- 15.6	~ 9.1	- 7.8	- 10.83
4	46.5	46.1	45.5	46.03	- 6.9	- 4.1	- 2.5	- 4.50
5	41.1	38.2	35.3	38.20	1.7	3.3	3.3	2.77
6	35.2	34.6	20.8	33.20	2.4	4.0	2.4	2.93
7 8	23.6	30.3	43.5	32-47	3.2	3-4	1.6	
	56.3	56.4	55.3	56.00	- 1.6	1.4	- 0.2	2.73
9	52.0	48.0	42.2	47.49	- 2.9			- 0.13
10	43.9	47 - 3	49.6	46.93	2.8	4.3	5.1	1.83
11	51.7	50.1		K				
12	45.4	45.5	49.2	50.33	1.1	3.2	1.2	1.87
13	45.6	45.5	44.9	45.27	0.9	1.9	1.8	1.53
14			48.5	46.97	2.3	2.0	0.4	1.57
	56.0	57.6	57-5	57.03	- 3.9	- 3.4	- 4.5	- 3.93
15	56.7	56.1	56.5	56.43	- 9.7	- 8.9	· 11.8	- 10.13
16	53.4	50.8	48.5	1 00.00	- 13.7	- 7.8	— 6.3	- 9.27
17	44.7	41.9	40.8	42.47	- 6.6	- 4.3	- 6.9	- 5.93
18	40.5	41.8	45-3	42.53	- 6.9	- 1.4	- 3.2	- 3.83
19	49.9	52.1	54.9	52,30	- 1.8	1.7	- 1.3	- 0.47
20	55.5	54.9	54.5	54.97	- 4.0	0.6	- 0.1	- 1.17
21	51.0	54.2	56.0	54.70	- 0.9	2.1	- 1.5	- 0.10
22	\$6.6	57.0	58.4	57.33				
23	59.4	58,9	58.6	58.97	- 4.3	0.3	- 4.2	- 2.73
24	58.1	57.0	56.1	57.07	- 10.3	- 4.8 - 2.8	- 7.9	- 7.67
25	54.1	51.0	48.1	51.07	- 2.7	3.5	- 3.0 3.3	- 5.37
26	48.1	50.3						1.37
27	58.4	58.6	55-9	51.43	1.1	1.6	- 0.3	0.80
28	59.5	60.1	60.5	59.17	- 3.5	- 2.4	- 3.8	- 3.23
29	58.2	58.0	60.1	59.90	- 2.6	- 0.9	1.8	- 0.57
30	55-4		58.3	58.17	3-5	6.5	5.8	5.27
31	44.4	52.4	50.4	52.73	3.4	4.0	3-5	3.63
3.	44.4	42.2	47-7	44.77	3.4	5.6	2.8	3.93
dittel	50.83	50.65	51.10	50.86	- 3.56	- 0.71	- 1.89	- 2.05

Tag	Dur	stdruck	in Millir	netern	Ref	ative F	uchtig	keit	Rich	tung	u. Stār Skala: o	ke d - 10	es Win	d c
	194	2 <sup>h</sup>	94	Tages- mittei	194	2 h	gh	Tages- mittel	194		2 h		9	
	1 55	1.0	1.0	1.0				1						
2	1.0	0.8	1.0	0.0	72 72	56 46	67	65	ZZM	3	NNE	2	NW	-
3	0.9	1.5	1.6	1.3	72	66	64	61	NNW	1	SW	1 2	SSW	1
4	2.5	3.0	3.5	3.0	92	89	92	91	SSE	2	851		SSW	-
5	4.0	4.8	4.8	4.5	77	83	51	81	**	4	2211	3	S	
6	4.7	4.3	4.3	4.4	85	70		78	SW	1	33	•	sw	
7	4.7	4.3	4.4	4.5	81	73	79 85	78 80	2.10	3	W.	4	2 M	
7 8	3.4	4.5	4.4	1 4.7	84	7.3 89	95			5 2	W.	5	8	-
9	3.1	3.8	3.4	3.4	85	62	95	90	***	0	S		SW	- 3
10	3.7	3.6	4.1	3.8	66	68	35	73	W	3	w	1	W	1
11	3.9	3.7	1.8	3.8	79	65	75	73	SW	1	SSW	3	SW	
12	3.4	3.9	4.1	3.8	68	75	78	74	58	3	SW	3	W	
13	3.8	4.5	4.4	4.2	70	85	92	82	W	4	W	2	N	-
8.4	3.0	2.4	2.8	2.7	89	67	86	81	NNE	4	NNW	3	N	3
15	1.8	1.6	1.5	1.6	84	72	82	79	SE	2	ESE	1	SE	i
16	1.3	1.9	2.2	1.8	84	77	79	80	WSW		ENE	,	SE	
17	2.0	2.0	2.2	2.1	73	61	81	72	ESE	3	SE	3	SE	3
18	2.0	3.1	3.1	2.7	75	74	57	79	E	3	SE	2	E	- 3
19	3-3	3-7	3.7	3.6	8.2	71	88	l So	ESE	ĭ	SE	1	3	
20	2.6	3.3	4.0	3.3	77	68	87	77	E	1	E	3	E	3
21	3.6	3.7	3.6	3.6	82	69	88	80	E	4	SE	3	Е	4
22	2.5	3.0	2.9	2.8	77	64	86	76	E	2	SSW	i	Е	- 2
23	1.9	2.3	2.0	2.1	93	71	80	81	SW	1	NW.	1	***	-
	1.8	2.4	2.9	2.4	90	66	78	78	SSW	1	1.00	0	***	C
25	3.1	2.8	4.7	3-5	83	47	82	71	***	0	11.	2	W5W	4
26	4.0	3.8	4.0	3.9	79	75	89	81	WXW	3	NW	4	NNW	4
27	3.0	3.3	3.1	3.1	87	87	91	88	NNW	4	NW	4	WSW	2
	3.3	3.8	4.5	3.9	87	88	85	87	S	i !	NE	i	SW	2
29	4-7	4.9	4-4	4.7	80	68	64	71	WSW	i	15	3	11.	3
30	4.8	4.5	4.6	4.6	82	73	78	78	WSW	2	W.	2	WSW	4
	9.7	4-3	3.3	4.1	80	64	59	68	SW	3	W.	4	NW	4
fittel	3.0	3.2	3.4	3.2	80	71	80	77		2.0		2.0		2

Tag		Bewöl	kung ur	[Skala: old Woll	= heite	er, 10 =	trūb]	Nieder- schlag in		1	3 e m e	rkun	gen	
	15	ph.	-	2 <sup>ls</sup>		94	Tagesmitt	metern						
3 4 5	S S 1	1 ···· 1 ···· 4 ··· 10 ···		4 K 1 4 10	FS S S FBS	0 ··· 2 ··· 10 ··· 10 ···	1.7 1.3 6.0 10.0	4.2	Morge Morge Morg.	ns = , . ns * u. s Windst	Be, vor	indstöße, m mit	Unterbre	chunge
6 7 8	HS S	9 W	HS	10 W	HS HS	10 W	10.0 9.7 1.0	3-5				Tropf., na	chts o u of., mittag abds, stù	s stürn
9		10	FHS	3 NW	FHS	10 NW	3.7	0.1	Morge	3 u. 7	⊬ Flo	cken,		
11 12 13 14	HS I	10 ··· 10 W	Fil	7 NW 8 W 10 4 N	FHS FH FHS HS	5 W 8 N 4 NE	9.0 7.7 9.3 6.0 1.7	0.3 0.3	Abend 19 <sup>h</sup> & Morge	u. ∺, Flocken. ns ==, :	Windsto vorm. mittags	ße, nacht u. nachm [@ Dunst a.	u. K.	
16 17 18 19	HS FIIS HS	2	FS FHS FHS FHS	3 ··· 10 ··· 6 ··· 3 E	FS FHS 	0 10 SE 8 0	4.0 5.0 9.3 5.3 7.7		Morge Morge Morge Morge	ns, mitt ns u. at ns =, ns =,	ags u. a cends = mittags	€, aben		
21 22 23 24 25		7 N 4 *** 8 *** 9 ***	FMS FS S HS	6 8 4	H S FS S	1 ··· 3 ··· 4 ··· 10 ···	3.0 4.3 6.7 7.7 10.0		Morge Morge Morge Morge	ns =,		ids =, ags =, a ags u. abe Flocken,	ends =	
26 27 28 29 30	FIIS	5 NW 10 N 9 NW	HS HS HS	8 N 10 10 NW	FHS HS S S	8 NW 10 10	7-7 9-3 10-0 9-7	0.6	Morg.	u. mitta	(s = 1, 10	×. en, nacht: y ×, 8 × Windstöß	Fl. u. 🕦	Glatte
31		10		10 W	FIIS	IO W	10.0	0,6	Vorm	ittags se	itw. 🚱	21º 0.	6° * u. /	7.
Mittel		7-9		6.3		6.5	6.9	S. 10.7						
	1				Luft		ographis aufo'redu				+			
Tag	12 <sup>b</sup>	14%	161	184	Luft 20h			ziert in Mill			10p	Tages- mittel	Max.	Min
1 2 3 4	12 <sup>b</sup> 47.3 60.1 60.9 50.0 45.1	48.6 60.7 59.9 49.1 43.9	16 <sup>1</sup> 50.3 61.1 59.0 48.4 42.7	18 <sup>5</sup> 51.8 61.3 57.9 46.6 42.1		druck	oh 2  55.9 56  62.1 65  55.9 46.6 46	ziert in Mill	limetern	=700°**  8°*  59.7  60.9  51.8  46.0		Tages- mittel 54-47 61.23 55.89 46.95 39.80	Max. 60.1 62.3 60.9 50.0 45.1	Mi 47 - 60 - 50 - 45 - 34 -
1 2 3 4 5 6 7 8 9	47-3 60.1 60.9 50.0 45-1 34-2 24.8 48.1 55-1 41-5	48.6 60.7 59.9 49.1 43.9 34.1 21.7 50.4 54.7 40.8	50.3 61.1 59.0 48.4 42.7 34.4 21.9 53.3 34.2 41.1	51.8 61.3 57.9 46.6 42.1 34.9 22.9 55.8 52.4 43.0	20h 53.4 61.8 57.5 46.4 40.7 35.1 24.7 56.8 51.1 44.9	22h  55.1 62.1 57.1 46.6 40.4 35.5 26.5 57.9 50.5 46.7	auf o* redu  ob 2  55.9 56 62.1 56 55.9 56 46.6 44 39.5 38 35.4 33 35.4 33 57.8 56 48.8 48 47.1 47	xiert in Mill 4 4 56.9 61.3 3.3 53.3 1.1 46.1 2.2 37.6 634.0 33.1 455.9 46.7 3 48.4	58.4 61.1 52.5 46.1 37.0 32.5 34.9 55.7 45.1 49.4	= 700° 1 8° 1 59.7 60.9 51.8 46.0 35.7 31.3 39.4 43.0 49.6	10 <sup>h</sup> 60.1 60.0 50.6 45.4 34.7 28.2 43.3 55.3 41.8 49.7	mittel 54-47 61.23 55.89 46.95 39.80 33.78 29.31 54.89 49.28 45.79	60.1 62.3 60.9 50.0 45.1 35.5 48.1 57.9 53.1 51.0	47. 60. 50. 45. 34. 21. 48. 41.
1 2 3 4 4 5 6 7 8 9 10 11 12 13 14 15	47-3 60.1 60.9 50.0 45-1 34-2 24-8 48-1 55-1 41-5 51-0 48-7 45-7 50-7 57-3	48.6 60.7 59.9 49.1 43.9 34.1 21.7 50.4 54.7 40.8 51.4 47.6 43.0 57.3 57.1	50.3 61.1 59.0 48.4 42.7 34.4 21.9 53.3 54.2 41.1 51.7 47.1 45.2 53.8 56.7	51.8 61.3 57.9 46.6 42.1 34.9 22.9 55.8 52.4 43.0 51.7 46.0 45.3 55.3 56.5	20 <sup>h</sup> 53.4 61.8 57.5 46.4 40.7 35.1 24.7 56.8 51.1 44.9 51.8 45.7 46.1 56.7 57.0	22h  55.1 62.1 46.6 40.4 35.5 57.9 50.5 46.7 51.9 45.3 46.7 57.5	auf o' redu  oh 2  55.9 56.2.1 66.55.9 57.7 57.7 57.56.6 56.6 56.7 execution of the control of t	miret in Mill  4 b  4 b  1.1   56.9    .4   61.3    .3   33.3    .1   46.1    .2   37.6    .5   34.0    .5   34.0    .7   3    48.4    .1   49.8    .5   45.2    .8   46.5    .5   56.2	58.4 61.1 52.5 46.1 37.0 32.5 34.9 55.7 45.1 49.4 50.1 45.2 46.8 57.5 56.3	= 700 <sup>m</sup> 8 <sup>h</sup> 59.7 60.9 51.8 46.0 35.7 31.3 43.0 49.1 45.0 47.7 57.5	10 <sup>h</sup> 60.1 60.9 50.6 45.4 34.7 28.2 45.3 55.3 41.8 49.7 49.1 45.0 49.6 57.7 56.4	mittel  54.47 61,23 55.89 46.95 39.80 33.78 29.31 54.89 45.79 50.67 46.02 40.49 55.99 56.62	60.1 62.3 60.9 50.0 45.1 35.5 48.1 57.9 51.0 51.9 48.7 50.7 57.7 57.7	47. 60. 50. 45. 34. 21. 48. 41. 40. 48. 44. 45. 50. 56.
1 2 3 4 5 6 7 7 8 9 10 11 12 13 14 15 16 17 18 19 20	47-3 60.1 60.9 50.0 45-1 34-2 24.8 48.1 55-1 41-5 51-0 48.7 45.7 45.7 50-7 57-3 50-0 47-4 40.8 46.6 55-4	48.6 60.7 59.9 49.1 43.9 34.1 21.7 50.4 54.7 40.8 51.4 47.6 43.0 57.3 57.1 40.6 43.0 57.3 57.1 40.6 43.0 57.3	50.3 61.1 59.0 48.4 42.7 34.4 21.9 53.3 54.2 41.1 51.7 47.1 45.2 53.8 56.7 55.0 46.2 40.3 55.3	51.8 61.3 57.9 46.6 42.1 34.9 52.9 52.4 43.0 51.7 46.0 45.3 55.3 56.5 54.1 40.5 49.3	20 <sup>h</sup> 53.4 61.8 57.5 46.4 40.7 56.8 51.8 44.9 51.8 45.7 46.1 56.7 57.5 46.6 40.7 50.2 55.6	druck 22 <sup>h</sup> 55.1 52.1 57.1 46.6 40.4 35.5 57.9 50.5 50.5 50.7 46.7 51.9 45.3 46.7 57.5 56.8 52.7 44.1 57.1	auf o' reduced ob 2.1 6.2.1 6.2.1 6.2.1 6.2.1 6.3 55.9 5.4 6.6 4.3 9.5 33 55.8 57.8 57.8 57.8 57.8 57.8 57.8 57.8	mint in Mill  4 4 61.3	6%  58.4 61.1 52.5 46.1 37.0 32.5 34.9 45.1 45.2 46.8 57.5 56.3 49.5 41.2 43.4 54.6	8% 8% 8% 8% 8% 8% 8% 8% 8% 8% 8% 8% 8% 8	10 <sup>h</sup> 60.1 60.9 50.6 45.4 34.7 28.2 45.3 41.8 49.7 49.1 45.0 45.6 57.7 56.4 48.3 41.0 45.6 54.9	mittel  54-47 61,23 55.89 46.95 39.80 33.78 33.78 45.79 50.67 50.62 46.02 46.49 43.73 41.95 51.12	60.1 62.3 60.9 50.0 45.1 35.5 48.1 37.9 53.1 51.0 48.7 50.7 57.7 57.7 57.3 56.0 47.4 46.6 55.5	45. 34. 21. 48. 41. 40. 56. 56. 47. 46. 54.
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Tag						L	ufttem	eratur	nach C	clsius					
Lag	124	140	161	185	30 L	221	Op	2 <sup>h</sup>	44	6r	81	104	Tages- mittel	Max.	Min.
1 2 3 4 5	- 9.8 -14.4 -14.1 - 7.2 - 1.3	-10.4 -14.8 -14.8 - 7.3 - 0.6	-11.5 -15.1 -15.4 -7.5 0.2	-13.0 15.5 -15.5 - 7.1	-13.3 -15.2 -15.5 - 6.4	-14.5 -11.1 - 5.7	-12.4 -13.2 -11.3 -4.4 3.4	-12.0 -11.6 - 9.1 - 4.1 3.3	-12.5 -11.7 - 8.2 - 3.6 3.3	-13. -12.6 - 8 - 3.	6 -13.1 4 - 8.1 2 - 2.9	-13.3 7.4 2.2	-12.34 -13.75 -11.83 - 5.13 2.03	- 9.8 -11.6 - 7.2 - 1.3 3.7	-14.4 -15.5 -15.7 - 7.6 - 1.3
6 7 8 9	3.7 0.8 0.5 - 0.3 5.0	- 1.5 4.7	2.7 3.0 - 0.6 - 2.1 4.8	2.4 3.4 - 1.4 - 2.8 2.7	2.5 2.4 - 1.8 - 2.3 3.0	- 1.6 - 0.6	3.6 3.5 0.0 2.3 3.2	4.0 3.4 1.4 4.3 2.0	3.8 2.5 1.4 4.2	2.0 2.0 0 4.:	0 1.9 4 0.1 3 4.9	0.0	3.03 2.30 - 0.10 1.29 2.64	4.1 3.8 4.4 5-3 5.0	0.8 - 1.8 - 2.9 0.2
11 12 13 14 15	0.7 0.8 1.8 0.1 - 6.0	0.8 0.6 2.0 - 2.0 - 7.7	1.2 0.5 1.7 - 2.9 - 8.7	0.7 1.7 - 3.7 - 9.4	0.8 2.3 - 4.1 -10.2	- 4.3	2,2 1,7 2,6 - 4.0 - 9.4	3.2 1.9 2.0 - 3.4 - 8.9	2.5 1.5 1.5 - 3.8 - 9.4	1.1 0.4 - 4.5	7 2.0 6 0.6 3 - 4.4	1.8 0.2 - 5.3	1.60 1.27 1.59 - 3.51 - 9.44	3.2 2.0 2.6 0.1 - 6.0	0.7 0.2 0.1 6.0 12.4
16 17 18 19 20	-12.4 - 7.0 - 7.4 - 3.4 - 3.5	- 7.6 - 2.8	- 6.9 - 7.8 - 3.4	-13.4 - 6.6 - 7.4 - 2.3 - 4.0	-13.3 - 6.2 - 6.3 - 1.2 - 3.6	- 5.7 - 4.2 - 0.2	-10.0 - 4.8 - 2.4 1.0 - 1.5	- 7.8 - 4.3 - 1.4 1.7 0.6	- 6.3 - 5.2 - 1.2 1.7 0.9	- 6.1 - 6.2 - 2.3 0.4	2 - 6,6 2 - 2,9 5 - 0,9	- 7.0 - 3.4 - 2.4	-10.04 - 6.17 - 4.52 - 0.88 - 1.82	- 6.1 - 4.3 - 1.1 1.9 1.2	-13.7 - 7.5 - 7.8 - 3.5 - 4.0
21 22 23 24 25	- 3.1 - 6.1 - 8.9 - 3.4	- 3.2 - 7.2 - 9.7	3.8	- 0.5 - 4.1 - 9.9 -10.5	- 0.5 - 4.2 -10.2 -10.1 - 2.1	- 3.7 -10.4 - 8.0 - 0.8	- 0.7 - 8.0 - 4.9	2.1 0.3 - 4.8 - 2.8 3.5	- 0.2 - 4.4 - 2.1 3.1	- 1.5 - 5.4 - 2.4	- 3.1 - 7.0 4 - 2.6	- 5.1 - 8.6 - 3.2	- 2.73 - 7.57 - 6.31 - 0.10	2.2 0.3 - 4.4 - 2.1 3.9	- 3.1 - 6.1 -10.4 -10.6 3.6
26 27 28 29 30	- 1.7 - 3.7 2.6 4.6 3.1	- 3.2 3.2 4.3	1.7 - 2.5 - 2.6 3.2 3.9	3.4 - 2.6 3.8 3.6	- 3.6 - 3.6 - 2.2 4.1 3.7 3.7	- 3.6	- 2.8 - 0.6 6.4 4.1 5.0	- 2.4 - 0.9 6.5 4.0 5.6	- 1.3 - 2.7 - 1.2 6.6 3.9	- 3.6 - 1.5 6,1	5.9 3 5.9 3 6	- 3.8 2.2 5.8 3.4	- 2.96 - 1.37 4.96 3.89	- 1.7 2.6 6.6 4.6	- 1.7 - 3.8 - 3.7 2.6 3.1 2.5
31 M.M.	- 2,82	- 3.08	3.34	3.3		1 - 2.81			- 0.84	- 1.4	15 - 1.7	1	3.73	5.6 0.23	- 4·49
			Richt	ung (I	il Ger	chwind					Calanda				H
Fag					.,,	cuwind	igkeit	(G) des	Winde	s in i	Sckunde	in Meterr	1		Tage
i	12° R G	14 <sup>b</sup> R G	164		184 [	20 <sup>b</sup> H G	R G	O <sup>h</sup>	Winde		A' G	in Meters	8° R G	R G	
1 2 3 4 5	N 4. *) 3. S 0. SW 2.	R G  5 N 3. 2 °) 3. 4 SSW 1. 6 SW 2.	16 <sup>b</sup> R 0 N 3 ") 1 S 2 SSW	G R	N 3.3 *) 2.21 S 1.0	20 <sup>b</sup> R G N **) 4.0 SSW 2.1 WSW 4.2	22* R G	R  o o o o o o o o o o o o o o o o o o o	G R	G 6.0 2.0 1.7 4.4	*) 3.5 N 1.5 S 1.2	6 R G  NNW 1,6 SSW 3.0 SSW 3.2	8° R G  °) 2.5  NNW 1.1  SSW 3.0  S 3.0	R 0	### ##################################
3 4 5 6 7 8 9	N 4. *) 3. S 0. SW 2. S 3. SW 5.	R G  5 N 3- 2 °) 3- 4 SSW 1. 5 W 2. 2 SW 6. 5 WSW 4. 6 WSW 4. 6 SSW 0.	O N 3 °) 1 SSW 2 SSW 3 WSW 0 WNW 7 N 6 S	G R 4.0 2.1 1.7 1.7 8.0 WN 4.0 WS' 8.0 WN	N 3.3 *) 2.21 S 1.0 W 4.2 W 6.5 W 4.0 W 5.5 W 2.0 N 5.4	20° R G N **) 4.0 (55**) 1.9 SSW 2.1 WSW 4.2 W 6.2	22* R G *) 5. *) 3. SSW 2. WSW 4. W 7. W 50 W W 10	R  O  O  O  O  O  O  O  O  O  O  O  O  O	G R  1.0 N** 1.1 SSW 1.0 SW 1.8 WSW 1.5 WNW 1.5 WNW 1.5 WNW	6.0 2.0 1.7 4.4 5.5 W 8.0 7.5 3.8 W 2.7	*) 3.5 N 1.5 N 1.5 SW 3.0 SW 5.1 W 3.5 W 9.4 (SW 1.5 SSW 2.1	6 4.1 NAW 1.6 SSW 3.0 SSW 3.2 SW 4.9 WSW 3.0 NW 9.5 SSW 1.0 SW 2.1	8° R G  °) 2.5  NNW 1.1  SSW 3.0  S 3.0  SW 4.4  SW 3.5  NW 7.5  SSW 2.6  SW 4.7	R 0 W 1. SSW 3. SSW 4. SW 5. SW 5. SW 5. SW 6.	mitte 62 63 64.0 72.0 72.0 73.4 75.5 74.5 77.7 73.4
3 4 5 6 7 8 9	R G  N 4. *) 3. * 5 0. * 5 0. * 8 2. * 8 3. * 8 5. * \$ 5. * \$ 8 4. * NNW 7. * \$ 7. * \$ 8 1.	R G  S N 3- 4 SSW 1- 0 SW 2- 2 SW 6- 5 WSW 4- 9 WSW 7- 6 SSW 0- 5 WSW 4- 5 SW 4- 1 SW 4- 1 NNE 4- 4 NNE 4-	0 N N N N N N N N N N N N N N N N N N N	G R 4.0 2.1 1.7 2.2 SS 7.0 4.0 WS' 8.0 WN 3.5 WN 1.1 5.5 5.2 1.5 5.2 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5	N 3.3 *) 2.2 S 1.0 W 4.2 N 6.5 W 4.0 W 6.5 W 4.0 W 6.5 W 4.0 N 3.5 W 3.5 N 3.5 N 3.5 N 4.9 N 4.9	20 <sup>b</sup> R G N **) 4.0 S58** 2.1 WSW 4.2 W 6.2 WSW 4.4 WNW 7.1 WNW 3.5 SSE 1.4 W 7.2 SW 2.5 W 6.6 N 4.0 E 2.1	22 <sup>k</sup> R G  *) 5.* *) 3. *SSW 2. *WSW 4. *W 7. *W 5. *WNW 10 *W 2. *S 2. *W 5. *SW 5. *WSW 7. *W 6.	0	G R  1.0 N** 1.1 SSW 1.0 SW 1.8 WSW 1.5 WSW 1.5 WSW 1.6 WSW 1.0 SSW	G 6.0 2.0 8.7 4.4 5.5 W 8.0 7.5 3.8 3.8 3.8 4.0 4.0 4.0 4.0 5.5 W 5.5 4.4 5.5 8.0 6.0 6.0 6.0 6.0 6.0 6.0 6.0 6	R G N 1.5 N 1.5 S 1.2 SW 3.0 (SW 5.1 W 3.5 W 9.4 (SW 1.5	6 4.4 NNW 1.6 SSW 3.0 SSW 3.2 SW 4.9 WSW 3.0 NW 9.5 SSW 1.0 SW 2.1	8' R G  ") 2.5 NNW 1.1 SSW 3.0 S 3.0 S 3.0 S 3.5 NW 7.5 SSW 2.6 SW 4.7 W 5.6	R 0  4) 2. W 1. SSW 3. SSW 4. SW 5. SW 3. SW 6. SSW 3. SW 6. SSW 3. SW 6. W 5. SW 2. W 5. SW 2. W 5.	mitte /2  8 4.0  9 2.1  7 2.0  9 3.4  1 5.5  7 4.5  7 3.4  9 2.2  9 5.6  4.4  4.1  4.1
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1 2 3 3 4 5 6 7 8 9 10 11 12 13 14	48.5 43.7 38.7 48.5 48.0 56.5 54.7 54.1 59.9 57.6 50.8 44.7 48.9 56.7	48.2 43.4 39.9 49.9 48.2 56.7 54.3 54.8 60.2 57.3 49.2 44.4 49.1 56.6	47.7 41.2 40.6 50.4 49.0 57.1 53.6 54.8 60.3 56.7 47.9 44.1 49.3 56.6	46.6 40.1 41.3 50.8 49.5 57.3 53.7 55.3 60.2 55.8 46.7 44.2 49.9	45.9 37.4 42.0 50.7 50.9 57.7 54.0 56.3 60.2 55.6 46.1 45.1 51.6 56.2	45.2 37.2 42.8 49.0 51.9 57.9 54.2 57.6 60.3 55.5 45.9 45.6 52.9 45.6 52.9	45.1 37.1 43.7 43.7 48.0 52.7 57.3 54.3 57.6 60.2 54.9 45.6 47.1 53.5 55.4	44.8 36.8 44.4 47.7 53.0 56.6 53.6 57.5 59.7 53.4 44.3 47.6 53.8	41- 43.9 43.9 45.9 47.8 53.9 53.2 57.8 59.0 52.4 44.5 47.9 54.3 55.7	43.6 37.9 46.9 47.9 55.0 56.2 53.4 58.5 59.0 51.8 44.3 48.4 55.5 53.4	8 <sup>h</sup> 44.0 38.1 47.5 55.9 55.8 53.6 59.2 58.4 51.6 44.6 45.6 56.2 53.4	44.0 38.4 47.4 47.5 56.1 54.9 59.7 58.3 51.5 44.9 48.9 56.8	mittel 45-57 39-07 43-43 48-81 52-01 56-69 53-83 59-64 54-51 46-23 46-23 46-25 55-13	48.5 43.7 48.5 50.8 56.5 57.9 54.7 59.9 57.6 50.8 48.9 36.8 56.7	43.6 36.8 38.7 47.5 48.0 54.7 53.2 54.1 57.6 50.8 43.6 44.1 48.9 52.4 51.9
1 2 3 4 5 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19	48.5 43.7 38.7 48.5 48.5 56.5 54.7 54.1 59.9 57.6 30.8 44.7 48.9 56.7 52.4 55.7 53.6 49.7 47.5	48.2 43.4 39.9 48.2 56.7 54.8 60.2 57.3 49.2 49.4 49.1 56.6 52.4 55.7 53.4 49.4 49.4 49.4 49.4	47-7 41-2 40-6 50-4 49-0 57-1 53-6 54-8 60-3 56-7 47-9 44-1 49-3 56-6 52-2 55-6 53-0 49-4 44-2	46.6 40.1 41.3 50.8 49.5 57.3 53.7 55.3 60.2 55.8 46.7 44.2 49.9 56.4 51.9 55.6 52.1 49.5	45.9 37.4 42.0 50.7 50.7 50.9 57.7 54.0 56.2 55.6 46.1 45.1 51.6 56.2 55.3 55.3 55.3	45.2 37.2 42.8 49.0 51.9 57.9 54.2 57.6 60.3 55.5 45.9 56.2 95.2 52.5 52.5 52.5	45.1 37.1 43.7 43.7 48.0 52.7 57.3 54.3 57.0 60.2 54.9 45.6 47.1 53.5 55.4 47.1 53.5 55.8 55.6 51.0 51.1	44.1 36.8 44.4 47.7 53.0 50.6 53.6 57.5 59.7 53.4 44.3 47.6 53.8 54.0 52.7 55.4 49.9 50.6 88.8	43.9 37.5 45.9 47.8 53.9 56.3 53.2 57.8 59.0 52.4 44.5 47.9 54.3 53.7 53.7 53.7 54.9 54.9 54.9 54.9 54.9 55.9	43.6 37.9 46.9 47.9 55.0 56.2 53.4 58.5 59.0 51.8 44.3 48.4 55.5 53.4 53.5 53.9 54.5 53.9	8°- 44.0 38.1 47.5 55.9 55.8 53.6 59.2 58.4 51.6 44.6 48.6 48.6 56.2 53.4 54.4 49.5 49.6 38.7	10 <sup>5</sup> 44.0 38.4 47.4 47.5 56.1 54.9 53.9 59.7 58.3 51.5 44.9 48.0 56.8 53.0 55.3 54.0 49.8 48.6 48.6	mittel  43-57 39-07 43-43-43 48-81 52-01  56-69 53-58 56-93 59-64 46-23 46-23 46-38 52-55 55-13 53-08 55-18 49-93 41-29	48.5 43.7 48.5 50.8 56.5 57.9 54.7 59.9 60.3 57.6 50.8 56.8 56.7 55.7 55.7 55.7 55.9	43.6 36.8 38.7 47.5 48.0 54.7 53.2 54.1 57.6 50.8 43.6 44.1 51.9 53.6 49.3 47.5
1 2 3 4 4 5 5 6 7 7 8 9 10 11 12 13 114 115 116 117 20 21 22 23 24	48.5 43.7 48.5 48.7 48.5 48.5 54.7 59.9 57.6 50.8 44.7 48.9 56.7 53.6 49.7 49.7 49.7 49.7 49.7 49.7 49.7 49.7	48.2 43.4 39.9 49.9 48.2 56.7 54.3 54.3 54.8 60.2 57.3 49.2 44.4 49.1 55.4 55.7 53.4 49.2 46.2 38.9 46.2 38.9	47.7 41.2 40.6 50.4 49.0 57.1 53.6 54.8 56.7 47.9 44.9 49.3 56.6 53.0 44.2 38.6 44.2 38.6 44.2 38.6	46.6 40.1 41.3 50.8 49.5 57.3 53.7 55.3 60.2 49.9 44.2 49.9 55.6 52.1 49.5 42.8 38.8 45.7 52.2 49.9	45.9 37.4 42.0 50.7 50.7 50.3 60.2 55.6 46.1 45.1 51.6 56.2 52.3 55.8 55.5 41.6 49.3 46.3 52.5 49.3	45.2 37.2 42.8 49.0 51.9 57.9 54.2 57.6 60.3 55.5 45.9 56.2 9 56.2 52.5 52.5 52.5 52.4 40.1 39.5 47.1 49.0	45.1 37.1 43.7 48.0 52.7 57.3 57.3 57.6 60.2 54.9 45.6 47.1 53.5 55.4 55.4 55.4 55.4 55.4 57.0 60.2 54.9 47.1 53.5 57.3 57.3 57.6 60.2 54.9 47.1 53.5 57.3 57.3 57.4 57.4 57.4 57.4 57.4 57.4 57.4 57.4	44.1 36.8 44.4 44.4 53.6 53.6 53.6 53.6 59.7 53.4 44.3 54.0 52.7 55.4 47.6 88.8 39.4 47.8 50.9 47.9	43.9 37.5 45.9 47.8 53.9 56.3 53.2 57.8 59.0 52.4 44.5 42.9 54.3 53.7 53.7 53.7 53.7 53.7 53.7 53.7 53	43.6 37.9 46.9 47.9 55.2 53.4 58.5 59.0 51.8 48.4 35.5 53.4 48.4 55.5 53.4 48.4 55.5 53.4 48.4 48.4 48.4 48.4 48.4 48.4 48.4 4	8°- 44.0 38.1 47.6 47.5 55.9 55.8 59.2 58.4 51.6 44.6 48.6 56.2 53.4 49.6 49.6 49.6 49.6 49.6 49.6 49.6 49	44.0 38.4 47.4 47.5 56.1 54.9 59.7 58.3 51.5 44.9 48.9 56.8 53.0 56.8 53.0 56.8 53.0 56.8 56.8 57.4 48.9 48.9 48.9 48.9 48.9 48.9 48.9 48	mittel  45-57 30-07 43-43 48-81 52-01 56-60 53-85 56-93 59-64 54-38 52-65 53-13 53-03 55-18 40-93 41-29 39-96 47-10 51-25 48-54 45-37	48.5 43.7 48.5 56.5 56.5 57.9 54.7 59.3 50.3 57.9 50.3 57.9 50.3 55.5 57.9 56.7 55.7 55.9 56.7 55.7 55.9 56.7 55.7 55.9 56.7 55.9 56.9 56.9 56.9 56.9 56.9 56.9 56.9	43.6 36.5 36.5 47.5 48.0 54.1 57.6 53.2 44.1 51.9 53.6 44.1 51.9 53.6 47.3 38.5 38.5 38.5 44.5

128	Tag						L	ifttemp	eratur	nach (	Celsius					
1 2 2 5 2 7 2 7 1 7 3 5 5 3 7 2 7 2 7 3 3 5 7 3 3 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1		124	145	164	184	204	326	Oh.	211	46	64	84	top	Tages-	Max.	Min.
7	3 4	3.7 2.7 0.8	3.8 2.3 0.6	4.1 1.6 0.7	1.	5 5.5 5 1.5 9 1.0	3.5 6,2 1.6 1.0	3.3 6.2 2.4 3.0	7.0 1.8 3.9	3.6 0.8 4.0	3.1 1.	7 3-3 3 1-0 0 4.6	3.0 1.1 5.0	4.55 1.63 2.46	7.0 2.9 5.3	2. 2. 0. 0.
12	7 8 9	5.2 4.3 1.3	4.7 3.9	4.7 3.5	3.	4 4.3 2 2.7 1 1.2	1.5	5.5 3.1	6.0 3.6 2.5	6.5 3.3 2.4	2.8	5.1 3 2.4 3 0.6	4.6 1.9 - 0.2	5.12 3.12 1.30	6.5 4.3 2.6	4. 4. 1. - 1. - 2.
17	12	- 1.0 - 3.7 - 5.4	- 1.9 - 3.7 - 5.7	- 1.8 - 4.3 - 6.2	- 3. - 5.	4 - 2.9 0 - 5.4 2 - 7.8	- 2.1 - 4.2 - 5.9	- 1.3 - 2.8 - 3.1	- 1.5 - 2.2 - 1.2	- 2.0 - 2.0 - 0.9	- 3.6 - 3.6 - 2.5	- 3.4 - 4.0 2 - 2.9	- 3.7 - 4.2 - 2.9	- 2.24 - 3.74 - 4.28	- 1.6 - 0.8	- 1. - 3. - 5. - 7. - 2.
22 0.5 0.4 0.2 0.3 0.5 1.7 1.7 4.0 5.0 3 1.1 1.6 1.4 1.50 5.0 5.0 1.3 1.0 0.5 1.7 1.7 1.7 1.7 4.0 5.0 3.1 1.6 1.4 1.50 5.0 5.0 5.0 1.3 1.0 0.5 1.7 1.1 1.0 0.0 0.5 5.0 1.5 3.0 1.0 1.0 1.0 1.1 1.0 1.1 1.0 0.5 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0	17	2.5 2.6 2.2	2.1 2.5 2.2	2.1 2.5 1.5	2. 2. 1.	0 2.2 8 2.7 9 2.6	2.6 2.7 2.9	4.6 3.5 3.6	5.7 3.8 4.4	5.5 3.9 4.3	3.8	3.4	3-3 2.8 3.0	3.32 3.03 2.96	5.7 3.9 4.4	1. 2. 2. 1.
27	22	0.5 1.0 3.4	0.4	0.2 0.1 3.5	0.	3 0.5 0 0.5 3 4.3	1.7 3.0 4.9	3.7 6.4 5.9	4.9 7.2 7.1	5.0 6.7 6.8	6.1	1 1.8 1 4.6 2 3.6	1.4 3.6 2.2	1.96 3.39 4.53	7.2 7.1	- 0. 0. 0.
Richtung (R), Geschwindig keit (d) des Windes in 1 Sekunde in Metern    R	27	3.1	2.5	1.9	2.	2.3	2.5	3.7	6.3	4.0	3.1	4.3	3.7	3.63	6.4 4-3	1.
		1.33	1.32	1.13		00 1.3	1.9"	3.13	3.95	3.04	1.5	3.30		2.10	12	0.
W   W   W   W   W   W   W   W   W   W	ag								_							Tag
3																0
0 N 1.0 NN 0.6 KN 0.3 KN 0.5 K	3 4	WSW 4.	WSW WNW	4.7 WN	W 5.11 W 6.5 W 5.8 V	WSW 6.0 W 6.1	W 4.8 W 4.5 W 4.5	WSW 4.	WNW WNW WNW	5.7 5.3 WN 9.0 WN	W 4.4			W 6.5	W 7.	6.
2 W 5,5 W W 5,0 W W 5,8 W W 5,8 W W 5,8 W W 5,8	789	SSW 2. W 4.	SSW W NNW	3.5 WN	W 2,0 W 1.5 E 0.9	SW 3.2 NW 0.9 ENE 0.3	NNE 1.1 SSW 1.8	NNE 2. SSE 1.	SSE	1.5 88	B 1.0	NNE 3.0 SE 2.5	NNE 2.0 SE 1.0	NI.	N 2.	2.
\$ \$8\\ 1.5 \ \$8\\ 1.7 \ \$8.0 \ \$8\\ 1.0 \ \$8\\ 0.6 \ \$8		WNW 2	NW	1.8 WS	W 5.8 V E 1.5 W 1.1 V W 2.2 V	NNW 3.9 NNW 1.5 WSW 2.0	W 4.4 NW 1.8 SW 2.6	NNW 3.	S N S SW			NNW 3.3 W 3.9	W 4.6 W 4.6 NNW 2.4 WSW 2.1	W 3.9 W 3.9 NW 2.0 SSW 2.2 N 0.3	WNW 3.	2.
2 E 6.7 ENE 1.0 E 3.0 ENE 2.2 E 2.5 E 5.5 ESE 3.0 ESE 3.6 E 4.0 E 3.8 ENE 3.2 E 2.8 E 5.0 ESE 3.0 E 5.0 E 5.	3 4	00 0 1.		1 0	Wor	SSW 0.6	SW 4.6	SW 4.	SSW	5.2 5	W 5.5	SSW 2.6 SSW 0.8 WSW 4.1	SSW 1.6 SW 1.6	SSW 0.4	SW 1.4	3.
7   S 1.2   S 1.0   SSE 1.0   SSW 2.2   SSW 2.1   SSW 2.2   S 2.0   SSE 1.0   SE 2.5   SSE 1.6   SSE 1.3   S 2.6	3 4 5 6 7 8 9	SSW 1.	S SW	2.1 SS	S 0.6	SSW 3.6	SSW 4.6	SW 4.	7 SW	1.7 N	W 0.7	ENE I.I.	ESE o.	ENE 1.3	ENE o.	
	13 14 15 16 17 18 19 19 10 11 11 12 13	SSW 1. S 2. WSW 3. ESE 0. E 3. E 2.	S SW SW 2 WSW 2 ENE 7 ENE 8 E	1.2 2.1 SS 2.6 S 1.0 E7 1.6 3.6 3.0	W 1.6 W 1.7 E 0.6 E 3.9 E 4.0 E 4.1	NNW 0.4 ENE 2.2 E 3.0 SE 4.5	SSW 4.6 SSW 1.1 NNW 0.4 E 2.5 E 4.0 SE 4.1	NNE o. E 5. E 5. SE 3.	5 XE 5 ESE 5 ESE 7 SSE	1.7 NV 2.2 5.0 ES 4.1 ES	E 2.5 E 3.6 E 5.1 S 3.7	ENE 1.1. E 3.9 E 4.0 ESE 2.8 SSE 3.3	ESE 0.5 E 3.8 ESE 4.0 S 2.4	E 2.8 E NE 3.3 E 3.3 E 3.3	E 1.: E 2.: E 3.: S 0.:	1 1.

ð	Luftdruc	k auf o' reduzi	ert in Millim.	= 700°° +	L	ufttemperat	ur nach Cels	ius
Tag	19 <sup>h</sup>	g b	9 <sup>h</sup>	Tagesmittel	19h	2h	9 <sup>b</sup>	Tagesmittel
1	+-	gyfs.	140	-			3.8	
1	35 - 4	35.4	35.7	35.50	1.1	7-3		4.07
2	34.5	34.5	37.2	35.40	3.6		5 - 7	5.80
3	40.4	42.4	44.0	42.27	4.8	7-1	5.8	5.90
4 1	45.7		46.8	46.73	3-3	0.4		3.77
5	47.9	47.1	40,8	47.27	0.3	0.9	0.5	0.57
6	46.1	45.0	44.0	45.03	0.8	4.1	4.4	1,10
7	41.5	42.0	42.3	41.93	3.6	6.3	4.2	4.70
7 8	38.0	38.2	42.3	39.50	1.8	5.4	4.2	4.47
9 1	47.2	44.4	40.7	44.10	2.4	7.9	5.0	5,10
10	37 - 3	38.6	39.5	38.47	5.8	6.2	4.0	5.33
11	40.4	39.7	38.9	39.67	4.4	7.8	7.1	6.20
12	38.1	30.8	36.2	37.93	2.8	12.4		7.57
13	40.5	40.9	42.1	41.17	6.5	10.4	7.5 6.2	7.70
14	41.2	37 - 3	39.6	39-37	1.6	11.8	8.7	7.37
15	41.4	39.8	37-9	39.70	6.3	12.3	7.9	8.77
16	17.5	36.3	36.1	36.63	6,2	9.4	7.0	7.53
	37-5	39.1	41.2	19.03	5.7	8.5	7.8	7.33
17	43.9	41.8	41.3	42.03	4.4	11.9	7.0	7.77
19	43.3	43-3	44-3	43.63	2.6	11.6	6.6	6.93
20	44.4	40.4	46.8	45.87	5.7	6,3	5.6	5.87
21	46.4	46.9	48.3	47.20	4.6	6.7	5.8	5.70
22	49.9	49.5	48.8	49.40	0.9		3.6	3.97
23	47.7	45.1	44.2	45.67	- 0.6	7-4 8-6	6.0	4.67
24	42.3	41.7	42.6	42.20	1.5	7.9	5.5	4.97
25	44.6	43 - 4	42.7	43-57	- 0.2	9.5	5.9	5.07
26	41.6	42.0	42.8	42.13	4.7	8.5	6.9	6.70
27	47.0	45.5	42.0	44.83	5,6	12.2	8.7	8.81
28	34.1	42.2	47-6	41.30	10.2	7.9	6.4	8.17
29	49.7	48.3	47.5	48.50	4.3	11.8	9.3	8.47
30	47.1	45.2	43.9	45.73	6.8	13.6	11.4	10,60
31	40.9	43.8	46.5	43-73	12.3	13.2	8.6	11.37
Mittel	42.31	42.25	42.65	42.40	4.05	8.66	6.09	6.27

Tag	Dun	stdruck	in Millim	etern	Rel	ative Fe	uchtig	keit	Richt	ung	u. Stār Skala: o	k c de — 10]	s Wind	e s
	194	2 <sup>h</sup>	94	Tages- mittel	19 <sup>h</sup>	2 <sup>h</sup>	9,	Tages- mittel	191		21		9 <sup>ti</sup>	
	4.3	3.7	4.8	4.3	87	49	So	72		.	SE	,	SE	
2	4.8	5.3	5.5	5.2	82	66	80	76	E	i	SE	3	SE	- 1
3	5.4	5.3	6.2	5.6	8.4	70	90	81	- 11	0	NNE	ĭ	***	-
4	5.2	5.0	4.5	4.9	90	69	87	82	N	1	NNE	2	NNE	1
5	4.0	3.9	3.8	3.9	85	79	80	81	NW	i	***	0	***	-
6	4.1	4.6	5.4	4.7	83	76	87	82	***		WSW	,	SW	,
7	5.0	4.4	5.2	4.9	85	62	84	77	W	i	NW	2	W	1
8	5.3	5.6	5.0	5-3	88	83	80	84	SSW	1	11.	1	WSW	
9	4.3	4.4	4.5	4.4	79	56	69	68	SSE	1	SW	3	S	
10	5.0	5.2	4.7	5.0	73	74	77	75	SW	2	W	3	S	2
11	4.8	6.0	6.1	5.6	77	80	81	79	SW	3	SW	3	8W	1
12	5.0	5.8	6.2	5.7	89	54	80	74	NW	ĭ	SE	i	ENE	1
13 .	6.0	5.1	5.4	5-5	83	54	76	71	WSW	1	W	1	5	1
14	4.7	4.9	6.1	5.2	91	48	73	71	SSW	1	SE	1	SW	
15	6.1	5.5	6.0	5.9	87	52	75	71	SE	1	S	2	SE	
16	5.8	5.7	6.0	5.8	82	65	79	75	S	2	ESE	1	ESE	1
17	6.5	6.3	6.0	6.3	96	76	76	83	NNE	1	NNW	1	WNW	1
18	5.3	4.7	5 - 4	5.1	85	45	72	67	SSW	2	E	1	***	
19	4.9	4.4	5.9	5.1	89	43	81	71		0	SSE	1	SW	1
20	6.2	5.4	6.0	5-9	91	76	88	85	NW	1	NNW	1	M.M.M.	
21	5.4	\$.6	5.6	5-5	86	77	82	82	N	2	E	3	ENE	
22	4.1	4.1	4.2	4.1	84	53	72	70	E	8	E	2	E	:
23	3.6	4.1	3.9	3.9	83	50	56	63	E	2	SE	3	ESE	:
24	4.0	4.0	4 - 4	4.1	78	51	65	65	ESE	1	E	2	E	:
25	4.0	4.0	4.7	4.2	89	45	68	67	SW	1	***	0	991	•
26	5-7	5.5	6.3	5.8	89	66	84	80	***	0	W	2	SW	:
27	5.3	4.5	5.0	4.9	79	42	59	60	SW	2	SW	1	S	1
28	7.4	4.9	5.3	5.9	79	61	73	71	SW	2	W	4	W	:
29	5.5	5.7	6.4	5.9	80	56	74	73	S	1	SSE		SSW	1
30	8.1	6.4	7.7	7.1 6.8	74	69	77	73	SW	2	XXW	1	NNW	-
3.	0.1	v.4	5.8	0.0	77	56	69	67	511	3	AM	3	WW.	
Mittel	5.2	5.1	5 - 4	5.2	84	61	77	74		1.2		1.6		

MARZ

	1	Bewő1	kung [	Skala: e d Woll	enzug	er, 10 -	trüb]		Nieder- schlag						
Tag	194		2	ds		94	Tages	mittel	Milli- metern		,	sem e	rkun	gen	
1	FHS 10		.11	5 E	s	10		.3		Morgo	ens =,	ے, abe	nds =,.		
3	S 10		HS I	0 5		10	10.		0.7	Morg	ens m.	abends	nds == 0	-71 u. n	achts @
4 5	HS 10			o NE	HS	10	10.	.0		Morgens ■ <sub>e</sub> , 8½ ⊕ <sub>e</sub> , nachts ⊕.  1.0 Morgens ■ <sub>e</sub> , 7½ ⊕ <sub>e</sub> , nachts ⊕.  Morgens ⊕ <sub>e</sub> , 7½ ⊕ <sub>e</sub> ⊕ <sub>e</sub> , nachts ⊕.  4.4 Morgens ⊕ <sub>e</sub> , 7½ ⊕ <sub>e</sub> ⊕ <sub>e</sub> ⊕ <sub>e</sub> , nachts ⊕.		74 1			
0	S 10	1		0	8	10			1.0	Morgens = 1, 8½ ● 2, nachts ● .  .0 Morgens = 1, 8½ ● 2, nachts ● .  Morgens ● 1, 7½ − 9½ ● 3, nachts ● .  Morgens = 2, 22 − 2½ ● 2, 7 − 9½ ● 3.  Morgens = 4, nachts gen morgen ● 2,					
7 8	HS 10			O W		10	10.	0	1.0 1			ts D.			
9	FHS 10	***	FHS	8 SW	8	10	9.	-3	***	Morgens = , 8½			en 🚭 "	nacatas	
10	, , , ,				FIS	3	10.0 1.0 Morgens = 81 10.0 Morgens = 10.0 Morge					ts 📵.			
11	FS 7	FHS 9 HS 10 W S 10 S 10 F FS 7 FS 10 F HS 10 HS 10 FS 3 FS 8	FIIS	10	10.		1.5	Morg	ent an.	-	<b>.</b> .				
13	HS 10	***			FS	3	7.	.7	1.4	Morge	ens =	α.	nachte		
15	FHS 10			6 5		10	8.	7	1.4	Morg	ens und	abenda	■, nache		
16	HS 10			0 ***		10 ···	10.		0.3	Morg	. u. abd	5. Me. 1	54 🚭 nac	hts 🖜	
17	S 10		FIIS	7	***	10 W	10.		2.0	Morg	cns u. a	bends (	ma.	. O, mit	Untert
19	FS 9			0	FS	7	8.	.7	3.2	Morg	cns =,,	-, nac	hts ttags regn	- deals	
21	HS 10			0		10	10.		3.2				204 O Tr		
22	8 3		IIS	2 E	100	0	1.	.7		Morg	ens 🖦,	-, abe	nds 🖦 a	m Hor.	
23	HS 10	1	HS I	S SE	FHS	8	7.	.3	***	Morg	cns e,	bends a	=		
25	FS 8			8 S	FS	9	8.	- 3	0.3	Morg	cns ==,	w, abo	nds 🚐 , 1		
26	FBS 6			o W		10 W	10		4.6	Morg	ens en,	10h-22	åt u. 3åt.	-7 to O., 1	nachts (
28					FHS	8 W	9.	. 3		Vorm	nittags z	citweise	• Tropfe	n.	
30	FS 10	-10	HS I	0 11	FS	7	9.	3	0.5	Morg	ens ==,	201 @	nds =	<b>3</b> .	
31				9 11	FHS	10 W.	9.	-7	***	ļ.					
Mittel															
	,	-5	FHS 6 NW HS 10 W S 10 HS 10 W HS 10 W FHS 8 W S 5 FHS 5 FHS 9 W						S. 25.9						
		-5		8.9		Auto		sche	S. 25.9 Aufzeit in Milli			. +			-
Tag	124	14 <sup>b</sup>	16h	181		Auto	graphi	sche	Aufzei			104	Tages- mittel	Max.	Min.
Tag	12h	14 <sup>b</sup>	161	18 <sup>t</sup>	Lufte 20h	Auto Iruck	graphi nufo re	ische duzier 2h	Aufzeiet in Millin	6h	= 700°**	10h	mittel	DA	
Tag	12h	14 <sup>h</sup>	16 <sup>h</sup>	18 <sup>t</sup> 35·2 34·3	20h	Auto lruck : 22h	graphi nuf of re ob	ab duzier 2h 35-4 34-5	Aufzeiet in Millin	6h 35,6 36,0	8h 8h 35-7 36.8	10 <sup>h</sup> 35 · 6 37 · 5	35.45 35.18	36.7 37.9	34.8 34.3
Tag	12h 35.0 35.1 37.9	35.0 34.8 38.5	16 <sup>b</sup> 34.8 34.3 39.1	18 <sup>t</sup> 35·2 34·3 40.1	20h	Auto lruck : 22h 36.2 34.6 41.9	graphi nuf o* re o* 36.0 34.5 42.2	35-4 34-5 42-4	Aufzeid tin Millin 4 <sup>th</sup>	6h 35.6 36.0 43.2	8h 35-7 36.5 43-9	35.6 37.5 44.3	35.45 35.18 41.43	36.2 37.9 44.3	34.8 34.3 37.9
Tag	12h	14 <sup>h</sup>	16 <sup>h</sup>	18 <sup>t</sup> 35·2 34·3	20h	Auto lruck : 22h	graphi nuf of re ob	ab duzier 2h 35-4 34-5	Aufzeiet in Millin	6h 35,6 36,0	8h 8h 35-7 36.8	10 <sup>h</sup> 35 · 6 37 · 5	35.45 35.18	36.7 37.9	34.8 34.3
Tag	35.0 35.1 37.9 44.5 48.3	14 <sup>h</sup> 35.0 34.8 38.5 44.5 48.3 46.7	16 <sup>b</sup> 34.8 34.3 39.1 44.5 47.9 46.5	35.2 34.3 40.1 45.1 48.0 46.0	20h 35-7 34-5 41.1 46.2 48.1	Auto lruck : 22h 36,2 34,6 41,9 46,3 48,2 46,2	graphi nuf o* ro ob 36.0 34.5 42.2 46.4 47.9	35-4 34-5 42-4 46-0 47-1 45-0	Aufzeie t in Millin 4h 35.2 35.3 42.6 46.1 46.5 44.3	35.6 36.0 43.2 47.1 46.9	8h 35-7 36-8 43-9 46-8 43-8	35.6 37.5 44.3 48.6 46.7	35.45 35.18 41.43 46.10 47.56 45.45	36.7 37.9 44.3 48.6 48.3	34.8 34.3 37.9 44.5 46.5
Tag	35.0 35.1 37.9 44.5 48.3 46.9 43.7 41.2	35.0 34.8 38.5 44.5 48.3 46.7 43.2 40.2	16 <sup>h</sup> 34.8 34.3 39.1 44.5 47.9 46.5 42.2 39.3	18 <sup>t</sup> 35·2 34·3 40·1 45·1 48·0 41·5 38·2	20h 35.7 34.5 41.1 46.2 48.1 46.3 41.6 38.0	Auto lruck : 22h 36,2 34.6 41.9 46.3 48.2 41.9 37.3	graphi nuf o* re o* 36.0 34.5 42.2 46.4 47.9 45.9 42.2 37.9	35-4 34-5 42-4 46-0 47-1 45-0 38-2	Aufzeid t in Millin 4h 35.2 35.3 42.6 46.1 46.5 44.3 41.7 38.9	6h 35.6 36.0 43.2 47.1 46.9 42.1 40.3	35-7 36-8 43-9 47-9 46-8 43-8 42-3 41-6	35.6 37.5 44.3 48.6 46.7 43.9 42.2 43.0	mittel 35.45 35.18 41.43 46.10 47.56 45.45 42.22 39.51	36.7 37.9 44.3 48.6 48.3 46.9 43.7	34.8 34.3 37.9 44.5 46.5 43.7 41.2 37.3
Tag	35.0 35.1 37.9 44.5 48.3 46.9 43.7	14 <sup>b</sup> 35.0 34.8 38.5 44.5 48.3 46.7 43.2 40.2	16 <sup>b</sup> 34.8 34.8 39.1 44.5 47.9 46.5 42.2 39.3 46.8	18 <sup>h</sup> 35.2 34.3 40.1 45.1 48.0 41.5 38.2 47.2	20b 35.7 34.5 41.1 46.3 48.1 46.3 41.6 35.0 47.4	Auto ruck : 22h 36,2 34.6 41.9 46.3 48.2 46.2 41.9 37.3 46.9	graphi nuf o* ro ob 36.0 34.5 42.2 46.4 47.9 45.9 42.8 37.9 46.0	35-4 34-5 42-4 46-0 47-1 45-0 42-0 38-2 44-4	Aufzeit in Millin 4h  um  35.2  35.3  42.6  46.1  46.5  44.3  41.7  38.9  42.7	6h 35.6 36.0 43.2 47.1 46.9 43.9 42.1 40.3 42.0	8h 35-7 36.8 43-9 47-9 46.8 43-8 41-6 41-2	35.6 37.5 44.3 48.6 46.7 43.9 42.2 43.0 40.5	mittel 35-45 35-18 41-43 46-10 47-56 45-45 42-22 39-51 44-60	36.2 37.9 44.3 48.6 48.3 46.9 43.7 44.4 47.4	34.8 34.3 37.9 44.5 46.5 43.7 41.2 37.3 40.0
Tag	12h 35.0 35.1 37.9 44.5 48.3 46.9 43.7 41.2 44.4 40.0	14 <sup>h</sup> 35.0 34.8 38.5 44.5 44.5 46.7 43.2 40.2 45.7 41.3	16h 34.8 34.3 39.1 44.5 47.9 46.5 42.2 39.3 46.8 38.0	18 <sup>t</sup> 35·2 34·3 40·1 45·1 48·0 41·5 38·2	20h 35.7 34.5 41.1 46.2 48.1 46.3 41.6 38.0	Auto lruck : 22h 36,2 34.6 41.9 46.3 48.2 41.9 37.3	graphi nuf of re ob 36.0 34.5 42.2 46.4 47.9 45.9 42.2 37.9 46.0 37.4	35-4 34-5 42-4 46-0 47-1 45-0 38-2	Aufzeic t in Millio 4 <sup>h</sup> 35.2 35.3 42.6 46.1 46.5 44.3 41.7 38.9 42.7 38.8	6h 35.6 36.0 43.2 47.1 46.9 42.1 40.3	35-7 36-8 43-9 47-9 46-8 43-8 42-3 41-6	35.6 37.5 44.3 48.6 46.7 43.9 42.2 43.0	mittel 35.45 35.18 41.43 46.10 47.56 45.45 42.22 39.51	36.7 37.9 44.3 48.6 48.3 46.9 43.7	34.8 34.3 37.9 44.5 46.5 43.7 41.2 37.3 40.0 37.4
Tag	12 <sup>h</sup> 35.0 35.1 37.9 44.5 4b.3 46.9 43.7 41.2 44.4 40.0 40.4 18.8	14 <sup>h</sup> 35.0 34.8 38.5 44.5 48.3 46.7 43.2 40.2 45.7 38.8	16 <sup>h</sup> 34.8 34.3 39.1 44.5 47.9 46.5 42.2 39.3 46.8 38.0 41.4 38.0	35.2 34.3 40.1 48.0 46.0 41.5 38.2 47.2 37.5 40.8	20b 35-7 34-5 41-1 46-3 48-1 46-3 41-6 38-0 47-4 37-5 40-2 37-9	Auto 1 ruck : 22h 36,2 34,6 41,9 46,3 48,2 46,9 37,3 46,9 37,4 39,2 37,4	graphi nuf of re ob 36.0 34.5 42.2 46.4 47.9 45.9 42.2 37.9 46.0 37.4 39.5	2h 35-4 34-5 42-4 46-0 47-1 45-0 38-2 44-4 38-6 39-7 36-8	Aufzeie in Millin 4h wm 35.2 35.3 42.6 46.5 44.3 41.7 38.9 42.7 38.8 39.8 36.6	metern 6h 35.6 36.0 43.2 47.1 46.9 42.1 40.3 42.0 39.2 39.2 36.0	8h  35-7 36.8 43-9 47-9 46.8 42-3 41.6 44.2 39.4 39.0 36.3	10 <sup>th</sup> 35.6 37.5 44.3 48.6 46.7 43.9 42.2 43.0 40.5 39.9 39.2 36.8	mittel 35.45 35.18 41.43 46.10 47.56 45.45 42.22 39.51 44.60 38.54 39.98	36. 7 37. 9 44. 3 48. 6 48. 3 46. 9 43. 7 44. 4 47. 4 40. 4 41. 4 38. 8	34.8 34.3 37.9 44.5 46.5 43.7 41.2 37.3 40.0 37.4 38.8 35.8
Tag	35.0 35.1 37.9 44.5 48.3 46.9 43.7 41.2 44.4 40.0 40.4 38.8 36.4 42.2	14 <sup>b</sup> 35.0 34.8 38.5 44.5 48.7 46.7 45.7 41.3 36.8 38.1	16 <sup>b</sup> 34.8 34.3 34.1 44.5 47.9 46.5 42.2 39.3 46.8 38.0 41.4 38.0 39.0 41.8	35.2 34.3 46.0 41.5 38.2 47.5 40.8 37.9 40.0 41.3	20h  35-7 34-5 41-1 46-3 48-1 46-3 41-6 38-0 47-4 37-5 40-2 37-9 41-1 40-9	Auto 22h 36.2 34.6 41.9 46.3 48.2 46.2 46.9 37.4 41.9 37.4 41.3 39.7	graphi nuf o* ro o* 36.0 34.5 42.2 47.9 45.9 42.2 37.9 46.0 37.4 39.5 37.2 41.1 38.6	35.4 34.5 42.4 46.0 47.1 45.0 42.0 38.2 44.4 38.6 39.7 36.8 40.9 37.3	Aufzeit in Millin 4h wm 35.2 35.3 42.6 46.1 46.5 44.3 41.7 38.9 42.7 38.8 30.8 36.6 41.0 37.5	metern  6h  35.6 36.0 43.2 47.1 46.9 42.1 40.3 42.0 39.2 36.2 36.3 41.3 38.4	8h  an 35-7 36.8 43.9 47-9 46.8 43.8 42-3 41.6 41.2 39.4 39.0 36.3 41.6 39.3	35.6 37.5 44.3 48.6 46.7 43.9 42.2 43.0 40.5 39.9 30.2 36.1 42.0 40.0	mittel 35.45 35.18 41.43 46.10 47.56 45.45 42.22 39.51 44.60 38.54 39.98 37.32 40.32 39.93	36.2 37.9 44.3 48.6 48.3 46.9 43.7 44.4 47.4 40.4 41.4 38.8 42.2	34.8 34.3 37.9 44.5 46.5 43.7 41.2 37.3 40.0 37.4 38.8 35.8 36.4 37.3
Tag  1 2 3 4 5 6 7 8 9 10 11 12 13 14 15	12h 35.0 35.1 37.9 44.5 48.3 46.9 43.7 41.2 44.4 40.0 40.4 38.8 36.4 42.2	14 <sup>h</sup> 35.0 34.8 38.5 44.5 48.3 46.7 43.2 40.2 45.7 38.8 38.1 41.3 36.8 38.1 42.2 40.6	16 <sup>b</sup> 34.8 34.3 39.1 44.5 47.9 46.5 42.2 39.3 46.8 38.0 39.0 41.4 38.0 39.0 41.8	18h 35.2 34.3 40.1 48.0 46.0 41.5 38.2 47.2 37.5 40.8 37.9 40.0 41.3	20b 35.7 34.5 41.1 46.3 48.1 46.3 48.1 46.3 37.9 41.1 40.2 37.9 41.1 40.9	Auto 1 22h 36,2 34,6 41,9 46,2 41,9 37,4 46,9 37,4 46,9 37,4 46,9 37,4 41,3 39,7 41,9	graphi nuf o* re o* 36.0 34.5 42.2 46.4 47.9 45.9 42.2 37.9 46.0 37.2 41.1 38.6 41.2	35.4 34.5 42.4 46.0 47.1 45.0 38.2 44.4 38.6 40.9 39.7 30.8 40.9 37.3 39.8	Aufzeit in Millin 4h mm 35.2 35.3 42.6 46.1 46.5 44.3 41.7 38.8 39.8 39.8 36.6 41.0 37.5 38.5	metern  6h  35.6 36.0 43.2 47.1 46.9 42.1 40.3 42.0 39.2 36.0 41.3 38.4 37.8	700°°° 700°°° 8°° 700°° 8°° 700°° 8°° 700°° 8°° 700°° 8°° 700°° 8°° 700°° 8°° 700°° 8°° 700°° 70	35.6 37.5 44.3 48.6 46.7 43.9 42.2 43.0 40.5 39.9 30.2 36.1 42.0 37.8	mittel 35.45 35.18 35.18 41.43 46.10 47.56 45.45 42.22 39.51 44.60 38.54 30.98 37.32 40.32 39.93	36.7 37.9 44.3 48.6 48.3 46.9 43.7 44.4 47.4 40.4 41.4 38.8 42.2 41.9	34.8 34.3 37.9 44.5 46.5 43.7 41.2 37.3 40.0 37.4 38.8 35.8 36.4 37.3 37.3
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Tag  1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16	12h 35.0 35.1 37.9 44.5 48.3 46.9 43.7 41.2 44.4 40.0 38.8 36.4 40.2 40.2 40.2 40.2	14 <sup>h</sup> 35.0 34.8 38.5 44.5 44.3 46.7 43.2 45.7 38.8 41.3 38.8 38.1 42.2 43.6 37.5 36.2 40.6	16 <sup>b</sup> 34.8 34.3 39.1 44.5 47.9 46.5 42.2 39.3 46.8 36.0 41.4 38.0 39.0 41.0 37.0 36.2	18 <sup>t</sup> 35.2 34.3 40.1 48.0 41.5 38.2 47.2 37.5 40.8 37.9 40.0 41.3 37.2 36.4	Zob  35.7 34.5 41.1 46.3 48.1 46.3 41.6 35.0 47.4 37.5 40.2 40.3 41.8 40.3 41.8 40.3 41.8 40.3	Auto lruck: 22h 36,2 34,6 41,9 46,3 48,2 41,9 37,3 46,2 41,9 37,4 39,7 41,9 37,4 41,3 39,7 41,9 37,6 38,3 43,1	graphi nuf o* ro ob 36.0 34.5 42.2 46.4 47.9 45.9 42.2 37.9 46.0 37.4 39.5 37.4 39.5 41.1 38.4 42.7	sche duzier 2h 35-4 34-5 42-4 46-0 47-1 45-0 42-0 438-2 38-7 36-8 40-9 37-3 39-8 36-3 39-1 41-8	Aufzeit in Milliu 4h 35.2 35.3 42.6 46.5 44.3 41.7 38.9 42.7 38.8 30.8 30.8 30.8 30.8 30.8 30.8 31.9 4	35.6 36.0 43.2 47.1 46.9 43.9 42.1 40.3 42.0 39.2 36.0 41.3 37.8 35.9 40.1	8h 35-7 36.5 43-9 47-9 46.8 43.8 42-3 41.6 41.2 39.4 39.0 36.3 41.6 39.3 37-9 36.1 40.8	10 <sup>th</sup> 35.6 37.5 44.3 48.6 46.7 43.9 42.2 43.0 40.5 39.9 30.2 36.1 42.0 37.8 36.4 41.7	mittel 35.45 35.18 41.43 46.10 47.56 45.45 42.23 40.32 39.93 36.88 38.34 42.18	36.7 37.9 44.3 48.6 48.6 48.7 44.4 47.4 40.4 41.4 40.4 41.4 38.8 42.2 42.2 42.2 42.2 43.2	34.8 34.3 37.9 44.5 46.5 43.7 41.2 37.3 40.0 37.4 38.8 35.8 35.8 37.3 37.5 35.9 40.9
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		6.3	5.8	5.8		5.8	6.6		6.5	8.6	8.0	7-9			8.8	9
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Richtung (R), Geachwindigkeit (C) des Windes in 1 Sekunde in Metern   T.		7-7	6.8	6.4	6,2	8.2	8.5	11.9	13.6	14.6	13.5	12.2	11.1	10.06	14.6	
Richtung (R), Geschwindigkeit (G) des Windes in 1 Sekunde in Metern  The sekunde in Metern	1	11.8	10.6	10.9	12.0	12.3	13.1	13.6	13.2	12,4	11.8	10.1	5.0	11.65	14.0	- 2
128	4.	*) 4-99	4.59	4.18	3.98	4.50	6,25	7.91	8,66	*)8.64	97-74	16.58	*)5-73	**)6.07	*)8.96	*)3
128				Rich	ung	(R), Ges	chwind	gkeit	G) des	Wind	es in 1	Sckunde	in Meter	n		Ta
R	kg	7.03	1	1 16	1	.01	anh	anh		_	ah I	46	- 6h	1 6	Lob	mi
B	_									G						L
Section   Sect		S 2.0	80	.6 SSW	1.0	55E 0.7	S 1.1	S 1.	o S	2.1	SE 2.1	SE 2.3	ESE 1.	ESE 1.	4 ESE 1.6	1
No.	2	PCF - 1	PCP a	.1 FOR	1.1	ESE 1.4			6 ESB	3.51	SE 6. 3	SE 3.4	SE 3.	SE 2.	e ESE 1.1	2
NNE     0		No.5	N I	2 NNE	2.0	NNE + 8	3 2 O	NNE 1	o NNE	2.5	NE 2 8	NNE 4 0	NNE 2	NNE 1	No.	2
WSW 1.2   SSW 1.4   SW 0.7   SW 1.5   W 1.5   W 1.0   W 0.5   S 1.0   SSW 1.6   W 1.1   W 1.8   W 1.0   W 1.5   W 1.0   W 1.5   W 1.		NNE 1.6	NI	.5 NNE	1.5	NNE 1.6	N 1.5	NNE 1.	1 NNE	1.6 7	NE 1.0	NNE o.6	NNW 1.	N 1.	WSW 1.2	1
W 2-0	J,	WSW 1.2	SSW 1	A SW	0.7	SW 0.7	SWILE	W t	8 W	1.0	W 0.8	\$ 1.9	SSW 1.4	SW L	W 2.1	1 1
SN   10   SN   12   SN   12   SN   12   SN   13   SN   13   SN   14   SN		W 2.0	SSW I	. z   SW	1.6	SSW 1.4	W 3.1	W 4.	1 W	3.4 W	NW 3. C	W 2.4	With	With	SW o.c	1 2
S   S   S   S   S   S   S   S   S   S		WSW 2.2	WSW 2	9 551	1.7	50.9		35W 2.				W 4. C	W 6.1	W 7.	W 5.6	3
WSW 1.0   WSW 0.4   SSW 1.0   SSW 0.5   SSW 1.0   SSW		51.1	SW s	4 88	2.4	SSW 2.4	SW 2 2	W 2	WNW	3.0 W	NW 5.8	WSW 4 5	WSW 2	SSW 2	WSW 1.6	3
SSV 1.0   SSW 1.6   WSW 0.6   N 1.0   NSW 0.7   SSE 1.9   S 2.0   SS 0.0   SS 1.5   ESC 1.5   E. 0.0			wew .	. cen			ccw - c		. cw							
SSV 0.9   WW 0.4   SSV 0.6   SS 0.5   SSV 0.5   SSV 0.5   SSV 0.5   SSV 0.6   SSV 0.		SSW 1-0	SSW I	6 WSW	0.6	N 1.0		SSE 1	0 8	2.0	SE 0.9	SE 3.5	ESE L.	E n	411 0.0	1 1
SN 1.9 SN 1.1 SR 6.5 SE 6.7 SN 2.0 SN 2.6 SN		SSW 0.9	WINW O	.4 SSW	0.4	50.2	SW 2.3	SW 1.	o SW	3.1 W	511 3.0	WSW 2.3	SW 1.3	2 SSW 1.	8 1.1	1 1
SSE 1.0   SSE 1.0   SSE 1.0   SSE 0.1   SSE 0.2   SSE 0.2   SSE 0.2   SSE 1.0   SSE 1.2   SSE 0.2   SSE		S 1.0	SSE 1	.1 SF	0.5	SE 0.5	SSE 0.9	33E 2.			SSE 3.6	SE 2.5	S 2.0	5 SSW 2.4	SW 1.6	1
SSE 1.0   ESC 1.0   E 0.5   E 0.1   NW 1.0   NXE 0.0   NXW 1.1   NXW 0.3   NXW 0.5																
NSW 1.0   NSW 3.0   NSW 1.0   NSW 1.5   NSW 1.0   NSW 1.4   NSW 1.4   NSW 1.4   NSW 1.6   NSW 0.5   NSW		SSE 3.0	SSE I	.9 ESE	0.5	SE 0.9	NYW . 6	SE 1.	4 ESE	2.2 1	ESE 2.6	E 2.6	ESE 3.0	ESE I.	ENE 1.2	
\$\begin{array}{c c c c c c c c c c c c c c c c c c c		101. 11	WYW 2	.0 SSW	1.0	SW o.8	SSW 1.6	WSW L.	4 WSW		SE o.o.	S 1.0	55W 0.1	50	NNE o. S	, š. 1
\$ 6.0 \$ 8.0.4 \$ 8.0.4 \$ NW 0.5 \$ NW 0.5 \$ NW 0.5 \$ NW 0.5 \$ NW 0.0				.0	0.0	u. 0 0	*** 0.0	SSW o.	4 SSW	1.1	\$ 1.6	SSW 1.1.	WNW 2.			1.0
ERRE-10	The second	ENE 0.2		.41 5	0.4		NAW 2.2	NNW 4.	5 N		NW 3.0	NNW 2.0	NNW 2.0	VA 1	3 ANW 2.8	
ERRE-10		ENE 0.2 S o.6	So				N	NNE 2.	7 ENE	3.2	XE 2.0	E 2.5	ENE 2.	ENE 2.	SE 2.0	2.
\$85.5   \$80.0   \$1.1   \$80.1		S o.6	S o	S NNW	1.5	X 1.6	4 1.9					ESE 4.0				
EREC. 5   NEC. 5		N 1.0 ENE 2.0	N I	S NNW	1.0	E 1.6	BAE 2.0	E. 2	8 E	4.1	200 3.3	wer.	ver 3.	ESE 3.	ESP C	1 2
\$ 5.0, \$ \$86. 0.4 \$WN 0.4 \$ \$W1.0; \$WX 0.6 \$WX 0.2, \$WX 0.6 \$WX 0.6 \$W 0.5 \$W 0.6 \$W 0		N 1.0 ENE 2.0 ESE 2.0	N I	5 ENF	2.1	E 1.6	E 2.4	ESE 1.		4.0 1	58B 3.0	ESE 4.3	ESE 3.1		ESE 2.8	2
W 50 NW 4-0 W 4-2 SW 7-2 W 3-1 WW 3-0 WWW 3-5 SW 5-5 SW 2-0 SW 5-1 SK 2-0 SW 3-0 NW 3-1 WW 3-0 WW 3-5 WW 3-1 SW 3-		N 1.0 ENE 2.0 ESE 2.5 ESE 2.5	S o	5 NNW ENF	2.1	E 1.6 E 1.3 NNE 1.1	E 2.4 ENE 1.8	ESE 3.	o E	4.0 E	ESE 2.8	SE 2.1	ESE 1.1	SSE o.	ENE 2.8	2 2
30 3.5   S 4.0 S8W 5.5   S5W 3.0 M3W 4.4 M3W 5.0   W 5.3   W 6.4 M3W 7.0 M3W 5.6   W 5.2 M3W 3.0   W 1.5 M3W 1.6 M3W 7.0 M3W 7.7 M3W 7		ENE 0.2 S 0.6 N 1.0 ENE 2.0 ESE 2.5 ESE 2.5 ENE 0.5	S o N I E I ESE o ESE 3 NNE o	.5 ENF	2.1 2.6 0.0	E 1.6 E 1.3 NNE 1.1 0.0	ENE 1.8 S 0.5	ESE 3. ESE 3. SW 0.	o E 4 SSW	3.2 I	SW 1.3	SE 2.1. S 1.4	ESE 1.1 SE 1.1	SSE o.	ESE 2.8 ENE 2.4	2 0
Number   N		ENE 0.2 S 0.6 N 1.0 ENE 2.0 ESE 2.5 ENE 0.5 S 0.9 W 5.0	S o N I ESE o ESE 3 NNE o	5 NNW 5 ENF 6 E 1 E 3	1.0 2.1 2.6 0.0	E 1.6 E 1.3 NNE 1.1 0.0 SW 0.5 W 2.7	ENE 2.0 E 2.4 ENE 1.8 S 0.5 WNW 0.6	ESE 3. ESE 3. SW 0. WSW 2. WSW 1.	SSW SSW WSW	3.2 I 1.5 S	SW 3.0 SW 3.0 SW 2.5	SE 2.1 S 1.4 W 3.1 SSW 2.0	SE 1.4 SW 1.6 S 1.1	SSE 0.	SW 2.2 S 2.1	2 2 0 1
WSW 3.5 WSW 1.5 WSW 3.0 WSW 4.1 WSW 2.4 W 3.2 NNW 5.8 NNW 6.0 NNW 3.6 NW 1.2 WNW 0.8 NNW 1.7 3		ENE 0.2 S 0.6 N 1.0 ENE 2.0 ESE 2.5 ESE 2.5 ENE 0.5 S 0.9 W 5.0 S 3.5	S o N i ESE o ESE 3 NNE o	5 NNW 5 ENF 6 E 1 E 3	1.0 2.1 2.6 0.0 0.4 4.2	E 1.6 E 1.3 NNE 1.1 0.0 SW 0.5 W 2.7 SSW 1.0	ENE 2.0 E 2.4 ENE 1.8 S 0.5 WNW 0.6 W 3.1	ESE 3. ESE 3. SW 0. WSW 2. WSW 3. WNW 5.	SW SW SW WNW	3.2 I 1.5 S 3.0 W 2.5 W	SW 3.0 SW 3.0 SW 2.5 W 6.4	SE 2.1 S 1.4 W 3.1 SSW 2.0 WNW 7.9	SE 1.3 SE 1.3 SW 1.6 S 1.1 WAW 5.6	SSE 0.1	SW 2.2 S X 2.1 S X 2.1 S X 2.1	2 2 0 1 2
		ENE 0.2 S 0.6 N 1.0 ENE 2.0 ESE 2.5 ENE 0.5 S 0.9 W 5.0 S 3.5 NNW 1.6	S o N i E i ESE o ESE 3 NNE o SSE o WNW 4	.5 NNW .5 ENF .6 E .1 E .3 WSW .0 SSW	1.0 2.1 2.6 0.0 0.4 4.2 5-5	E 1.6 E 1.3 NNE 1.1 0.0 SW 0.5 W 2.7 SSW 3.0	EAE 2.0 E 2.4 ENE 1.8 S 0.5 WNW 0.6 W 3.1 WNW 4.0 SSE 1.2	ESE 3. ESE 3. SW 0. WSW 2. WSW 3. WNW 5.	SW S	3.0 W 2.5 W	SW 3.0 SW 3.0 SW 2.5 W 6.4 S 1.8	SE 2.1 S 1.4 W 3.1 SSW 2.0 WNW 7.0 SSW 2.7	SE 1.3 SE 1.3 SW 1.6 S 1.1 WNW 5.6	SSE 0.1	SW 2.2 S 2.1 WNW 3.0	2 2 0 1 2 4
2.12 (.88 (.53 (.35 1.78 2.49 2.91 3.09 2.83 2.10 1.90 1.85 2		ENE 0.2 S 0.6 N 1.0 ENE 2.0 ESE 2.5 ENE 0.5 S 0.9 W 5.0 S 3.5 NNW 1.6	S o N I ESE o ESE 3 NNE o SSE o WNW 4 WNW 3	.5 NNW .5 ENF .6 E .1 E .3 WSW .0 SSW .0 SSW	1.0 2.1 2.6 0.0 0.4 4.2 5.5 1.0	E 1.6 E 1.3 NNR 1.1 0.0 SW 0.5 W 2.7 SSW 3.0 SSE 0.5 SSW 1.0	EAE 2.0 E 2.4 ENE 1.8 S 0.5 WNW 0.6 W 3.1 WNW 4.0 SSE 1.5 SW 2.0	E 2. ESE 3. ESE 3. SW 0. WSW 2. WSW 3. WNW 3. SSW 1. SSW 1.	5 WSW 6 SSW 6 WSW	4.0 II 3.2 II 1.5 S 3.0 W 2.5 W	SW 3.0 SW 1.3 SW 2.5 W 6.4 S 1.8	SE 2.1 S 1.4 W 3.1 SSW 2.0 WNW 7.0 SSW 2.7 SW 1.2	SE 1.4 SE 1.4 SW 1.6 S 1.1 WNW 5.6 S 1.5	SSE 2.	SW 2.2 S 2.1 WNW 3.0 S 2.7 SSW 3.6	2 2 0 1 2 4 1

APRIL

PPH		loor.

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2	48.9 35.8		44.7	39.3		44.30	5.7		11.1	10.4	8.33
3	35.8		40.3			40.97	4.1		6.9	6.4	5.03
5	49.2 38.5	1	47.5	33-3		46.93 35.90	6.1		8.3	8,2	5.43
6	31.3		34.0	36.4		33.90			3.1	1.6	2.40
7 8	41.6		40.7	36.5		40.27	- 1. i	Y	4.4	2.6	1.97
8	35.0	j	41.6	43.8		40.13	- 0.4		6.9	0.2	3,40
10	45.5 38.2		36.6	39.5		36.47	4.4		14.6	10.7	9.90
11	34.0		33-3	33.5		33.60	7.5		14.0	11.1	10.87
12	36.4			41.6		38.87	9.1		11.6	11.8	10.87
13	45.0 46.6		46.0	46.5		45.30	8.3		7.7	5.8	6.23
15	43-3		42.0	41.9		42.40	2.2		12.9	5-1 7-7	7.60
16	41.6		41.2	41.8		41.53	4.5		7.9	5 - 7	6.03
17	41.6 39.1		40.5	38.3		41.07 38.43	3.3		2.7	5.5	2.33
19	38.2		39.6	41.4	1	39.73	3.6		5.7	5.1	4.50
20	41.6		40.3	38.4	. [	40.10	3.8		7.9		6,60
21	33.2		30.2	33.6		32.33	7.6		8.2	6.3	7-37
22	36.5 42.3		37.8	41.3		38.53	5.5		8.3	5.0	6.37
24	41.2		40.5	41.5		41.07	5.2		7.9	5.2	6,10
25	40.1		47.0	47.9		47.00	4-4		9.0	7.0	6,80
26	48.3		45-5	45.2 45.7		46.33	7-4		13.0	8.6	9.70
28	44.6		40.5	41.9	1	43.03	7.9	1	16,6	13.0	12.50
30	42.3		42.5	41,0		42.10	13.2		18.5	14.6	14.83
-	40.7		42.49	43.2		42.17	13.2				14.43
littel	41.49	'	41.11	41.2	7	41.29	4.9	3	9.69	7.06	7.22
Tag	Dun	stdruck	in Millim	etern	R	telative Fer	chtig	ceit	Richtung	u. Stärke d [Skala: o - 10	les Wind
ag	19 <sup>b</sup>	2 <sup>t<sub>1</sub></sup>	94	Tages- mittel	19 <sup>h</sup>	34	9 <sup>h</sup>	Tages- mittel	19h	34	9h
	4.3	3.4	4.2	4.0	63	34	56	51	NW 3	WSW 2	w
	4.5	4.7	5.1	4.6	77 69	42	54 72	58 65	N 2	NW 2 W 4	W
2			4.5	4.0	73	55 46	62	60	Wı	NW I	S
		3.7		5.9	69	69		72	SSW 3	WSW 2	WSW
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3 4 5 6	3-7 4.8 5-1	3.6	3.3	4.0	93	62	64	73	W 2	W 4	W
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2 3 4 5 6 7 8 9 10	3-7 4.8 5.1 3-7 3-5 3-9 4-3 6.4 7-5 6.4	3.6 2.7 4.8 2.5 5.4 7.4 9.4 5.9	3.3 3.6 3.5 3.8 6.0 8.0 8.6 5.1	3.3 3.9 3.4 5.2 7.3 5.5	88 78 56 68 83 85 75	62 43 87 38 44 62 94 53	64 65 74 63 63 81	65 80 61 58 75 89 69	W 2 W 3 XW 3 SSW 1 SSW 1	W 5 NNW 4 SW 2 SSW 1 0 NNW 1 NE 3	SSW
2 3 4 5 6 7 8 9 10	3-7 4.8 5-1 3-7 3-5 3-9 4-3 6-4 7-5 6-4 5-4	3.6 2.7 4.8 2.5 5.4 7.4 9.4 5.9	3.3 3.6 3.5 3.8 6.0 8.0 8.6 5.1	3.3 3.9 3.4 5.2 7.3 8.5 3.8	88 78 58 68 83 85 78 78	62 43 87 38 44 62 94 53 62	64 65 74 63 63 81 84 75	65 80 61 58 75 89 69	W 2 W 3 NW 3 SSW 1 SSW 1	NNW 4 SW 2 SSW 1 0 NNW 1 NE 3 NE 1	SSW
2 3 4 5 6 7 8 9 10 11 12 13 14 15	3-7 4.8 5-1 3-7 3-5 3-9 4-3 6.4 7-5 6.4 5-4	3.6 2.7 4.8 2.5 5.4 7.4 9.4 5.9 4.9 5.6	3.3 3.6 3.5 3.8 6.0 8.0 8.6 5.1 5.2	3.3 3.9 3.4 5.2 7.3 8.5 3.8 3.2 5.3	88 78 58 68 83 85 78 78 94	62 43 87 38 44 62 94 53 62 51	64 65 74 63 63 81 84 75 80 68	65 80 61 58 75 89 69 73 71	W 2 W 3 XW 3 SSW 1 SSW 1 S 1 o NNE 1 E 2 X 1	W 5 NNW 4 SW 2 SSW 1 0 NNW 1 NE 3 NE 1 ESE 2	SSW NE ENE SE
3 4 5 6 7 8 9 10 11 12 13 14 15 16 17	3-7 4.8 5.1 3-7 3-5 3-9 4-3 6.4 7-5 6.4 5.1	3.6 2.7 4.8 2.3 5.4 7.4 9.4 5.9 4.9 5.6 3.6	3.3 3.6 3.5 3.8 6.0 8.0 8.6 5.1 5.2 5.3	3.3 3.9 3.4 5.2 7.3 8.5 5.8 5.2 5.3	88 78 58 68 83 85 78 78 94	62 43 87 38 44 62 94 53 62 51 45	64 65 74 63 63 81 84 75 80 68	65 80 61 58 75 89 69 73 71	W 2 W 3 NW 3 SSW 1 SSW 1 S 1 o NNE 1 E 2 N 1	NW 5 NW 2 SSW 2 SSW 1 0 NNE 1 ESE 2 E 3 NE 1	W W SSW  NE ENE SE NE
3 4 5 6 7 7 8 9 10 11 12 13 14 15 16 17 18	3.7 4.8 5.1 3.7 3.5 3.9 4.3 6.4 7.5 6.4 5.4 5.1	3.6 2.7 4.8 2.3 5.4 7.4 9.4 5.9 4.9 5.6 3.6	3.3 3.6 3.5 3.8 6.0 8.6 5.1 5.2 5.3 4.0	3.3 3.9 3.4 5.2 7.3 8.5 3.8 5.2 5.3 3.9 5.2	88 78 58 68 83 85 78 78 94 65 65	62 43 87 333 44 62 94 53 62 51 45 44	64 65 74 63 63 81 84 75 80 68 58	65 80 61 58 75 89 69 73 71	W 2 W 3 NW 3 SSW 1 SSW 1 S 1 o NNE 1 E 2 N 1 E 2 N 1	W 5 NNW 4 SW 2 SSW 1 0 NNW 1 NE 3 NE 1 ESE 2 E 3 NE 2 NNW 1	SSW SSW NE ENE SE NE NE WNW
3 4 5 6 7 8 9 10 11 12 13 14 15 16 17	3.7 4.8 5.1 3.7 3.5 3.9 4.3 6.4 7.5 6.4 5.1 4.1 3.9 4.9	3.6 2.7 4.8 2.3 5.4 7.4 9.4 5.9 4.9 5.6 3.6	3.3 3.6 3.5 3.8 6.0 8.0 8.6 5.1 5.2 5.3	3.3 3.9 3.4 5.2 7.3 8.5 3.8 3.9 3.9 3.9 5.6	88 78 58 68 83 88 78 78 94 65 68 91	62 43 87 33 44 62 94 53 62 51 45 44 98	64 65 74 63 63 81 84 75 80 68 58 62 96 85	65 80 61 58 75 89 69 73 71 56 58	W 2 W 3 NW 3 SSW 1 SSW 1 S 1 o NNE 1 E 2 N 1	NW 5 NW 2 SSW 2 SSW 1 0 NNE 1 ESE 2 E 3 NE 1	W W SSW  NE ENE SE NE
3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19	3.7 4.8 5.1 3.7 3.5 3.9 4.3 6.4 7.5 6.4 5.4 5.1	3.6 2.7 4.8 2.3 5.4 7.4 9.4 5.9 4.9 5.6 3.6 3.5 5.8	3.3 3.6 3.5 3.6 8.0 8.0 8.6 5.1 5.2 5.3 4.0 4.2 5.5 6.1	3.3 3.9 3.4 5.2 7.3 5.5 5.5 3.9 5.2 5.3 3.9 5.2 5.3	88 78 58 68 83 85 78 78 94 65 65	62 43 87 333 44 62 94 53 62 51 45 44	64 65 74 63 63 81 84 75 80 68 58 62 96 85	65 80 61 58 75 89 69 73 71 56 58 95 88	W 2 W 3 XW 3 S5W 1 SW 1 SW 1 0 NNE 1 E 2 X 1 E 1 X 1 NW 6	W 5 NNW 5 NNW 2 SSW 1 NE 3 NE 3 NE 2 E 3 NE 2 NNW 1 NNW 3 NE 2 NNW 3	NE ENE NE WNW N E NXW
2 3 4 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 20 20 21 22 22	3.7 4.8 5.1 3.7 3.5 3.9 4.3 6.4 5.4 5.4 5.4 5.4 5.5 5.0 6.4	3.6 2.7 4.8 2.5 5.4 7.4 9.4 9.5 5.6 3.6 3.5 5.8 6.1 8.0	3.3 3.6 3.5 6.0 8.0 8.6 5.1 5.2 5.3 4.0 4.2 5.5 6.1	3.3 3.9 3.4 5.2 7.3 8.5 5.2 5.3 3.9 5.2 5.6 5.7 6.5	88 78 56 68 83 85 78 78 94 65 68 91 83 82 74	62 43 87 33 44 62 94 53 62 91 45 44 98 85 76	64 65 74 63 63 63 84 75 80 68 58 62 96 85 75	65 80 61 58 75 89 69 73 71 56 58 78 85 78	W 2 W 3 NW 3 SSW 1 SSW 1 S 1 0 NNE 1 E 2 E 1 NW 1 SE 1	W 5 NNW 4 SW 2 SSW 1 NNW 1 NE 3 NE 1 ESE 2 NSW 1 NSW 1 NSW 3 NE 2 NSW 3 NE 2 NW 3	SSW NE ENE SE NE NE WNW N E E NNW N N W
2 3 4 5 6 7 7 8 9 10 11 12 13 14 15 16 17 18 19 19 19 20 21 22 23	3.7 4.8 3.7 3.5 3.9 4.3 6.4 5.4 5.1 4.1 3.9 4.9 5.5 6.4 4.9	3.6 2.7 4.8 2.5 5.4 7.4 9.4.9 5.9 4.9 5.5 5.5 5.5 5.5 8.0 4.1	3,3 3,6 3,8 6,0 8,6 5,1 5,2 5,3 4,0 4,2 5,5 5,1 5,2 5,3 4,0 4,2 5,5 6,1	3.3 3.9 3.4 5.2 7.3 5.5 5.2 5.3 3.9 5.2 5.2 5.2 5.2	88 78 88 68 83 88 78 78 94 65 68 93 83 82 74	62 43 87 333 44 62 94 53 62 51 45 44 95 85 76 99 50 46	64 65 74 63 63 81 84 75 80 68 58 62 96 75 75	65 80 61 58 75 69 73 71 56 58 95 78 85 65 78	W 2 W 3 NW 3 S5W 1 SSW 1	W 5 NNW 4 2 SSW 2 SSW 1 0 NNW 1 NE 3 NE 2 ES 2 ES 3 NE 2 NNW 1 NNW 3 NE 2 NNW 3 NNW 3 NNW 3 NNW 3 NNW 3 NNW 4	NE ENE NE WNW N E NXW
2 3 4 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 20 20 21 22 22	3.7 4.8 5.1 3.7 3.5 3.9 4.3 6.4 5.4 5.4 5.4 5.4 5.5 5.0 6.4	3.6 2.7 4.8 2.5 5.4 7.4 9.4 9.5 5.6 3.6 3.5 5.8 0.1	3.3 3.6 3.5 6.0 8.0 8.6 5.1 5.2 5.3 4.0 4.2 5.5 6.1	3.3 3.9 3.4 5.2 7.3 8.5 5.2 5.3 3.9 5.2 5.6 5.7 6.5	88 78 56 68 83 85 78 78 94 65 68 91 83 82 74	62 43 87 33 44 62 94 53 62 91 45 44 98 85 76	64 65 74 63 63 63 84 75 80 68 58 62 96 85 75	65 80 61 58 75 89 69 73 71 56 58 78 85 78	W 2 W 3 XW 3 S5W 1 SSW 1	W 5 NNW 4 SW 2 SSW 1 NNW 1 NE 3 NE 1 ESE 2 NSW 1 NSW 1 NSW 3 NE 2 NSW 3 NE 2 NW 3	NE SSE NE
2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 26 26 27 28 29 29 20 20 20 20 20 20 20 20 20 20 20 20 20	3.7 4.8 5.1 3.7 3.9 4.3 6.4 7.5 6.4 5.1 3.9 4.3 5.1 5.0 4.9 4.0 4.0 4.0 4.0 4.0 4.0 4.0 4.0 4.0 4.0	3.6 2.7 4.8 5.4 7.4 5.9 4.9 5.6 3.6 3.5 5.5 8.0 4.1 8.0 4.7	3,3 3,6 3,6 6,0 8,6 5,1 5,2 4,7 5,3 4,7 5,3 4,7 5,3 4,7	3.3 3.9 3.4 5.2 7.3 5.5 5.2 5.3 3.9 3.9 5.6 5.7 6.5 7	88 78 68 83 88 78 94 65 68 91 93 82 74 67 79 72	62 43 33 44 44 62 94 53 52 51 45 44 98 85 76 99 50 46	64 65 74 63 63 81 84 75 86 62 96 85 75 74 72 80 80 81 81 81 81 81 81 81 81 81 81 81 81 81	65 86 61 58 75 69 73 71 56 58 78 85 65 57 72 62	W 2 W 3 XW 3 SSW 1 SSW 1 S 1 NNE 1 E 2 E 1 NW 6 SE 1 NW 6 SE 1 NW 2 SW 2 SW 2 SW 2	W 5 NNW 4 SW 2 SSW 1 NNW 3 NE 1 ESE 2 NNW 1 NNW 3 NE 2 NNW 3 NE 2 NW 3 WNW 4 SW 3 W 3 W 1	W W SSW SSW SSW SSW SSW SSW SSW SSW SSW
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2 3 4 5 6 7 8 9 10 11 2 13 14 15 17 8 19 20 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	3.7 4.8 5.1 3.7 3.9 4.3 6.4 7.5 6.4 5.4 5.1 3.9 4.3 5.5 5.0 6.4 5.0 4.0 4.0 4.0 4.0 4.0 4.0 4.0 4.0 4.0 4	3.6 2.7 4.8 5.4 5.4 5.9 5.6 3.5 5.5 8.0 4.1 8.0 4.7 4.9 3.7 4.9 3.7 4.9 3.7 4.9 3.7 4.9 5.6 6.1	3,3 3,6 3,6 6,0 8,6 5,1 5,2 4,7 5,3 4,7 5,3 4,7 5,3 4,7	3.3 3.4 5.2 7.3 5.5 5.5 5.2 5.3 3.9 5.7 6.5 5.7 6.0 4.0 4.0 4.4 5.4 6.0 6.9	88 788 68 83 83 78 78 94 65 94 65 77 77 77 77 77 78	62 43 33 44 62 94 53 62 51 45 44 95 85 76 99 50 46 61 41	64 65 74 63 63 81 84 75 86 62 96 85 75 74 72 80 80 81 81 81 81 81 81 81 81 81 81 81 81 81	65 86 61 58 75 69 73 71 56 58 78 85 65 57 72 62	W 23	W 5 SW 2 SSW 1 SW 2 SSW 1 SE 2 SSW 1 SE 2 SSW 1 SE 2 SSW 3 SE 2 SSW 3 SE 2 SSW 3 SW 3 SW 3 SW 3 SW 3 SW 3 SW 3 S	W W W SSW
2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 19 21 22 23 42 5 26 7 7 8	3.7 4.8 5.1 3.7 3.5 4.3 6.4 7.5 6.4 5.1 4.1 5.1 4.9 4.9 5.0 4.9 5.0 4.9	3.6 2.7 4.8 5.4 7.4 5.9 4.9 5.6 3.6 3.5 5.5 8.0 4.1 8.0 4.7	3.3 3.6 3.8 6.0 8.6 5.1 5.2 4.2 5.3 4.0 4.7 4.3 5.5 6.7 6.3 8.0	3.3 3.9 3.4 5.2 7.3 5.5 5.2 5.3 3.9 5.2 5.6 5.7 6.5 7.4 4.0	88 788 68 83 88 78 78 65 94 65 93 83 77 77 77 77 72 83	62 43 33 34 62 94 53 62 51 45 44 98 85 76 99 50 46 61 41	64 65 74 63 63 81 84 75 80 68 58 62 85 75 74 72 80 81 72	65 80 61 58 75 89 69 73 71 56 55 55 78 85 65 77 72 62 65 66 66	W 2	W 5 NNW 4 SW 2 SSW 1 NNW 3 NE 1 ESE 2 NNW 1 NNW 3 NE 2 NNW 3 W 3 W 3 W 3 W 3 W 3 W 1 NNE 1 S 2 S 2 S 2 S 2 S 3 S 3 S 3 S 3 S 3 S 3	W W W SSW  NE ENE SE NE WNW NE SW WSW WSW WSW WSW SSW

Tag	Bewo	lkung [Skala: e und Woff	heiter, to trūb]	Nieder- schlag in	Bemerkungen
	10,	24	9ª Tagesmitte	Milli- metern	
1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25	FIIS 3 W FS 10 HS 10 HS 10 W HS 10 W HS 2 NW FS 10 HS 10 W HS 2 NW HS 10 NE FS 2 HS 10 NE FS 3 0 HS 10 NE FS 3 0 HS 10 NE FS 10 HS 10	HS 10 W HS 10 W H 10 NW H 1 1 W HS 10 W	Fill 5   6.0	1.7 9.1  2.7 0.9 2.1  1.3  0.8 13.0 0.2  4.3 	Abends =  Abends =  Morgens =  **If u 2* ** Tropfen, 0** ** ** ** ** ** ** ** ** ** ** ** **
26 27 28 29 30	FHS 10 W HS 10 HS 10 HS 9 HS 10 SW	FHS 9 W FHS 6 FHS 10 W HS 10 H 4 SW	HS 10 W 0.7 FS 2 6.0 FS 3 7.7 FHS 10 9.7 HS 2 5.3	0.3    0.1	Morgens = 0. 9 <sup>h</sup> ⊕ Tropfen. nachts ⊕. Abends = 1. 9 <sup>h</sup> ⊕ 2. Morgens und abends = 1. Morgens und abends = 1. 0 <sup>h</sup> ⊕ Tropfen. Morgens = 1.0 <sup>h</sup> − 21 <sup>h</sup> ⊕ 2.
littel	8.2	8.3	7.7 8.1	S 27.4	

Tag	12h	144	16h	181	20%	22h	O/r	24	45	6h	Sh	104	Tages- mittel	Max	Min
	47.4	48,2	48.5	49.2	50.0	50.3	49.9	49.3	49.2	49.7	50.4	50.7	49,40	50.7	47-4
2	\$0.6	50.1	49.9	49.3	48.7	48.1	46.5	44.7	42.7	41.3	39.8	38.6	45.86	\$0,6	30.0
3	16.6	34.5	35.7	35.7	35.8	16.0	38.8	40.3	42.2	41.8	46.2	47.4	39.49	48.1	34.5
4	48.1	45.3	48.2	48.7	49.6	49.5	48.6	47.5	46.4	45.4	44.7	43.7	47.39	49.7	42.0
5	42,6	41.4	19.9	18.8	18.4	37.9	37.0	35.9	34-4	33.6	33.4	32.8	37.18	42.6	32.1
6				-											
	32.1	31.0	30.7	30.7	31.4	33.0	33.5	34.0	34.7	35.2	36.1	37-9	33.36	40.5	30.
7	40.5	41.6	42.5	43-3	43.7	43.3	42.2	40.7	39.6	38.8	37 . 1	35.6	40.74	43.7	33-
	33.5	31.7	31.1	33.0	36.1	38.6	40.6	41.6	42.2	42.6	43.6	44.0	35.22	44.6	31.1
9	44.6	44.6	44-7	45.3	45.5	44.9	43.8	42.6	41.2	40.3	39.8	30.3	43.05	45.5	39.0
10	39.0	38.6	38.3	38.1	38.2	37.9	37 - 4	36.6	35.3	34.5	34.6	34-3	36.90	39.0	34.1
11	34.4	34.0	33-7	33.8	34.1	33.7	33-5	33.3	32.8	32.8	33.2	33.7	33.56	34.1	32.5
12	34.1	34.5	35.0	35.7	36.8	37.3	38.0	38.6	38.9	40.0	41.2	41.9	37.67 €	42.9	34.1
13	42.9	43.5	43.9	44.6	45.4	45.5	45.0	44.4	44.5	45.0	45.9	46.7	44.78	46.9	47.9
14	46.9	46.9	46.7	46.6	46.5	46.6	46.5	46.0	45.4	45.0	45.0	44.8	10.05	46.9	44.
15	44.5	43-7	43-4	43.2	43.4	43.0	42.8	42.0	41.2	41.0	41.2	42.1	42.63	44.5	41.9
16	41.0	41.7	41.4	41.6	41.7	41.7	41.6	41.2	41.0	41.2	41.5	42.0	41.54	42.0	41.5
17	41.8	41.4	41.5	41.3	41.7	41.3	40.0	40.5	40.4	40.5	41.0	41.1	41.13	41,8	40.4
18	40.8	39.9	39.4	19.0	38.6	18.4	35.0	37.9	17.8	17.9	35.2	38.3	38.68	40.8	37.8
19	38.3	37.9	37.9	37.9	38.4	38.8	39.2	19.6	40.1	40.6	44.4	41.4	39.27	41.8	37.5
30	41.8	41.5	41 -3	41.5	41.5	41.5	41.3	40.3	***			37.9	***	41.8	36.
21	36.3	34.6	34.0	33.5	32.8	11.9	31-3	10.2	31.2	12.2	33.1	31.6	32,88	36.3	30.3
22	34.5	35.4	35.6	36.0	***	***	3	17.8	38.9	19.6	49.8	41.6		42.1	34.5
23	42.1	42.3	42.1	42.2	42.2	42.1	41.5	41.2	41.0	41.2	41.6	41.6	41.76	42.3	41.0
24	41.8	41.5	41.3	41.2	41.0	41.2	40.9	40.5	40,2	40.5	41.2	41.6	41.08	42.5	40.3
25	42.5	43.3	44 4	45-4	46.3	47.2	47.0	47.0	47.3	47.3	47.7	45.2	46.13	45.3	42.5
26	48.3	48.3	48.2	48.3	48.2	47.6	46.7	45.5	44.9	44.6	44.9	45.5	16.75	48.3	44.6
27	45.4	45.4	45.6	46.2	46.9	47.3	47.0	46.5	46.0	45.6	45.8	45.6	46.11	47.3	45.4
28	45.4	45.0	44.6	44.5	44.6	44.3	43.8	42.6	41.0	41.7	41.7	41.9	43.50	45.4	41.7
29	42.1	42.1	41.9	42.1	42.2	42.6	42.6	42.5	41.9	41.7	41.6	41.6	42.08	42.6	41.0
30	41.0	40.1	39.9	40.1	41.2	42.0	42.5	42.6	42.2	42.3	43.0	43.5	41.70	44.0	39.7
littel	41.619	11.29	41.23	41.41	41.76	41.50	41.68	41.26	40.95	40.94	41.24	41.41	41,39	43.92	38.1

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1 2 3 4	7.4 5.8 9.3 3.4	6.3 4.7 5.7 2.6	6.0 3.8 4.2 2.0	3.9	.5 9.0 .8 7.8 .9 5.0	9.9 10.3 6.1 7.1	15.0 15.1 6.9 8.3	10.7 11.0 5.5 9.4	8.7 10.4 5.1 8.9	7.2 9.7 4.3 6.8	6.6 9.6 3.8 5.7	7.87 7.69 5.31 5.38	11.1 11.2 9.4 9.5	5.1 3.3 3.4
5 6 7 8 9	7.7 - 1.2 1.5	4.8 - 7.3 - 1.3 0.8 - 1.3	4.7 - 5.8 - 1.5 - 1.0	1.4	.8 9.4 .3 4.0 0.2 2.4 1.2 0.2 1.4 3.4	10.9 4.8 3.6 1.3 5.6	3.1 4.4 2.4	2.9 4.1 2.4 6.8	10.1 2.2 3.2 1.7 6.4	8.5 1.1 2.7 0.7 4.6	7.9 0.9 2.0 - 0.2 3.7	8.07 3.71 1.37 0.98 2.73	7.7 4.6 2.4 6.0	- 1. - 1. - 0.
10	3.6 9.2 10.3	8.5 9.2	4.1 7.9 8.4 8.5	3.9 3 7.5 7 8.8 10	.5 8.9 .9 10.4 .9 13.2	12.6 11.6 14.0	14.6 14.0 11.6	15.4 14.1 13.8	15.2 13.3 13.2	11.5 11.9 12.2	10.5	9.16 10.58 11.42	16.1 14.1 14.7	3 · 7 · 8 ·
3 4 5 6	10.8 5.4 3.8 6.6	9.5 5.5 3.5 6.2	5.4 3.4 5.6	5.6 6 2.4 3 4.5 5	.7 10.1 .2 6.9 .8 8.8	7-8 18-2 7-5 6,8	7.7 12.9 7.9	11.4 7.8 13.4 8.2	9.7 7.5 12.3 7.8	6.9 6.3 9.1 6.6	5.4 4.5 7.1	9.54 6.32 7.64 6.43	13.0 8,0 13.5 8.2	3.
7 8 9	5.1 4.3 2.8 5.0	4.5 3.5 3.4 4.8	4.2 3.0 3.2 4.7	2.5 3.6 3.8 3.8	.8 6.1 .9 2.2 .8 4.5 .8 4.8	2.5 5.6 6.4	8.0 2.7 5-7 7-9	7.4 3.2 6.2 8.4	6.9 3.2 5.9 8.4	5-9 1-7 5-4 8-0	5.3 2.1 5.1 7.7	5.56 2.73 4.58 6.14	8.0 4.3 6.2 8.5	2.
3 4 5	7.4 6.1 4.5 5.3 4.3	7.0 5.8 3.5 4.7 4.1	7.0 5.5 3.5 4.3 3.9	5.3 5 3.0 4 4.3 6	.0 9.3 .9 6.8 .7 6.4 .2 7.9	9.8 8.2 8.4 7-5 8.2	8.2 8.6 8.3 7-9	6.5 7.0 9.5 8.4 9.3	6.4 6.4 8.3 7.4 8.7	6.4 5.2 6.7 6.0 7.5	6.4 4.8 5.8 4.6 6.4	7.47 6.30 6.05 6.21 6.32	9.1 9.6 9.6 9.6	6. 4. 3. 4.
6 7 8 9	5.6 7.8 7.8 10.9	5.1 7.6 7.2	4.5 7.0 6.8 9.7	4.6 6 6.5 8 7.4 8 9.6 12	.2 10.5 .0 10.2 .5 12.7 .1 10.0	11.8 11.6 14.4 17.7	13.0 12.5 16.6 18.5	12.7 12.7 16.9 19.3	11.4 11.3 16.0	9.1 10.1 13.8 15.6	8.3 8.6 12.7	8.57 9.58 11.73 14.32	13.0 13.0 17.1 19.3	4. 6. 6. 9.
M.	5.94	5-33	4.90	4.53 5	.68 7.58	8.98	9.69	9.79	9.01	7-52	6.64	7.14	18.1	3
			Richte	ng (R), G	eschwine	ligkeit	G) des W	indes	in s Se	kunde	in Meters			T
g	12h R G	14 <sup>3</sup>	164	181	20 <sup>h</sup>	ligkeit (	oh	24		4 <sup>b</sup>	in Metern	8 g	R G	mi
Company of Street	WNW 3.0 W 2.0 SW 3.5 NNW 4.6	NW 1 SSW 1 WSW 5 NW 1	3 W 4	18° R (	20 <sup>h</sup> R G R G NW W 4,1 NW 0,1	R G W 5. SW 3. W 7. NSW 1.	6 WNW 4.	B WNW	G A	W 4.5 W 4.0 W 6.0 E 0.0	H G W 4.4 W 3.0 WNW 4.8 SE 2.0	8 G WSW 2.2 SSW 2.6 WNW 4.6 SSE 0.4	R G WSW 1. NW 2, SSW 1.	o 3
- The second sec	R (4 WNW 3.0 W 2.0 SW 3.5 NNW 4.5 SSW 2.1 WSW 3.1 X 6.0 SW 3.0 SW 3.0 SW 2.2	NW 1 SSW 1 WSW 5 NW 1 SSW 4 NNW 3 SSW 1 WSW 2	3 W 4 S 2 S NW 1 S 2 S NW 3 S NW 3 S NW 3 S NW 2 S NW 3 S NW 3 S NW 2 S NW 3 S NW 2 S NW 3 S NW 2 S NW 3 S	18° R (  14 WNW 5 3 SSW 2 4 W 4 6 NW 6 8 SSW 4 5 WNW 4 5 WNW 4 5 WNW 4 6 N 3 6 SW 2	20% R G 1 WNW 4.4 0 S 3.4 0 W 6. 7 NW 6. 0 WSW 3.5 8 WNW 5.6 6 AW 4.5 5 N 3.5 5 N 3.5	22h R G SW 5. SW 7. NNW 1. SWSW 4. SWNW 7. NW 5. NW 5. WSW 3.	6 WNW 4. 6 WNW 7. 1 SSW 1. 5 WNW 4. 1 WNW 8. 1 NW 7. 4 NW 7. 4 NW 8.	5 WNW 6 W 3 WNW 4 WSW 1 WNW 0 WNW 9 WNW 2 SSW	G A 4.0 4.0 6.5 WN 1.4 SS 4.8 WN 7.0 WN 6.9 WN 4.7 WN	4 <sup>h</sup> 4.5 W 4.5 W 6.0 E 6.0 W 5.6 W 8.0 W 6.5 W 4.8	W 4.4 W 3.6 WNW 4.8 SE 2.0 WSW 3.5 WNW 6.8 WNW 3.2 NW 2.0 SSW 2.8	8 G WSW 2.5 SSW 2.6 WNW 4.6 SSE 0.4 WSW 3.7 WNW 7.5 WSW 3.0 WNW 2.0 WNW 1.9	R G WSW 1. NW 2. SSW 1. WSW 3. NNW 6. SW 2. W 2. SSW 2.	0 3 7 2 8 5 5 1 4 0 6 9 4 8 3
The second secon	R (4 WNW 3.0 SW 3.5 NNW 4.5 SSW 2.1 WSW 3.1 SSW 3.0 SW 2.2 S 2.1 ESE 1.0 WNW 0.4 NNW 0.7 NNW 2.0	R 6 NW 1 SSW 1 SSW 5 NW 1 SSW 4 W 4 NNW 3 SSW 1 WSW 2 SW 2 NE 0. SSW 0. NNW 1 NNE 1	3 W 4 A C C C C C C C C C C C C C C C C C C	7 R (WNW 5 S S W 2 A S W 2 A S W 2 A S W 3 W 3 W 3 W 3 W 3 W 3 W 3 W 4 A S W 3 W 4 A S W 3 W 4 A S W 3 W 4 A S W 5 W 4 A S W 5 W 5 W 4 A S W 5 W 5 W 5 W 5 W 5 W 5 W 5 W 5 W 5 W	20° R G R G NWW 4.1 0 W 6. 7 NW 0.0 0 W 8W 3. 8 WNW 5. 66 NW 4. 5 SW 3. 5 SW 3. 5 WSW 1.2 3 NNE 1.2 3 NNE 1.2 5 SE 1.6	228 R G W 5.5 S W 7.5 N W 7.5 N W 5.5 N X 5.5 N X 6.5 WSW 3.6 S WSW 3.6 S WS	6 WNW 4. 6 WNW 7. 8 SWW 7. 8 SSW 4. 1 WNW 4. 1 WNW 8. 1 NW 7. 4 NNW 4. 2 WSW 3. 7 S 1. 5 ESE 1. 7 WNW 4.	2 R  5 WNW 6 WN 6 WN 6 WN 6 WN 7 ENE 5 NNW 7 ENE	G A 4.0 S 6.5 WN 1.4 SS 1.4 SS 4.8 WN 7.0 WN 6.9 WN 4.7 WN 3.7 SS 3.6 NN 3.6 NN 3.6 NN	4 <sup>h</sup> 4 G W 4.5 W 4.0 W 6.0 W 5.6 W 8.0 W 6.5 W 4.2 S 2.2 E 1.0 N 2.1 E 2.5	H G W 4.4 W 3.0 WNW 4.8 SE 2.0 WSW 3.5 WNW 6.8 WNW 3.2 NW 2.0 SSW 2.8 SSE 2.6 NNW 1.0 NN 1.2 ENE 3.5	8 G R G WSW 2.2 SSW 2.4 WNW 4.6 SSE 0.4 WSW 3.7 WNW 7.5 WNW 1.9 SSE 1.8 NNW 0.5 NNW 0.5 ENE 1.6 ENE 1.8	R G  W 3, WSW 1, NW 2, SSW 1, WSW 3, NNW 6, SW 2, SSW 1, S 0, NNW 0, NNW 0, NNE 2, EXE 2	0 3 2 3 3 5 5 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6
The state of the s	R G WNW 3.00 W 2.00 SW 3.5 NNW 4.5 SSW 2.1 WSW 3.1 X 50.0 SSW 3.0 SW 2.2 S 2.1 ESE 1.0 WNW 0.4 NNW 0.7 NNW 0.7 NNW 0.3 E 3.0 E	B 6 NW 1 SSW 1 SSW 1 WSW 5 NW 1 SSW 4 NNW 3 SSW 1 WSW 2 NE 0 SSW 0 NNW 1 NNE 1 0 E 3- E 2 N 1 N 1	3 W 4 1 S 2 S 2 S 3 S 4 S 5 S 8 W 2 S 5 W 3 S 4 S 6 S 8 W 2 S 6 S 8 W 2 S 6 S 8 W 2 S 6 S 8 W 3 S 6 S 8 W 3 S 8 W 3 S 8 W 4 S 6 S 8 W 5 S 8 W	183 8 W 1 W 1 W 1 W 1 W 1 W 1 W 1 W 1 W 1 W	7 R G R G R G R G R G R G R G R G R G R	228 R G 6 W 5 S W 3-5 S W 3-5 S W 3-5 S W 3-5 S W 3-7 S W 5	6 WNW 4. 6 WNW 4. 5 WNW 7. 5 WNW 4. 1 WNW 8. 1 NW 7. 4 NNW 4. 1 WNW 8. 7 S 1. 7 WNW 4. 6 SE 2. 6 E 5. 8 N 3. 9 N 3.	8	G A 4.0 S 4.0 S 6.5 WN 1.4 SS 4.8 WN 7.0 WN 4.7 WN 3.7 SS 2.9 I.6 N 3.6 NN 2.4 EN 3.3 ES 3.1 ES 3.1 ES	4 <sup>h</sup> (7) W 4.5 W 4.0 W 6.5 W 8.0 W 6.5 W 8.2 S 2.2 E 1.0 E 3.5 E 2.5 E 2	# G W 4.1 W 3.2 WNW 4.8 SE 2.0 WNW 3.2 NW 2.0 SSW 2.8 SSE 2.6 NNW 1.0 NN 2.0 NN	R G WSW 2.2 SSW 2.2 SSW 2.2 WNW 4.6 WSW 3.7 WSW 3.7 WSW 3.7 WSW 3.7 WSE 1.8 NNW 0.5 0.0 NE 3.3 ENE 1.5 ESE 3.1 E 4.5 E 3.4 NN 2.6 NN 2.6 N	R G W 3. WSW 1. NW 2. SSW 1. WSW 3. NNW 6. SW 2. W 2. SSW 1. S 0. NNW 0. NNW 0. NNW 0. NNE 2. ENE 1. ENE 3. E 4. NE 3. NNE 0.	m 3 3 2 2 3 3 3 2 2 3 3 3 2 2 7 3 3 3 2 2 7 3 3 3 2 2 7 3 3 3 3
The second secon	# # # # # # # # # # # # # # # # # # #	R (  NW 1  SSW 1  SSW 1  SSW 4  NW 1  SSW 4  NW 3  SSW 1  WSW 2  SW 2  SW 0  SSW 0  SS	3 W 4 A S O	180   180	1 WNW 4.4	228 R G G W 5.5 S W 5.5 S W 5.5 S W 5.5 S W 7.5 S W 7.5 S W 7.5 S W 5.5 S W 5.	R   G   WNW 4   WNW 4   WNW 4   WNW 4   WNW 4   WNW 4   ESE 2   ESE 1   WNW 8   ESE 1   WNW 8   WNW 4   WNW 5   WNW	8 R 5 WNW 6 WN 6 WNW 8 WNW 1 WNW 9 WNW 2 SSW 6 SSW 1 ENE 5 NNW 7 ENE 8 E 9 ENE 1 N 9 ENE 1 N 9 ENE 1 N 1 ENE 5 WNW 7 ENE 8 E 9 ENE 1 N 1 ENE 1 N 1 ENE 1 ENE 8 E 9 ENE 1 ENE 8 E 9 ENE 1 ENE 8 E 9 ENE 1 N 1 ENE 1 ENE 8 E 9 ENE 1 N 1 ENE 1 ENE 1 ENE 8 E 9 ENE 1	G A.0 S 6.5 WN 7.0 WN 7	4 <sup>b</sup> G  W 4.5  W 4.0  W 5.6  S 2.2  E 1.0  S 5 2.2  E 1.0  S 5 2.2  E 1.0  S 5 2.2  E 1.0  S 7 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8	# G  W 4.1  W 3.0  WN 4.8  SE 2.0  WN 5.2  WN 5.2  WN 5.2  SSW 2.8  SSE 3.6  NN 1.2  ENE 3.5  ENE 3.9  NN 2.5  ENE 3.9  NN 3.1  ENE 3.5  ENE 3.9  NN 3.1	R G WSW 2.: SSW 2.6 WNW 4.6 SSE 0.4 WSW 3.7 WSW 3.0 WNW 1.9 SSE 1.8 NNW 0.5 0.0 ESE 3.4 F 2.4 NSE 1.5 SE 1.5 NNE 3.3 ENE 1.5 NNE 3.3 ENE 1.5 NNE 3.4 NNE 3.4 NNE 3.4 NNE 3.5 WSW 3.7 NNE 3.3 NNE 3.4 NNE 3.4 NNE 3.5 NNE 3.4 NNE 3.5 NNE 3	R G  W 3 3 WSW 1-1 NW 2-2 SSW 1-1 WSW 3-1 NNW 6-1 SSW 1-2 SSW 1-1 SSW 2-2 SSW 1-1 SSW 2-2 SSW 1-1 SSW	07788551469833223333319333193331933
2345	# # # # # # # # # # # # # # # # # # #	R (  NW 1  SSW 1  SSW 5  NW 1  SSW 4  NNW 3  SSW 1  WSW 2  NE 0  NNW 1  NNE 0  E 3-  N 1  NNE 0  ENE 0  WNW 2  NNW 2  NNW 2	3	18   18   18   18   18   18   18   18	20   R   G   G	R   G   W   S   S   W   S   S   W   S   S   S	6 WNW 4 2 5 WNW 2 5 WNW 4 1 WNW 4 1 NW 4 1 WNW 5 1	R   2   N   W   W   W   W   W   W   W   W   W	4.0 S 4.0 S 6.5 WS 6.5 WS 6.9 WS	4 <sup>b</sup> 6 W 4.50 W 6.00 W 6.00 W 6.00 W 6.50 W 6.50 W 6.50 W 6.50 W 7.00 W 7.00	# G W 4.1 W 3.0 WNW 4.8 SE 2.0 WSW 3.5 WNW 3.5 WNW 3.5 SSW 2.8 SSE 3.6 NNW 1.0 NNW 1.0 ENE 3.5 E 5.5 E 3.5 E 5.5 E	8	R G  WW 3. WSW 1. NW 2. SSW 1. WSW 3. NNW 6. SW 2. SSW 1. SO. NNW 6. SW 2. SW 3. SW 3. SW 4. SW 5. SW 2.	0 3 2 2 3 3 3 2 2 3 3 3 3 3 3 3 3 3 3 3

	Luftdru	ck auf o' redu	ziert in Millim	. = 700°° +	1.	ufttemperat	tur nach Cel	sius
Tag	19b	26	94	Tagesmittel	190	2h	9h	Tageamitte
	45.8	44.8	1-10	44.67	13.3	22.1	17.3	1
2	45.3	41.6	43-4	44.67	13.3	23.5	17.3	17-57
3	47 - 5	48.3	49.6	45.47	12.5	14.4	12.0	17.77
3 1	50.8	48.8	48.5	49.37	9.4	18.7	14.4	14.17
3	47.7	47.2	47.8		13.0	17.2	14.8	15.00
				47-57				
6	47.0	46.1	46.4	46.50	14.6	23.3	17.6	18.50
7 8	45-5	44-5	44.5	44.93	17.0	25.1	18.4	20.17
	45.0	43.8	43.6	44.13	14.8	21.5	16.4	17-57
9	44.5	47.5	50.4	47-47	7.3	8.5	9-3	9.07
10	53.2	51.9	51.9	52.33	7.3	12.4	9.9	9.87
11	51.6	50.1	49.0	50.23	8.7	17.3	14.0	13.33
12	48.7	45.8	43.6	46.03	11.3	21.0	15.2	15.80
13	42.6	44.2	46.3	44-37	10.1	7.5	8.4	8.67
14	47.1	48.0	48.0	47-70	9.6	11.0	10.7	10.43
15	47.8	47.0	47.6	47 - 47	0.11	17.6	12.7	13.77
16	47.6	46.8	47.2	47.20	11.1	19.7	15.0	15.27
	47 - 4	47.2	46.6	47.07	12.3	15.2	14.5	15.07
17	46.2	44.2	44.2	44.87	11.8	21.0	16.7	16.80
19	44.0	42.8	40.9	42.57	13.0	17.7	15.0	15.23
20	38.5	37.1	35.9	37.17	14.1	14.9	14.0	14.33
21	36.2	16.6	37.2	36.67	11.8		12,2	12.53
22	37.6	37.4	37.7	37.57		13.6	10.9	10.13
23	39.7	40.6	41.1	49.47	7:3	8.9	8.1	8.19
24	40.6	41.5	43.3	41.80	8.1	12.0	9.8	9.97
25	45.5	46,1	47.2	46.27	9.4	13.7	11.8	11.63
26				1				
37	49.0	49.2	49.8	49.33	10.4	15.3	11.0	17.23
28	\$1.5	51.4	52.2	51.70	8.8	15.2	13.4	13-47
29	54.0	53-5	53.3	53.77	10.0	20.2	14.9	15.03
30	51.3	52.3	51.2 48.2	52.50	10.5	22.4	16.9	16.70
31	47.8	45.6	45.2	49.67	13.2	24.0		
3.	47.0	45.0	44.8	46.07	13.9	20.5	19.6	19.67
Mittel	46.40	45.85	46.01	46,00	11.26	17.40	13.86	14.17

Tag	Dun	stdruck	in Millim	etern	Re	lative F	euchtig	keit	Richt	ung	u. Stār Skala; o	ke de - 10]	s Wind	e
	19%	2 <sup>h</sup>	9 <sup>ts</sup>	Tages- mittel	19 <sup>h</sup>	2 <sup>h</sup>	9h	Tages- mittel	196		21		94	
	7.8	8.0	8.9	8.2	68	41	61		SE	. 1	S	.	SSW	
2	8.5	8.7	7.1	8.1	73	40		57	SE	:	SE	2	W	
3	6.9	8.1	6,9	7.3	64	66	53	55	W	:	SW	:	WXW	
4	6.8	7.2	8.5	7.5	78	45	70	64	NW	: 1	NNE	2	E	-
5	10.2	11.8	10.5	8.01	93	81	84	86	NE	2	ENE	2	ENE	
6	9.1	5.7	6.8	7.2	74	37	45	49	SE	2	ESE	4	ESE	
7 8	6.5	7.1	8.8	7.5	46	30	\$6	44	В	1	SSE	4	***	
	8.6	6.4	8.8	7.9	69	34	64	56	W.	2	S	2	NNW	
9	8.6	6.4	5.6	6.9	98	77	63	79	NW.	2	NW	2	W	- 1
10	6.4	3.7	5.1	5.1	85	34	56	58	NW	1	N		7.	-
11	5.9	7.2	8.6	7.2	70	60	73	64	S	,	WSW	2	SSW	
1.3	7.5	7.5	8.8	7.9	75	41	68	61	S	1	SE	1	NE	
13	6,8	7.3	6.9	7.0	74	94	84	84	N	3	NNW	2	N	3
14	6.7	7.0	7.6	7.1	75	71	79	75	N	1	NAW	1	NNW	:
15	7.0	5.1	6.9	6.3	71	34	63	56	NW	1	NE	3	ENE	
16.	6.7	7-4	7-4	7.2	68	43	58	56	E	2	ENE	2	E	
17	6.8	7.0	8.6	7.5	64	45	69	59	NE	1	ENE	4	E	:
	8,8	9.4	9.6	9.3	86	48	68	67	E	1	SE	2	511	- 1
19	9.2	9.9	10.4	9.8	83	66	82	77		0	NE	1	***	•
20	10.2	9.6	9.6	9.8	86	76	81	81	SSW	1	SW	2	W.	1
21	7.4	8.0	7.6	7.7	72	69	72	71	***	0	NNE	. 1	WSW	
22	5.6	6,6	4.9	5.7	72	64	51	62	NE	1	5	1	N	
23	5.5	4.9	5.2	5.2	72	58	64	65	N	2	NW	2	N	;
24	5.6	4.9	5.3	5.3	68	47	58	58	N	2	E	2	E	:
25	5.7	4.5	5.3	5.2	65	38	51	51	NNE	1	NE.	1	SE	
26	7.1	4.9	6,1	6.0	75	38	62	58	***	0	SE	1	E	
27	6.5	5.4	7.0	6.3	77	35	61	58	SW	1	5	1	***	- 6
28	6.7	5.5	8.3	6,8	73	31	66	57	SW	1	NE	1	444	•
29	7.4	6.0	8.9	7.4	76	30	63	56		0	ESE	1	***	
30	8.6	6.1	9.1	7-9	76		57	53	SW	1	ESE	2	***	
31	8.8	7.5	9.9	8.7	7.5	31	58	55	SSE	1	SE	1	***	
Mittel	7.4	6.9	7.7	7.3	7.4	49	65	63		1.1		1.8		

							2**	744							1903
Tag	1	ew öl	kung [	Skala: o	= heite	r, 10 ==	trāb]		Nieder- schlag in		F	eme	rkun	zen	
	198		21		9	ph.	Tages	mittel	Milli- metern						
1 2 3 4 5	FIIS 9 FIIS 8 IIS 10 FIIS 3 HS 10	11111	HS 1	3 8 9	FHS 1	2 0 8 0	4. 8. 9. 7.	3 3	0.9 11.9	Morge	ns mm, 6	achts 🖷	nisch, 6}h nit Unterb	nacht rechunger	ıs 🚳.
6 7 8 9	FHS 1 FS 6 FHS 8 HS 10 FH 4	  NW	FIIS 1 FII IIS 1	4 W	HS 1	4 ··· 6 ··· 2 ···	3 · 7 · 8 · 7 · 6 · 7	3 7 3	2.7 6.3	Morger		ig, mitta	gs zeitw.	stürmisch	-
11 12 13 14	HS to FHS to FHS to FHS to	 N	FIIS II IIS 1	8 NW 7 SE 0 NW 0 7 SE	FHS HS I	4 5 10 N	7- 5- 10-	3 7 0	6.2		ns ⇒,. tags un		ittags zei ittags reg		
16 17 18 19	FHS 9 FHS 7 E FHS 10 HS 10 FHS 9 E HS 8 SE HS 10 S 10 HS 10 W HS 10 FMS 9 HS 10 NW FMS 9 HS 8 W		FIIS 3 FIIS 5 NE FIIS 8 SE FIIS 10 FIIS 10 W		8.7 6.3 8.3 8.3 10.0		2.0	Morgens =, △, 19 <sup>h</sup> ⊕, 1½ <sup>h</sup> ⊕ Tropfen, Morgens und abends =, 1 <sup>h</sup> und 18½ <sup>h</sup> ⊕ Morgens =, 19 <sup>h</sup> ⊕, 0½ <sup>h</sup> [< u. ⊕, 8 <sup>h</sup> ⊕,					ahen		
21 22 23 24 25		 NW	HS HS		IIS I	10	9. 10. 9.	3	0,6	45 U. 5	sh <b>⊜</b> Tr o^ <b>⊙</b> ₀.	opfen, 8 abends :	• O., nac	hts 📵.	
26 27 28 29 30 31	HS 10 HS 10 FS 2 S 6 FS 5		FIIS IIS II	8 SW 3 1 NE	FBS FBS FS FS FS	3 ··· 3 ··· 3 ··· 5 ···	9. 7. 2. 3. 3.	.7		Morge Morge Morge	ns = <sub>1</sub> , ans = <sub>1</sub> .	abends = abends = abends = abends =	ds ⇒		
Mittel		.9		7.5		7.1	7	- 1	S. 33. 8	Monge		ancings .			
					-	b) Aut	graph	ische	Aufze	ichnur	gen				
Tag					Luftd	ruck	ant oo to	eduzier	t in Milli	metern	= 700°	+	-		1
1 ag	124	14 <sup>b</sup>	16h	134	30 <sup>h</sup>	2.214	Ot-	21.	4 <sup>2</sup>	6 b	84	109	Tages- mittel	Max.	Min
1 2 3 4 5	44.0 46.0 30.0 48.6	44.2  46.3 50.2 48.5	44.7  46.3 50.4 47.9	45.2 47.0 50.7 47.7	46.1 47.8 50.8 47.8	46.3  48.2 50.2 47-9	45.6 48.6 49.7 47.7	44.8 41.6 48.3 48.8 47.2	41.3 48.3 48.2 46.9	41.3 48.5 48.1 46.8	43.8 49.2 48.3	45.3 49.6 48.6 47.7	47.84 49.50 47.68	\$0.0 \$0.8 48.6	46. 48. 46.
6 7 8 9	47.7 46.2 45.2 43.6 51.4	47.6 45.7 44.9 43.6 51.8	47.0 45.5 44.8 43.6 52.2	47.1 45.4 45.0 44.0 52.9	47.2 45.5 44.9 44.9 53.3	46.1 45.4 44.9 46.5 53.4	46.9 44.9 44.4 47.0 52.8	46.8 44.5 43.8 47.5 51.9	45.7 44.2 43.2 47.9 51.6	45.9 44.5 43.0 48.8 51.3	46.4 44.8 43.3 49.8 51.6	46.4 45.1 43.6 50.9 52.1	46,68 45.14 44.25 46.51 52.19	47.7 46.2 45.2 51.4 53.4	45. 44. 43. 43. 51.
11 12 13 14	51.9 49.0 42.8 46.7 48.2	51.6 48.7 42.5 46.7 48.0	51.5 48.6 42.3 46.7 48.0	51.5 48.4 42.4 46.9 47.7	51.5 48.6 42.6 47.2 47.9	51.3 48.3 43.0 47.5 47.9	50.8 47.2 43.4 47.8 47.5	50.1 45.8 44.2 48.0 47.0	49.5 44.8 44.6 47.9 46.9	49.0 43.9 45.4 47.5 46.7	48.9 43.6 46.0 47.8 47.1	49.1 43.5 46.6 48.2 48.0	50.56 46.70 43.82 47.41 47.58	51.9 49.0 46.7 48.2 48.2	48. 42. 42. 46.
16 17 18 19	48.2 47.5 46.9 44.4 40.4	48.2 47.3 46.7 44.3 39.7	47.9 47.3 46.3 43.9 38.7	47.6 47.4 46.2 43.9 38.4	47.7 47.7 46.2 44.1 38.5	47.6 47.6 46.0 43.9 38.4	47.5 47.4 45.3 43.6 37.7	46.8 47.2 44.2 42.8 37.1	46.5 46.9 43.7 41.9 36.5	46.5 46.6 43.4 41.3 36.0	46.7 46.6 43.7 40.9 35.9	47.4 46.8 44.5 40.7 35.9	47.38 47.19 45.26 42.98 37-77	48.2 47.7 46.9 44.4 40.4	46. 46. 40. 35.
21 22 23 24 25	35.7 37.6 38.5 40.9 43.8	35.7 37.5 38.8 40.4 44.1	35.5 37.5 38.9 40.4 44.3	36.0 37.5 39.4 40.4 45.1	36.5 37.7 39.8 40.7 45.7	37.8 37.8 39.9 41.1 46.0	37-1 38.1 40.4 41.3 46.0	36.6 37.4 40.6 41.5 46.1	36.9 37.0 40.1 41.7 46.1	36.9 37.0 40.4 41.9 46.2	37.0 37.3 40.9 42.8 46.7	37.4 38.1 41.0 43.5 47.6	36.53 37-54 39.89 41.38 45.64	37.6 38.5 41.1 43.8 48.3	35 37 38 40 43
26 27 28 29 30 31	48.3 50.1 52.7 53.8 51.2 48.3	48.4 59.4 52.9 53.9 51.3 48.0	48.3 50.0 53.4 53.8 51.2 47.6	48.6 51.0 54.2 53.9 51.3 47.7	49.0 51.7 54.7 54.1 51.2 47.7	49.1 51.8 54.5 53.7 50.7 47.2	49.1 51.4 54.1 53.3 50.1 46.5	49.2 51.4 53.5 52.3 49.5 45.6	49.1 51.3 53.1 51.4 48.8 44.8	49.1 51.3 52.9 51.2 48.3 44.3	49.4 51.8 53.2 51.1 48.1 44.5	\$0.0 52.3 53.7 51.2 48.2 45.0	48.97 51.26 53.58 52.81 49.99 46.41	50.1 52.7 54.7 54.1 51.3 48.3	48. 50 52 51 48
Mittel	46.40°)		46,22	46.39	46.66	46.66	46.47	46.0	1	45.61	45.89	46.30	46.22	47-77	44

Tag	.1					L	ufttemp	peratu	nach	Celsius					
	12 <sup>h</sup>	14%	164	184	201	22 <sup>h</sup>	Oh	2 <sup>h</sup>	411	64	8,	100	Tages- mittel	Max.	Min
3 4	11.6 15.9 13.4 10.6	11.5 14.3 12.2 9.7	11.5 13.7 12.3 8.4	11.6 13.8 12.4 8.1	15.5	17.3 19.1 12.6 14.6	20.8 21.9 13.2 16.4	22,1 23,5 14,4 18,7	22.5 23.0 14.2 18.4	21.1 21.5 14.0 17.0	16.5	16.7 14.6 11.6	16.62 17.80 12.99 13.49	22.5 24.0 14.5 18.7	13.4
5 6 7 8	13.3 12.9 16.1	12.4 12.1 15.4 15.9	12.2 11.5 14.7	12.7 12.5 15.6	18.7	20.6 22.6 19.1	14.6 22.2 24.6 20.7	23.3 25.1 21.5	23.0 24.8 21.7	20,8 22,6 20,4	18.4	14.2 17.0 17.2 16.1	14.52 17.63 19.74 17.86	17-5 23-3 25-5 22-1	11.4 14.4 13.9
9 10	16.5 14.8 7.1 9.4	13.9 6.6 8.6	12.7 5.9 7.7	6.3	8.6	7 · 4 10 · 3	6.8	8.5 12.4 17.3	9.7 13.0 18.2	10.3	10.0	8.3 9.8	10.19	14.8 13.3 18.2	5.7
13 14 15	11.9 12.1 8.7 10.3	10.7 11.7 9.0 10.0	9.9 10.9 8.9 9.8	9.9 10.5 9.1 10.2	13.5 9.0 10.3 12.1	17.6 8.0 10.8 14.3	7.1 11.5 15.4	7.5 11.0 17.6	21.0 7.7 11.1 17.3	7.5 11.3 16.1	17.7 S.1	8.6 10.7 12.1	15.66 9.06 10.28 13.24	21.2 12.2 11.7 17.8	9.5 7.1 8.7 9.7
16 17 18 19	10.5 12.8 12.2 13.6 13.7	9.7 11.7 11.3 12.8 13.3	9.0 10.8 10.8 11.6	9.4 11.2 11.0 12.4	12.8 13.7 13.4 13.4 14.8	16.4 16.8 17.8 15.5 16.8	18.3 17.9 20.3 16.7	19.7 18.2 21.9 17.7 14.9	19.3 17.6 20.6 17.9 16.9	18.4 17.0 19.7 17.4 16.7	15.8	14.1 13.8 15.5 14.4 13.9	14.46 14.78 16.02 14.95	19.9 18.4 22.0 17.9 18.0	9.0 10.7 10.7 11.6
21 22 23 24 25	13.4 10.5 10.0 7.2	13.0 9.8 8.6 6.6 8.7	12.5 6.7 7.4 6.1 8.3	11.5 8.2 7.1 7.0 8.7	12.8 7.5 6.9 9.4	13.0 8.5 7.9 10.9	9.2 9.4 12.0	13.6 12.0 8.9 12.0	12.8 12.7 9.4 12.2	13.2 13.1 9.0	12.8 12.0 8.2 10.4	11.9 10.4 7.7 9.7	12.83 10.05 8.37 9.58	13.7 13.7 9.4 12.4	7.5 7.1 6.1
26 27 28 20	10.9 8.4 10.2	10.3 7.0 8.6	9.9 6.8 7.6 9.3	9.0 8.0 7.9 9.9	11.7 10.9 12.9	12.5 13.9 15.2 17.4 19.4	14.8 16.5 18.9 21.2	13.7 15.3 18.2 20.2 22.4	13.5 15.3 17.8 20.7 22.7	13.2 14.7 17.7 20.4 21.8	12.3 12.5 15.4 16.7 18.6	11.4 10.2 12.3 13.8 15.9	11.21 12.38 12.85 14.61 16.51	14.2 15.8 19.1 21.0	8.4 6.8 6.9 9.2
30 31	14.1	12.7	12.5	11.8	17.3	21.1	22.9 24.1 16.42	25.5	24.0 25.8	23.6 25.4	20.5	17.3 18.4	18.40	24.7 26.2	11.1
		-	-				-	.,			1		13.7	10.20	9.0
Гаg	12h	141		tung 6h	18%	chwind 206	igkeit (	G) des	Vinde	s in 1	Sekunde 4 <sup>th</sup>	in Meters	81	10%	Tage
_	R G		G R	G	R G	R G	R G	R	G R	G	R G	R = G	R G	R G	G
3 4 5	SSW 2,6 S 1,5 WNW 1,2 SSW 0,9 NNE 1,4	SSW SSW	1.8 ESI	2.6 E 0.7 V 2.0 V 0.7	S 1.0 ESE 0.4 W 3.3 S 0.6 NNE 2.3	WSW 2.8	WSW 3. ENE 3.	WSW E	2.1 581 1.9 S1	S 3.0 N 2.0 N 2.6 E 2.8 E 3.0	SSE 3.2 S 2.0 SW 2.7 E 4.5 ESE 2.9	SSE 2.7 WSW 3.1 SW 3.0 E 3.5 ESE 4.0	SSW 1.1 NW 3.0 WSW 1.5 E 2.6 NE 2.0	WSW 1.5 E 2.0	2.4 1.9 2.3 2.2
6 7 8 9	E 2.0 ESE 1.9 ESE 0.5 N 1.6	ENE C	.6 ENI	E 0.5 E 1.9 F 1.2	ENE 3.5	SE 4.5 S 1.1 WNW 2.1 N 5.2	SSE 4. S 5. W 2.	SE SE	5.8 S	E 5.7	SE 5.2 S 6.7 WSW 1.0	SSE 2.1 SW 4.6 SW 1.1 N 2.8	SE 1.3 SW 2.0 N 3.6 N 0.5	ESE 2.3 S 0.2 N 2.8	2.5 3.3 3.3 1.8
11	N 2.1 SSW 1.1 SSW 0.8	SSW 2	.0 NNW	1.4	S 1.5 S 1.0	S 2.0 SSW 2.3	WSW 1.5	NAW :	4 WAY	¥ 2.5 ¥ 1.0	N 1.0 SE 1.4	NNE 1.6 S 1.5 SE 1.0	NNE 1.4 SSW 1.5 SSE 1.0	NNE 0.5 SSW 2.0 NNW 1.4	1.5
14	N 1.7 N 2.3 NNW 1.4 NE 1.6	NNW o	A NNW	4.9 2.6 0.6	N 3.7 NNE 3.0 NNW 1.2 NE 1.7	N 5.2 NNE 2.7 NE 1.5 E 3.8	N 4.6 NNE 2.4 NE 2.5 E 4.5	NNE :	.5 EN	N 4.0 N 1.5 E 3.0	N 3.0 N 2.1 E 3.5 E 5.1	N 4.8 N 1.5 E 2.6 E 5.9	NNW 1.1	3 2.0	3.8 2.1 2.1 3.4
78 9	E 0.8 ENE 1.2 SSW 0.6 SW 0.2	NE I NE O SSW o	.6 NNE	0.6	NE 1.0 NNE 0.9 0.0 SSW 0.7	E 3.3 E 0.6 NE 0.6 SSW 0.5	E 4.8 SSE 1.4 N 1.6 WSW 1.9	SSW :	I SSV	2.6		E 2.7 VNW 1.5 N 0.7 W 0.5	ENE 3.1 W 0.6 0.0 W 2.1	E 1.4 SW 0.8 SW 0.2 WSW 3.2	3.4 2.8 1.3 0.7
3	N 1.5 N 1.5 N 1.5 N 1.5 ENE 0.8	NW 2 NNE 0 N 1 N 3 ENE 0	S ENE	2.8	NW 2.6 NE 1.8 N 1.4 N 3.1	NNW 2.5 NNE 1.4 N 2.2 NNE 2.1 NNE 1.0	N 0.9 NNE 1.4 N 2.3 NE 3.3 NE 1.4	NNE 1 NNE 2 NNE 2	.9 SE	1.6	N 2.0 NNE 1.5 NNE 2.9 E 1.9 NE 1.5	NW 1.2 N 0.9 N 2.0 SE 2.0 NNE 1.8		WNW 2.4 N 1.0 N 1.4 ENE 0.6 ESE 0.2	2.1 1.3 1.9 2.4
6 7 8 9	ESE 0,2 0.0 S 0.9 SSE 0.6 SE 0,4	SSE 0. SW 0. SSW 1. SSE 0. SW 0.	2 SSE 2 S 1 S	0.4	SSE 0.5 S 0.4 S 0.5 S 0.5 S 0.3	SSW 1.1 NE 0.8 S 0.6 ENE 0.0 ESE 0.7	ESE 1.4 E 1.1 ENE 1.3 ESE 1.6 ENE 2.3	SSE 1 SE 1 S 1 ESE 2	SE S	1.8	E 1.6 SSE 1.4 SE 2.0 ESE 2.6 SE 1.9	ESE 2.0 ESE 2.1 E 1.0 SE 1.5 ESE 1.8	SE 0.3 ESE 0.2 SE 0.3 ESE 0.2	S 0.3 0.0 0.0 SE 0.4	0.9 0.9 1.0 1.3
1	··· 0.0	50.	8 SSE	0.6	SSE 0.5	SSW 1.6	SSW 1.3	SSE 1	5 SE	2.5	ESE 2.2	SE 2.1	ENE o.6	8 0.5	1.2

						JUNI					1905
						rekte Ables	ungen				
T	1. uf	tdruck	auf o" red	uziert in N	Tillim.	= 700=+		Lu	fttemperatu	r nach Celsiu	8
Tag	19 <sup>h</sup>		24	96		Tagesmittel		94	2 h	94	Tagesmittel
1	45.8		45.0	45-7	,	45.50	1	6.7	26.7	19.8	21,07
2	47.7		48.5	49.1		45.43				19.4	19.67
3	50.3		48.7	47.9	2	48.97	- 1	5.3	25.7	21.2	29.73
5	47.8		45.5	44.5		45.93	1 2	0.8	30.4	23.9 23.1	23.93
6	40.5	1		37.4	- 1	38.60	8	9.7	27.0	20.2	22.30
7 8	35.8	1	37.9	38.0	)	36.03		5.9	24.1	15.2	19.40
8	41.2		40.8	42.2		41.40		4.8	20.8	16.5	17.37
10	42.0		42.9	42.2		42.50		3.2	17.1	14.6	14.97
	42,0		41.0	41.5		41.50		2.7	19.2	14.3	15.40
12	43.1		43.1	43.0	1	43.07		2.0	17.5	14-4	14.93
13	43.2		41.2	42.5		42.83	1	0.5	14.9	13.0	12.97
15	42.7	1	41.9	42.4		42.33	1	1.4	24.5	20.8	19.90
16	43.8		42.4	41.7	.	42.63	11	6.7	26.1	21.5	21.43
17	40.5		38,6	38.1		39.07		6.1	24.4	18.4	19.63
18	37.7 44.5	i	35.0 45.9	41.2		38.97 45.79	1 :	6.3	20.6	19.2	18.97
20	49.2		49.7	51.3		50.07	1	7.0	24.7	20.0	20.57
21	53.2	i	51.9	50.9	.	52.00	1	5.7	25.5	21.2	21.13
22	48.7	1	46.5	47.1	1	47.43	13	5.4	23.4	17.4	19.73
23	46.7		45.7	46.1		46.17 47.67	1.	4.0	20.9	15.2	14.67
25	46.4		45.6	45.6		45.87		5.6	23.8	19.6	19.67
26	45.6		44.6	45.2		45.13	- 12	3.3	19.5	19.1	18.97
27	45.0		41 1	43.7	1	44.07	10	7.6	26.3	19.1	21.00
20	44.0		41.7	41.2		42.30		7 - 5	27.0	21.1	22.17
30	43.1		42.4	43.4		42.97	2	i.i	29.7	25.2	25.33
Mittel	44.3	9	43 - 47	43-7	7	43.88	10	5,22	23,10	18.78	19.37
Təg	Dun	stdruck	in Millim	Tages-	198	Relative Fer	chtig	Tages-	Richtung	u. Stärke d Skala: o — 10	es Windes
	1		-	mittel	.,		,	mittel	.,		
1 2	9.2	7.0	10.9	9.0	65	27	63 66	52	S I N 2	ESE 1	NNW 2
3	10.8	7.1 8.8	9.8	9.7	76 80	35	53	59	SSW 1	SSE	E 2
4	10.3	7-7	11.6	9.9	64	37	5.3	47	NE 1	SSE 1	8 1
5	11.6	9.4	12.6	11.2	64	29	60	51		SE 1	
6	11.8	10.5	12,6	11.7	70 73	40 55	72 65	61	WNW I	NNW 3	NNW 1 W 3
8	7.7	7.4	9.7	8.3	62	41	69	57	WAW 2	NW 2	0
9	8.6	7.4	8.5	7.9	74 76	51	60	63	NW 2 NE 3	NNW 2 E 4	ENE 1
11	6.6	6.1	6.9	6.5	60	37	57	51	ENE 2	E 2	ENE 4
12	5.6	5.1	6.4	5.4	51	34		43	ENE 2	NE 3	SE I
13	6.1	5.8	6.5	6,1	62	47	45 58	56	SE I	ENE 2	ENE 2
14	9.7	7.4	9.2	7.8	73 80	45	71 62	63	ENE I	SE 2	ESE 1
16	11.2	9.0	11,4	10.5	79	37	60	59	0	SE 3	E 2
17	10.3	9.4	12.1	10,6	76	42	77 68	65	*** 0	NAE 1	N 1
18	11.7	12.2	11.3	11.7	81			72	S 1	NNW 2	W 2
20	11.3	8.4	12,6	10.8	79	55 36	77 72	73 62	SSW 1	N	E 1
21	11.5	9.1	10.9	10.5	81	38	59	59	S 1	NE I	0
22	9.6	11.1	8,2	9.6	61	52	56	\$6	SE I	N 1	0
23	7.5	8.8	9.4	9.9	61	67	78	69	W 2 E 1	ENE 2	N 1
25	10.9	10.3	12.5	11.2	83	47	74	68	ENE :	ESE 3	SE 1
26	11.9	14.8	12.8	13.2	77	88	78	Sı	SE 1	0	0
27	10.5	9.2	12,8	10.8	70	37	78	62	ESE 1	NSW 2	NNW I
28	11.2	9.7	15.3	10.0	75 82	37	59	57	S 1	E 1	NNW I
30	14.1	13.1	14.5	13.9	76	42	61	60	ESE :	SSE	0
Mittel	10.1	0.2	10.7	10.0	73	44	65	61	1.2	1.5	1.1
	i i	1	1		.,		.,				

1	Tag		Bewöl	kung [	Skala; o	kenzu	g, 10 ==	trüb]		Nieder- schlag in			Beme	rkun	gen	
18			9h	1	ph .		9h	Tages	mittel							
4	2		10	FHS	5 11	FIIS	10 W	8	. 3		Abene	ls dunst	tig.		m NE, n	ichts
7 FINS 10   FINS 10 W   F	5	FS FS	4	FIIS	7 7 N	FHS	S	5	.7	***	Morge	ns =:	RUCHUS .	autistig.		
18	7 5	FHS	7	FHS	10 W	Fils	10 NW	10	.0	2.5	5070-	201. 0			<b>⊚</b> , ℝ	
13	10	HS .	3	FHS	6 E 7 NE	FHS	3 3 E	E 4.3		0.5	21 h-23h @,.					
S	13	H FS	0	FHS	8	FHS	3 ···	7.0 8.0 5.0		0.5	Abends dunstig.  Morgens = , , a abends dunstig, 25 0 ,					
Fills   0	16	FHS	4	FHS	9	FHS	9	6.3		8.4						
FN   10	19	HS FHS	9	FH 8 FHS 3 FS 5 H 7 N FHS 5 FS 10 FHS 4		5	7.0		7.8	Morge	ns =,	abends	dunstig.			
## 15   10   10   10   10   10   10   10	22 23 24	FR FRS	9 FHS 10 NW		FHS FHS HS	9 N	9.	3	0.9	Morge 22h	ns =.	u. sta	n			
Pi   10   Pi   Pi   Pi   Pi   Pi   Pi   Pi   P	26	FS	FIS 10 FIS 10 FIS 10 SE FS 7 IIS 9 S S 1 IIS 9 S W S 9 S S S S S S S S S S S S S S S S S		FHS	3 8 SW	6.	.1	10.6			V. dunst	Tropi			
Luftdruck auf o' reduziert in Milimetera	28	FHS	0			FHS 10 W 6.7		7	***	Morgens u. abends dunstig.					[[₹ u.	
Leftdruck auf o' reduzieri in Millimeters 700°° +  Leftdruck auf o' reduzieri in Millimeters 700°° +  1 43° 140° 150° 150° 22° 00° 22° 00° 22° 00° 00° 178ges Max.  1 43° 3 45° 3 45° 3 45° 2 45° 10° 10° 10° 10° 10° 10° 10° 10° 10° 10							6.4	7.	.0	S 42.0						
Tags  1	Mittel		0.7		7.0			9		0. 41.0						
129	Mittel		0.7		7.0				ische	Aufzei						_
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$						Lufte	lruck :	aufo'r	ische	Aufzei	metern	700***		Tages.		
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$		124	145	16 <sup>h</sup>	18h	Lufte 201	lruck 22h	oh	eduzica 2 <sup>k</sup>	Aufzeirt in Milli	mctern 65	700*** Sh	10h		Max.	М
5         44.8         44.0         44.7         44.4         43.8         42.6         41.2         41.2         41.0         41.2         41.9         41.2         41.2         41.0         41.4         41.75         44.8           6         44.1         40.5         40.5         60.6         40.5         60.7         30.4         37.0         37.6         37.8         39.6         30.6         30.8         40.8         40.8         41.7         42.7         42.0         42.0         42.0         42.0         42.0         42.0         42.0         42.0         42.0         42.0         42.0         42.0         42.0         42.0         42.0         42.0 <td>Tag</td> <td>45.3</td> <td>145</td> <td>16<sup>h</sup></td> <td>18h</td> <td>20"</td> <td>22h</td> <td>oh</td> <td>eduzica 2<sup>k</sup></td> <td>Aufzeirt in Milli</td> <td>65 44.8</td> <td>700*** Sh</td> <td>10<sup>h</sup></td> <td>mittel</td> <td>46.3</td> <td>41</td>	Tag	45.3	145	16 <sup>h</sup>	18h	20"	22h	oh	eduzica 2 <sup>k</sup>	Aufzeirt in Milli	65 44.8	700*** Sh	10 <sup>h</sup>	mittel	46.3	41
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	Tag	45.3 46.3 49.9	14 <sup>3</sup> 45-3 46.6 49.8	16 <sup>h</sup> 45.2 46.7 49.6	18h 45.7 47.7 50.0	Lufte 20's 46.0 48.2 50.4	22h 45.9	oh 0 1 1 45.5 49.2 49.5	2 <sup>t</sup> 45.0 48.3 48.7	4 Aufzei rt in Milli 4 4 7 48.1	65 44.8 48.2 47.5	700*** Sh 45.2 48.5 47.7	10 <sup>h</sup> 45.9 49.5 48.0	mittel 45.38 48.04 49.09	46.3 49.9 50.4	44 46 47
8 90.6 90.6 90.7 90.7 90.7 90.7 90.7 90.7 90.7 90.7	Tag	45.3 46.3 49.9 48.2	14 <sup>3</sup> 45.3 46.6 49.8 48.1	16 <sup>h</sup> 45.2 46.7 49.6 47.8	18h 45·7 47·7 50·0 47·8	Lufte 20'4 46.0 48.2 50.4 47.8	22h 45.9 49.0 50.2 47.0	oh 45-5 49-2 49-5 46-5	2 <sup>t</sup> 45.0 48.3 48.7	Aufzei rt in Milli 4 <sup>k</sup> 44.7 48.1 47.8 44.8	65 44.8 48.2 47.5 44.1	700°°° 8°° 8°° 8°° 8°° 8°° 8°° 8°° 8°° 8°	10 <sup>h</sup> 45.9 49.5 48.0 44.6	mittel 45.38 48.04 49.09 46.37	46.3 49.9 50.4 48.2	44 40 47 44
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	Tag  1 2 3 4 5 6	45.3 46.3 49.9 48.2 44.8	14 <sup>5</sup> 45-3 46.6 49.8 48.1 44.6	16 <sup>h</sup> 45.2 46.7 49.6 47.8 44.4	18h 45·7 47·7 50.0 47.8 44.6	20° 46.0 48.2 50.4 47.8 44.7 40.5	22h 45.9 49.0 50.2 47.0 44.4 40.2	ob 45.5 49.2 49.5 46.5 43.8 39.4	45.0 45.0 48.3 48.7 45.5 42.6	41.5 37.0	65 44.8 48.2 47-5 44.1 41.2 37.6	700°00 Sh 45.2 48.5 47.7 44.2 41.0	10 <sup>h</sup> 45.9 49.5 48.0 44.6 41.4	mittel 45.38 48.04 49.09 46.37 13.25 39.18	46.3 49.9 50.4 48.2 44.8 41.1	44 40 47 44 41
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	Tag  1 2 3 4 5 6	45.3 46.3 49.9 48.2 44.8 41.1 37.4	14 <sup>5</sup> 45-3 46.6 49.8 48.1 44.6 36.6	16 <sup>h</sup> 45, 2 46, 7 49, 6 47, 8 44, 4	18h 45-7 47-7 50-0 47-8 44-6 40-6 35-7 40-9	20° 46.0 48.2 50.4 47.8 44.7 40.5 35.9	1ruck 22h 45.9 49.0 50.2 47.0 44.4 40.2 35.5	45.5 49.2 49.5 46.5 43.8 39.4 35.0	45.0 48.3 48.7 45.6 37.9 34.3	44.7 44.7 48.1 47.8 44.8 41.5 37.0 35.7	63 44.8 48.2 47-5 44.1 41.2 37.6 36.7	700°00 Sh 45.2 48.5 47.7 44.2 41.0 37.5 37.2	10 <sup>h</sup> 45.9 49.5 48.0 44.6 41.4 37.3 35.6	## 45.38 48.04 49.09 46.37 13.25 39.18 36.18	46.3 49.9 50.4 48.2 44.8 41.1 39.0 42.5	44 40 47 44 41 37
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	Tag	45.3 46.3 49.9 48.2 44.8 41.1 37.4 39.6 42.5	14 <sup>3</sup> 45.3 46.6 49.8 48.1 44.6 40.5 36.6 39.9 42.4	16 <sup>h</sup> 45.2 46.7 49.6 47.3 44.4 40.5 35.5 40.2 42.3	18h 45-7 47-7 50-0 47-8 44-6 40-6 35-7 40-9 42-5	Lufte 20" 46.0 48.2 50.4 47.8 44.7 40.5 35.9 41.1 42.7	45-9 49-0 50-2 47-0 44-4 40-2 35-5 41-2 42-6	45.5 49.2 49.5 49.5 43.8 39.4 35.0 40.8 42.3	2th 45.0 48.5 48.7 45.5 42.6 37.9 34.3 40.8	43.1 44.1 47.8 44.7 47.8 44.5 37.0 35.7 40.8 41.8	44.8 48.2 47-5 44.1 41.2 37.6 36.7 41.1 41.7	700°°° Sh 45.2 45.2 48.5 47.7 44.2 41.0 37.5 37.5 41.7 41.8	10 <sup>h</sup> 45.9 49.5 48.0 44.6 41.4 37.3 35.6 42.4	## 45.38 48.04 49.09 46.37 13.25 39.18 36.18 40.87 42.23	46.3 49.9 50.4 48.2 44.8 41.1 39.0 42.5 42.8	44 46 47 44 41 37 34 39 41
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	Tag  1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28	45.3 46.3 46.9 48.2 44.8 41.1 37.4 42.5 42.4 42.3 42.2 42.9 42.5 42.3 42.9 42.5 42.9 42.5 42.9 42.5 42.9 42.5 42.9 42.5 42.9 42.5 42.5 42.9 42.5 42.5 42.5 42.5 42.5 42.5 42.5 42.5	14 <sup>3</sup> 45.3 46.6 49.8 49.8 144.6 10.5 16.6 10.5 10.9 12.4 42.1 42.1 42.1 42.1 42.1 42.1 42.1	16 <sup>th</sup> 45.2 46.7 49.6 44.4 40.7 49.6 44.7 49.6 44.4 40.2 42.3 41.9 42.1 42.1 42.1 43.6 43.6 43.6 46.9 46.3 46.9 46.3	18 <sup>h</sup> 45.7 50.0 42.7 50.0 44.6 47.7 50.0 42.5 41.9 42.7 42.3 42.3 42.3 42.6 43.0 42.3 43.0 42.5 41.9 42.6 43.0 42.6 43.0 42.6 43.0 43.0 43.0 43.0 43.0 43.0 43.0 43.0	Luftc 20' "" 48.2 47.4 47.5 44.7 40.5 50.4 44.7 42.7 42.0 43.1 42.6 43.8 43.8 43.1 49.6 43.8 48.1 49.6 45.7 45.1	### ### ### ### ### ### ### ### ### ##	and o' r oh 45-5 49-2 49-2 49-3 49-3 49-5 49-6	24 45.0 48.7 45.5 48.7 45.6 48.7 45.6 48.7 41.8 41.8 41.8 41.2 41.2 42.8 41.2 42.8 41.2 42.6 43.1 43.1 43.1 43.1 43.1 43.1 43.1 43.1	Aufzei rt in Milli 44-7-7-48-11 44-7-7-48-11 47-8-8-44-8 44-8-8-44-8 44-8-44-1 40-5-5-48-8 41-3-3-1 41-4-9-1 42-1 43-1 44-7-8-4 44-7-8-8 44-7-8 4	mctern 6h 44.8 48.2 47.5 44.1,3 37.6 41.2 41.7 41.9 40.7 41.9 40.7 41.1 41.9 40.7 41.6 42.5 42.6 42.6 42.6 43.3 47.2 45.1	700***  Sh  45.2 48.5 45.7 45.2 48.5 45.7 41.0 41.3 41.5 41.9 41.5 41.9 42.9 41.5 41.9 40.2 40.2 40.2 40.4 40.4 40.4 40.4 40.4	10h 45.9 49.5 48.0 44.6 41.4 37.3 35.0 42.4 42.3 42.3 42.4 42.5 42.5 42.5 42.6 43.6 51.0 51.8 51.0 51.8 51.0 45.2 46.5 47.0 45.2 46.5 47.0 45.2 46.5 47.0 47.0 47.0 47.0 47.0 47.0 47.0 47.0	mittel  75.38 48.04 49.09 46.37 49.27 49.28 49.28 49.28 49.28 40.27 42.28 42.28 42.28 42.28 42.47 44.48 42.76 430.68 42.76 430.68 42.48 44.48 44.48 45.20 44.48 45.20 44.48	40-3 49-9 50-4 48-8 41-1 39-0 42-5 42-8 43-2 42-3 43-3 43-3 43-3 43-3 43-7 41-7 47-7 52-2 43-2 47-7 47-7 52-2 48-2 46-9 45-8 45-1 44-1	444 447 444 413 379 411 40 42 42 41 41 41 38 37 41 47 50 45 45 46 46 47 46 47 47 47 47 47 47 47 47 47 47 47 47 47
Mittel 44.23 44.11 44.06 44.28 44.46 44.34 44.07 43.47 43.23 43.16 43.41 43.94 43.90 45.33	Tag  1 2 3 4 5 6 7 8 9 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 29	45.3 46.3 40.9 48.2 44.8 41.1 37.4 42.4 42.4 42.3 42.4 42.3 42.7 42.7 38.0 41.7 51.0 47.7 52.2 51.0 47.9 47.7 47.7 47.9 47.9 47.9 47.9 47.9	14 <sup>3</sup> 45.3 46.6 49.8 40.5 30.9 42.2 42.3 42.4 42.3 42.4 42.5 42.4 42.5 42.4 42.5 42.4 42.5 43.1 61.4 6.7 6.6 7.6 6.7 6.8	16h 45,12 46,7 49,6 47,8 44,4 40,5 33,5 42,9 42,3 42,3 42,3 42,3 42,3 42,3 42,1 42,4 43,6 43,6 43,6 43,6 44,0 45,6 46,7 46,7 46,7 46,7 46,7 46,7 46,7 46	18h 45-7, 50-6 44-6, 44-6, 44-6, 42-5, 42-5, 42-6, 42-7, 43-9, 42-6, 43-9, 42-7, 43-9, 42-8, 43-9, 42-8, 43-9, 42-8, 43-9, 42-8, 43-9, 43-	Luftc  20' 40.0 50.4 47.5 50.4 47.5 40.7 40.7 40.7 40.7 40.7 40.7 40.7 40.7	22h 45.9 49.0 50.2 47.0 48.2 49.2 49.2 49.2 49.2 49.2 49.2 49.2 49	oh 45-5 49-2 45-6 49-2 45-8 45-5 18-0 45-5 18-0 45-5 18-0 45-5 18-0 45-5 18-0 45-5 18-0 45-6 18-	2h 45.0 48.5 48.7 45.6 48.7 45.6 48.7 45.6 48.7 41.8 41.8 41.8 41.9 41.1 42.8 41.2 45.6 45.6 45.6 41.6 45.6 41.6 45.6 41.6 45.6 41.7 41.7 41.7 41.7 41.7 41.7 41.7 41.7	Aufzeit tin Milli d. 44-7 48-11 44-7 48-11 47-8 44-8 44-8 33-9 40-8 44-8 44-8 44-8 44-9 44-9 44-9 44-9 44	metern  44.8  48.2  47.5  44.1  37.6  36.7  41.1  41.7  42.8  41.2  41.2  41.3  38.3  39.5  45.9  45.3  45.3  45.3  40.8  40.8	700***  Sh  ****  ****  ****  ***  ***  *	10 <sup>h</sup> 45.9 46.0 44.6 41.4 37.3 38.6 42.4 42.3 41.7 42.8 41.6 38.1 41.4 47.0 51.8 51.0 47.2 47.8 45.8 41.7 42.8	mittel  75, 38 48.04 49.09 46.37 13.25 39.18 30.18 40.87 42.23 42.47 41.53 42.47 41.85 42.27 41.85 42.85 42.27 44.95 44.95 44.95 44.95 44.95 44.95 44.95 44.43 47.46 45.20 44.37 42.73	40-9 40-3 49-9 50-4 48-2 48-2 41-8 41-1 39-0 42-8 43-3 43-3 43-3 43-3 43-3 43-3 43-3 43-3 43-3 43-9 41-7 41-9 41-7 41-9	444 447 444 413 379 411 40 42 42 42 41 41 41 41 47 50 45 46 46 47 48 48 48 48 48 48 48 48 48 48 48 48 48

ag	124	141	165	184	204	225	04	ah	4h	6h	89	100	Tages-	Max.	Min.
,	12°	14"	10.	10.	20"	22	0.	2"	4"	-	0.		mittel	Max.	pann.
1	17.2	16.1	14.9	15.3	19,2	23.1	25.2	26.7	27.0	23.1	20.7	19.7	20,68	27.1	14.4
3	18.5	16.7	16.0	16.4	18.3	18.9	21.0	22.8	26.0	22.4 25.8	20.1	18.4	19.32	23.3	15.6
	18.7	17.9	16.4	17.0	21.9	26.4	28.5	20.4	29.6	28.9	25.3	23.5	23.62	30.1	16.3
6	21.5	20.6	19.1	19.3		26.7	29.8	30.4	30.2	27.2	21.6	19.8	24.54 22.08	27.5	17.2
7	18.6	19.7	17.8	17.8	19.7	24.7	23.1	27.0	23.9	18.5	16.2	15.1	19.16	24.5	14.1
	14.1	13.6	12.5	13.6		17.9	19.4	18.4	17.0	16.5	17.2	15.5	16.71	21.5	12.4
0	14.7	14.8	13.7	13.2		12.8	14.7	17.1	17.4	17.3	15.8	13.8	14.92	18.0	12.1
1	12.1	11.9	11.3	11.5	14.7	17.7	19.0	19.2	19.2	18.7	15.6	13.5	15.37	19.6	11.0
	13.4	11.5	10.9	11.0		13.7	17.0	17.5	17.8	17.0	15.1	14.0	14.65	17.9	10.5
	11.1	9.1	7.5	8.6		16.5	19.0	19.2	19.1	19.9	16.8	14.7	18.92	20.4	7.5
5	17.9	16.3	15.0	11.5		23.1	23.8	26.1	25.2	25.4	22.3	20.5	21.23	26.7	15.0
,	18.6	17.2	15.6	14.9	18.9	21.1	24.0	24.4	22.8	20.5	19.2	17.6	19.57	25.2	14.9
3	16.6	16.3	16.1	16.7		28.1	23.5 18.6	20.6	19.0	20.4	19.8	18.7	18.90	23.5	16.1
,	16.7	16.0	15.7	16.9	18.1	22.2	23.7	24.7	25.0	25.2	21.7	19.2	20.43	25.6	15.5
ı	17.6	16.0	15.0	15.0		23.3	24.6	25.5	25.4	25.6	22.5	20,1	20.92	26,3	14.5
2	18.4	17.2	16.6	17.3	19.9	13.4	23.7	15.4	15.3	16.3	19.4	17.5	14.67	16.3	13.1
	13.1	12.4	12.2	12.7	15.2	17.8	20,1	20.9	20.7	20,5	18.9	18.2	16.80	21.2	14.7
6	17.0	15.2	16.0	16.8		23.9	25.3	19.5	23.5	23.0	1	18.2	19.74	25.3	15.6
7	17.1	16.1	15.0	15.5		24.8	25.9	26.3	23.0	21.5	20.3	18.5	20.38	27.7	15.0
3	17.7	16.7	15.7	16.6		23.5	25.5	27.0	26.8	25.4	23.5	22.0	21.72	27.8	17.8
5	20.4	19.0	18.2	19.5	23.2	26.0	28.4	29.7	30.2	30.0	26.6	24.5	24.64	30.9	18.3
11.	16.63	15.62	14.69	15.1	1 17-95	20.61	22.54	23.10	22.75	22.3	3 19.94	18.13	19.12	24.14	14.22
7			Rich	tung	(R), Ges	chwind				es in s		in Meter	n		Tages
z z	12 <sup>b</sup>	14 R		tung	(R), Ges	chwind 20 <sup>k</sup> R G	igkeit	01		es în a	Sekunde	in Meter	n 8 <sup>5</sup>	10 <sup>1</sup>	Tages mitte
	R G	H	G R	66 (3	18 <sup>k</sup> R G	20h R G	22 <sup>b</sup> H G	R of	a 2.1 SS	R G	R G SE 2.1	R G	R 0	R	mitte
	R G	R	G R	66 /j	18 <sup>b</sup> R G S o.9 N 2.9 SSW o.4	20h R G S 1.1 N 1.7 SSW 0.8	22 <sup>b</sup> R G SSW 2. N 1. WSW 1	6 SSW 8 N 4 SSW	G 2.1 St	R G	R G SE 2.1 NNW 2.0	R G WNW 1. SSW o. SE 1.	8 W 3.3 ESE 1.6 SE 2.0	N I	mitte G G
	NW 1.0	NW WSW	G R	65 67 8 0.2 7 2.1 7 1.0 E 0.2	18 <sup>h</sup> R G S o.9 N 2.9 SSW o.4 NE o.5	S 1.1 N 1.7 SSW 0.8 NE 0.8	R G SSW 2. N 1. WSW 1.	6 SSW 8 N 4 SSW	G 2.1 St 1.9 NO 1.8 5	26 R G SW 2.2 SW 1.9 SW 1.4 S 3.5	8E 2.1 NNW 2.0 S 1.0 S 2.8	8 G WNW 1. SSW 0. SE 1. S 3.0	8 0 W 3.3 ESE 1.6 SE 2.0 S 2.0	R E I	mitte G G .4 1.5 .0 1.7 .0 1.1
	NW 1.4 NW 1.4 NNE 0.5 0.6 S 1.1	AW WSW	G R 0.0 1.6 NNV 0.9 SSV 0.0 1.6	65 67 8 0.2 7 2.1 7 1.0 E 0.2 S 1.2	8 o.9 N 2.9 SSW o.4 NE o.5 S 1.1	S 1.1 N 1.7 SSW 0.8 NE 0.8 SSW 3.1	8SW 2. N 1. WSW 1. S 3. SW 2.	E SSW 8 N 4 SSW 5 S S SE	G 2.1 St 1.9 NO 1.8 2.1 4.6 2.1	R G SW 2.2 SW 1.9 SW 1.4 S 3.5 SE 2.1	8E 2.1 NNW 2.0 S 1.0 S 2.8 SE 2.1	8 G WNW 1, SSW 0, SE 1, S 3,6 N 2,1	8 W 3.3 ESE 1.6 SE 2.0 S 2.0 N 0.6	R E i o	mitte G G 1.4 1.5 1.0 1.7 1.0 1.1 1.7 2.0 1.6 1.6
	NNE 0.5 S 1.0 NNE 0.5 S 1.1	NW WSW S SSW WNW	G R  0.0 1.6 NNV 0.9 SSV 0.0 NI 1.6 0.4 SI	66 (3) 8 0.2 7 2.1 7 1.0 E 0.2 S 1.2 E 0.4	18 <sup>6</sup> R G S 0.9 N 2.9 SSW 0.4 NE 0.5 S 1.1 SW 0.7 N 0.6	S 1.1 N 1.7 SSW 0.8 NE 0.8 SSW 3.1 NW 0.6	22 <sup>h</sup> H G SSW 2. N 1. WSW 1. S 3. SW 2. N 1.	6 SSW 8 N 4 SSW 5 S S SE O NNW	G 2.1 St 1.9 NO 1.8 2.1 4.6 2.1	R G SW 2.2 SW 1.9 SW 1.4 S 3.5 SE 2.1	8E 2.1 NNW 2.0 S 1.0 S 2.8 SE 2.1	R G WNW 1. SSW 0. SE 1. S 3.5 N 2.1 NE 2.5 NW 2.8	8 0 W 3.3 ESE 1.6 SE 2.0 N 0.6 NNE 1.3	N I E I	mitte G G .4 1.5 .0 1.7 .0 1.1 .7 2.0 .6 1.1 .6 1.1
	S 1.0 NW 1.9 NNE 0.5 0.6 S 1.1 0.6 N 1.1	NW WSW S SSW WNW WNW	G R 0.0 1.6 NNV 0.9 SSV 0.0 NI 1.6 0.4 SI 0.7 V 1.6	66 G 8 0.2 7 2.1 7 1.0 E 0.2 S 1.2 E 0.4 N 0.9 N 1.6	18 <sup>k</sup> R G S 0.9 N 2.9 SSW 0.4 NE 0.5 S 1.1 SW 0.7 N 0.6 NSW 2.6 NSW 2.6	S 1.1 N 1.7 SSW 0.8 NE 0.8 SSW 3.1 NW 0.6 N 2.6 WNW 4.3 N 3.0	R G  SSW 2. WSW 1. S 3. SW 2. N 1. N 0. WNW 3. NNE 2.	6 SSW 8 N 4 SSW 5 S S O SE O NNW 6 NNW N N N N N N N N N N N N N N N	G 2.1 St 1.9 NT 1.8 2 4.6 2.1 1.6 NN 2.4 NN 2.4 NN	26 R G SW 2.2 SW 1.4 S 3.5 SE 2.1 SW 1.1 SW 2.6 SW 2.6 SW 2.6	8E 2.1 NNW 2.0 S 1.0 S 2.8 SE 2.1 WNW 3.2 WNW 2.8 NW 3.1 E 3.0	R G WNW 1. SSW 0. SE 1. S 3.6 N 2.1 NE 2.5 NW 2.3 ENE 2.6	8 W 3.3 ESE 1.6 SE 2.0 S 2.0 N 0.6 S NNE 1.3 WNW 4.7 WNW 2.0 ENE 2.7	N I E I S S S S S S C N N N N N N N C E N E	mitte G G .4 1.5 .0 1.7 .0 1.1 .7 2.0 .6 1.1 .9 2.2 .8 2.4 .1 2.4
	S 1.0 NW 1.9 NNE 0.5 0.6 S 1.1 0.6 N 1.1 NW 1.5 N 1.4 NE 0.6	NW WSW S SSW WNW WNW NNE	G R  0.0 1.6 NNV 0.9 SSV 0.0 1.6 0.4 SI 0.7 1.7 V 1.6 1.6 N	66 (2) 8 0.2 7 2.1 7 1.0 8 0.2 8 1.2 8 0.4 8 0.9 7 1.6 8 1.0 8 0.9 8 1.0 8 0.2	18 <sup>k</sup> R G 8 0.9 N 2.9 SSW 0.4 NE 0.5 S 1.1 SW 0.7 N 0.6 WSW 2.6 N 2.3 ENE 3.2	S 1.1 N 1.7 SSW 0.8 NE 0.8 SSW 3.1 NW 0.6 N 2.6 WNW 4-3 N 3.0 E 3.5	N 1	6 SSW 8 N 4 SSW 5 S S O NEW 6 NNW 6 NNW 6 NNW 6 E	G 1.9 N.7 1.8 5 4.6 2.1 1.6 N.7 2.4 N.7 2.7 N.7 3.5 N.7 2.7	26 R G SW 2.2 NW 1.9 SW 1.4 S 3.5 SE 2.1 (W 1.1 (W 2.6 NE 3.5 E 5.4	R G SE 2.1 NNW 2.0 S 1.0 S 2.8 SE 2.1 WNW 3.2 WNW 2.8 NW 3.1 E 3.0 E 4.4	R G WNW 1 SSW 0 SE 1 S 3.6 N 2 NE 2.8 NW 2.3 ENE 2.6 E 3	R 0 W 3.3 ESE 1.6 SE 2.0 S 2.0 N 0.6 NNE 1.3 WNW 4.7 NNE 2.0 ENE 2.7	N I E I SSE O SSE O N O S I SSE O SS	mitte G G 1.4 1.5 1.0 1.7 1.0 1.1 1.7 2.0 1.6 1.6 1.6 1.1 1.9 2.2 2.8 2.4 1.1 2.4 1.5 2.7
	N G  S 1.0  NN 1.2  NNE 0.0  S 1.1  0.0  N 1.1  NW 1.5  N 1.4  NE 0.0  BNE 1.0	NW WSW SSW WNW WNW NNE	G R  0.0 1.6 NNV 0.9 SSV 0.0 NI 1.6 0.4 SI 0.7 1.7 V 1.6 NI 1.6 NI	66 67 77 1.0 E 0.2 E 0.4 N 0.9 N 1.0 E 2.0 E 1.0 E 1.0 E 1.0 E 1.0	S 0.9 N 2.9 SSW 0.4 NE 0.5 S 1.1 SW 0.7 N 0.6 N SW 2.6 N	S 1.1 N 1.7 SSW 0.8 NE 0.8 SSW 3.1 NW 0.6 N 2.6 WNW 4.3 E 3.5 ENE 2.8 E 2.0	22h R G SSW 2. N 1. S 3. SW 2. N 1. N 0. W N W 3. N E 2. E 2. E 3. F 3.	6 SSW 8 N 8 SSW 5 S SE S S SE S S S SE S S S SE S S S S	G 1.8 2.1 1.9 NN 1.8 2.4 NN 2.4 NN 2.0 N 3.5 N	25 R G SW 2.2 SW 1.9 SW 1.4 S 3.5 SE 2.5 SW 1.1 IW 3.0 (W 2.6 NE 3.5 E 5.4	R G  SE 2.1 NNW 2.0 S 1.0 S 2.8 SE 2.1 WNW 3.2 WNW 2.8 NW 3.1 E 3.0 E 4.4 E 3.2 ESE 2.2	R G WNW 1. SSW 0. SE 1. S 3.6 N 2.1 NW 2.3 NW 2.3 NW 2.3 ENE 2.6 E 3.1	8 W 3.3 ESE 1.6 SE 2.0 N 0.6 NNE 1.3 WNW 4.7 NNE 2.0 ENE 2.7 NE 2.0	R  N 1 E 1 C S 2 SSE C WNW 1 NNE C ENE 1 ESE 2 ESE	mitte G G 1.4 1.5 1.0 1.7 2.0 1.1 2.7 2.0 3.6 1.6 3.9 2.2 3.8 2.4 4.1 2.4 1.5 2.7 1.3 2.7
	N G  S 1.0  NW 1.0  NNE 0.0  S 1.1  NW 1.5  N 1.1  NE 0.0  ENE 1.0  ENE 1.0	NW WSW S SSW WNW NN NN NN E NNE NN E	G R  0.0 1.6 NNV 0.9 SSV 0.0 NI 1.6 0.4 SI 0.7 1.7 V 1.6 NI 1.6 NI 1.6 NI 1.7 NI	65 (3) 8 0.2 7 2.1 7 2.1 8 0.2 8	18 <sup>6</sup> G S 0.9 S 0.9 S 80.9 S S W 0.4 NE 0.5 S 1.1 S W 0.7 N 0.6 WSW 2.6 V N 2.3 ENE 3.2 ENE 1.7 ESE 1.9	20 <sup>h</sup> R G S 1.1 N 1.7 SSW 0.8 NE 0.8 SSW 3.1 NW 0.6 N 2.6 WNW 4.3 N 3.0 E 3.5 ENE 2.8 E 2.0 SSE 0.8	R G SSW 2. N 1. S 3. SW 2. N 1. N 0. N 1. N 1. N 2. E 2. E 3. E 4. SSE 1.	6 SSW 8 N 4 SSW 5 S S S S S S S S S S S S S S S S S	G 2.1 St 1.9 NT 1.8 5.4.6 2.1 1.6 NN 1.2.4 NN 2.0 7 3.5 NO 2.7 4.0 E 5.0 E	25 R G SW 2.2 SW 1.4 S 3.5 SE 2.1 SW 1.1 SW 2.6 SW 1.4 SW 2.6 SE 3.5 SE 3.4 SE 3.4	R G  NE 2.1 NNW 2.0 S 1.0 S 2.8 SE 2.1 WNW 3.2 WNW 2.8 NW 3.1 E 3.0 E 4.4 ESE 3.2 ESE 3.2	R G WNW 1. SSW 0. SE 1. S 3.6 N 2.1 NW 2.2 N 3.6 E 3.1 E 4. E 5.	8 0 W 3.3 ESE 1.6 S 2.0 S 2.0 NNE 1.3 WNW 4.7 NNE 2.0 ENE 2.0 ENE 2.0 ENE 2.0 ENE 2.0	N I E I I I I I I I I I I I I I I I I I	mitte G G .4 1.5 .0 1.7 2.0 1.6 .7 2.0 .6 1.6 .9 2.2 .8 2.4 .1 2.4 .5 2.7 .1 3.4 .9 3.9 .9 3.9 .9 3.9 .9 3.9 .0 3.7 .0 3.7
	R G  S 1.6  NW 1.9  NNE 0.6  S 1.1  0.6  N 1.1  NW 1.5  N 1.4  NE 0.6  ENE 1.6  ENE 1.6	NW WSW S SSW WNW WNW NNE E NNE NNE NNE NNE NNE NNE	G R  0.0 1.6 NNV 0.9 SSV 0.0 NI 1.6 0.4 SI 0.7 1 1.7 V 1.6 NI 1.6 NI 1.6 NI 1.7 NI 0.5 NNI 1.7 NI	66 67 77 1.0 E 0.2 E 0.4 N 0.9 N 1.0 E 2.0 E 1.0 E 1.0 E 1.0 E 1.0	18 <sup>6</sup> R G S 0.9 S 0.9 S 2.9 S S W 0.4 NE 0.5 S 1.1 S W 0.7 N 0.6 W S W 2.6 V 2.3 ENE 3.2 ENE 1.7 ESE 3.0 NNE 0.9	S 1.1 N 1.7 SSW 0.8 NE 0.8 SSW 3.1 NW 0.6 N 2.6 WNW 4.3 E 3.5 ENE 2.8 E 2.0	R G SSW 2. N 1. S 3. SW 2. N 1. N 0. N NW 3. NNE 2. E 2. E 4. SSE 1. ENE 2.	6 SSW 8 N 4 SSW 5 S S O SE C NNW NNW 1 NW 1 NW 1 NW 2 ENE ENE ENE 2 ENE 2 ENE 2 ENE 2 ENE	G 2.1 S2 1.9 N2 1.8 4.6 2.1 1.6 NN 2.4 NN 2.5 N 2.7 4.0 E 1.8 E 1.8 E 2.6 E 2.6 E	25 R G SW 2.2 SW 1.9 SW 1.4 S 3.5 SE 2.1 SW 2.6 W 2.6 NE 3.5 E 5.4 NE 3.3 SE 3.4	R G  SE 2.1 NNW 2.0 S 1.0 S 2.8 SE 2.1 WNW 3.2 WNW 2.8 NW 3.1 E 3.0 E 4.4 E 3.2 ESE 2.2	R G WNW 1. SSW 0. SE 1. S 3.6 N 2.1 NW 2.3 NW 2.3 NW 2.3 ENE 2.6 E 3.1	R O  W 3.3 ESE 1.6 SE 2.0 S 2.0 N.E 1.3 WNW 4.7 NNE 2.0 ENE 2.7 NE 2.0 ESE 2.4 NNE 2.5 ESE 2.4 NNE 2.5 ESE 2.4 NNE 2.5 ESE 2.4	N I S I S I S I S I S I S I S I S I S I	mitte G G 1.4 1.5 1.0 1.7 1.0 1.7 1.0 1.7 1.0 1.7 1.0 1.1 1.1 1.2 2.4 1.3 2.7 1.3 2.7 1.3 2.7 1.3 2.7 1.3 2.7 1.3 2.7 1.4 2.4 1.5 2.7 1.6 2.7 1.7 2.0 1.8 2.4 1.9 2.2 1.9 2 1.9 2
	R G  S 1.0  NW 1.5  NNE 0.5  S 1.1  0.0  N 1.1  NW 1.5  N 1.4  NE 0.0  ENE 1.0  ENE 1.0  ENE 0.8  E 0.8  E 0.8	R NW WSW S SSW WNW NNE NE	G R  0.0 1.6 NNV 0.9 SSV 0.0 1.6 SI 1.6 NI 1.7 NI 1.8 NI 1.7 NI 1.8 NI 1.8 NI 1.9 NI 1.9 NI 1.9 NI 1.0 NI 1	66 // / / / / / / / / / / / / / / / / /	18 <sup>b</sup> R G S S S S S S S S S S S S S S S S S S	20 <sup>h</sup> R G  S 1.1 SSW 0.8 NE 0.8 SSW 3.1 NW 0.6 N 2.6 WNW 4.3 N 3.0 E 3.5 ENE 2.8 ENE 1.4 ENE 2.2 NE 0.9	R G  SSW 2.  SSW 2.  WSW 1.  S 3.  SW 2.  N 1.  N 0.  N WSW 3.  N 0.  E 2.  E 3.  E 4.  SSE 1.  ENE 2.  S 3.  ESE 2.	6 SSW 8 N SSW 5 S S SE NNW 6 NNW NW 5 N S S S S S S S S S S S S S S S S S S	2.1 St 1.9 NO 1.8 2 4.6 2.1 1.6 NN 2.0 N 3.5 N 2.7 4.0 E 1.8 2.6 E 3.5 E	26 R G SW 2.2 SW 1.9 SW 1.4 S 3.5 SE 2.1 SW 2.6 NE 3.5 E 5.4 NE 3.3 SE 3.4 E 3.4 SE 4.77 SE 2.4	R G  SE 2.1 NNW 2.0 S 1.0 S 2.8 S 2.8 WNW 3.2 WNW 3.2 WNW 3.1 E 3.0 E 4.4 E 3.2 E SE 3.2 E SE 2.8 E SE 2.8	R G WNW 1 SSW 0 SS 1 S 3 NE 2 NE 2 N 3 ENE 2 ENE 2 ENE 2 ENE 2 ENE 2 ENE 2	R O SE 2-0 SE 2-0 SE 2-0 SE 2-0 SE 2-0 SE 2-0 SE 2-7 SE 2-5 SE 2-4 SE 2-7 SE 2-	R  N   E   1   C   S   S   S   C   S   C   C   C   C	mitte  G G  1.4 1.5 1.0 1.7 1.0 1.7 1.0 1.6 1.6 1.6 1.1 1.7 2.0 1.6 1.6 1.8 2.4 1.1 2.4 1.4 2.4 1.4 2.4 1.4 2.4 1.4 2.4 1.4 2.4 1.4 2.4 1.4 2.4 1.4 2.4 1.4 2.4 1.4 2.4 1.4 2.
	R G  S 1.0  NW 1.5  NNE 0.5  S 1.1  NNE 0.5  S 1.1  NW 1.5  N 1.4  NE 0.6  ENE 1.0  ENE 1.0  ENE 0.6  ENE 0.6  ENE 0.6  ENE 0.6  ENE 0.7	NW WSW SSSW WNW WNW NNE NE	G R  0.0 1.6 NNV 0.0 9 NV 0.0 1.6 1.6 1.6 1.6 1.6 1.7 NN 1.6 1.7 NN 0.5 NNI 1.7 N 0.8 ENI 0.3 NV 0.9 NV	66 (7) 8 0.2 7 2.1 7 1.0 8 0.2 8 1.2 8 0.9 7 1.0 8	18 <sup>h</sup> R G  S 0.9 N 2.9 N 2.9 SSW 0.4 NE 0.5 S 1.1 SW 0.7 N 0.6 N 2.3 ENE 1.7 ENE 1.7 ENE 1.7 ENE 0.9 ENE 0.9 ENE 0.5 NW 0.4 W 0.6 S 1.0	20th R G S 1.1 N 1.7 SSW 0.8 NB 0.8 SSW 3.1 NW 0.6 NN 4.3 N 3.0 E 3.5 ENE 2.8 ENE 2.8 ENE 2.2 NE 0.9 X 1.9	22b R G SSW 2. N 1. WSW 1. S 3. SW 2. N 1. N 0. WNW 3. NNE 2. E 2. E 3. SSE 1. ENE 2. S 3. ESE 2. NNE 1.	6 SSW 8 N 8 SSW 5 S S S S S S S S S S S S S S S S S	G 1.9 N.3 1.8 5 4.6 1.9 N.3 1.8 5 4.6 1.9 N.3 1.8 1.9 N.3 1.8 1.9 1.9 1.9 1.9 1.9 1.9 1.9 1.9 1.9 1.9	26 R G SW 2.2 SW 1.9 SW 1.4 S 3.5 SE 2.4 SE 3.4 SE 3.4 SE 3.4 SE 3.4 SE 3.4 SE 3.4 SE 2.4 SE 2.4	B G  NE 2.1 NNW 2.0 S 1.0 S 2.8 S 2.8 S 2.8 S 2.1 WNW 3.2 WNW 2.8 NNW 3.1 E 3.0 E 4.4 E 3.2 E 5.6 E 3.2 E 5.6 E 3.2 E 5.6 E 3.2 E 5.6 E 3.4 E 5.7 E 5.6 E 5.8 E 5.	R G WNW 1 SSW 0 SS 1 S 3 NE 2 NE 2 N 3 ENE 2 ENE 2 ENE 2 ENE 2 ENE 2 ENE 2	R O SE 2-0 SE 2-0 SE 2-0 SE 2-0 SE 2-0 SE 2-0 SE 2-7 SE 2-5 SE 2-4 SE 2-7 SE 2-	R  N   E   1   S   S   S   S   C   S   S   C   S   C   S   C   S   C   S   C   S   C   S   C   S   C   S   C   S   C   S   C   S   C   S   C   S   C   S   C   S   C   S   C   S   C   S   C   C	mitte G G 1.4 1.5 1.0 1.7 1.0 1.7 1.7 2.0 1.6 1.6 1.9 2.2 1.8 2.4 1.1 2.4 1.1 2.4 1.1 2.4 1.2 2.7 1.3 2.7 1.3 2.7 1.3 2.7 1.4 2.9 1.5 2.7 1.5 2.7 1.6 2.8 2.4 1.7 2.0 1.8 2.4 1.9 2.2 1.9 2.2 1.0 2.0 1.0 2
	R G  S 1.0  NW 1.2  NNE 0.5  S 1.1  NW 1.5  N 1.4  NE 0.6  ENE 1.6  ENE 0.4  ENE 0.5  S 1.7  NE 0.6  ENE 0.7  ENE 0.8  E	NW WSW WNW NNE NE	G R  0.0 1.6 NNV 0.9 SSV 0.0 NI 1.6 SI 0.7 1 1.6 NI 1.7 NI 1.6 NI 1.7 NI 0.5 NNI 1.7 NI 0.5 ENI 0.7 NV 0.9	66 67 77 1.0 E 0.2 E 0.4 E 1.0	8 0.9 N 2.9 SSW 0.4 NE 0.5 S 1.1 SW 0.7 N 0.6 WSW 2.6 V 2.3 ENE 1.7 ENE 3.0 NNE 0.9 ENE 0.5 NW 0.4 W 0.6 S 1.0 NW 0.4	20th R G S 1.4 N 1-7 SSW 0.8 NE 0.8 SSW 3.1 NW 0.6 N 2.6 WNW 4.3 N 3.0 E 3.5 ENE 2.8 ENE 1.8 ENE 2.0 NE 0.9 N 1.9 S 0.4	22b R G SSW 2. N 1. S 3. SW 2. N 1. S 3. NN 0. WNW 3. NNE 2. E 2. E 4. SSE 1. ENE 2. S 3. ESE 2. NNE 3.	6 SSW 8 N SSW 5 S S S S S S S S S S S S S S S S S	G 1.9 N7 1.8 5 1.9 N7 1.9 N	8W 2.2 8W 1.9 8W 1.9 8W 1.4 S 3.5 SE 2.1 6W 1.1 6W 2.6 6W 2.6 6W 2.6 6W 2.6 6W 2.6 6W 2.6 8E 3.4 8E 3.4 8E 3.4 8E 3.4 8E 2.4 NE 3.6 8E 2.4 NE 4.0 6W 4.5 NE 4.0	B G  SE 2.1  NNW 2.0  S 1.0  S 2.5  SE 2.1  WNW 3.2  WNW 3.1  E 3.0  E 4.4  E 3.2  ENE 3.4	R G WNW 1 SSW 0 SE 1 S 3.6 N 2 NE 2.5 NW 2.2 NE 2.5 NE 2.6 E 3 E 4.6 E 5 E 4.6 E 3 E 4.6 E 5 E 5 E 5 E 5 E 6 E 7	R 0  W 3-3  S ESE 1-6  SE 2-0  N 0-6  SNE 1-3  WNW 4-7  NNE 2-0  ENE 2-7  NE 2-0  ENE 2-7  ENE 2-1  T NNE 2-0  ENE 2-7  ENE 2-1  ENE 2-1  ENE 2-2  ENE 2-1  ENE 2-2	R	mitte  G G  1.4 1.5 1.7 1.0 1.7 1.7 2.0 1.6 1.1 1.9 2.2 1.8 2.4 1.5 2.7 1.1 2.
	R G  S 1.0  NW 1.2  NNE 0.5  S 1.1  NW 1.5  N 1.4  NE 0.6  ENE 1.6  ENE 0.6	R NW WSW S SSW WNW NNE E NE	G R  0.0 0.9 NSV 0.0 0.1 1.6 0.4 SI 0.7 1 1.6 0.4 SI 0.7 1 1.7 N 0.5 NNI 1.7 N 0.8 ENI 0.9 NV	66 67 7 2.1 Y 2.1 Y 2.2 S 1.2 E 0.4 Y 1.0 E 2.0 E 1.0	18 <sup>k</sup> G S 0.9 N 2.9 SSW 0.4 NE 0.5 S 1.1 SW 0.7 A 0.6 WSW 2.6 V 2.3 ENE 3.2 NE ENE 3.2 NE ENE 3.2 NNE 0.9 ENE 0.9 ENE 0.9 ENE 0.9 S 1.0 S	20h R G S 1.1 N 1.7 SW 0.3 NE 0.8 SSW 3.1 NW 0.6 N 2.6 WNW 4.3 N 3.0 E 3.5 ENE 2.8 E 2.0 SSE 0.8 E 2.0 E 0.9 E 0	22b R G SSW 2. N 1. WSW 1. S 3. SW 2. N 1. N 0. WNW 3. NNE 2. E 5. E 4. SSE 4. SSE 2. NNE 3. WSW 3. SSE 2. NNE 2. SSE 3. SSE 2. NNE 2.	6 SSW 8 SSW 5 S S S S S S S S S S S S S S S S S	G 2.1 S2 1.9 NO 1.8 1.8 1.6 NN 2.0 N NO 2.1 1.6 NN NO 2.0 N NO 2.0	26 G SW 2.2 SW 1.9 SS 3.5 SE 2.1 GW 2.6 NE 3.5 E 5.4 SE 3.4 SE 4.7 SE 2.4 SE 2.4 SE 2.4 SE 2.4 SE 2.4 SE 2.4 SE 3.4 SE 3.	R G  NE 2.1 NNW 2.0 S 1.0 S 2.5 S 5E 2.1 WNW 3.2 WNW 3.8 NW 3.1 E 3.0 E 4.4 ENE 3.2 ENE 3.4 ENE 4.0 S 2.8 ENE 2.1 NN 3.1 E 3.0 E 4.4 ENE 3.4 ENE 2.1 NN 3.1	R G WNW 1 SSW 0 SSW 0 S 3 S 3 N 2 NW 2.2. N 3 ENE 2 E 4 E 52 E 4 E 52 E 53 E 54 E 52 E 53 E 54 E 54 E 54 E 54 E 54 E 54 E 54 E 55 E 56 E 56	R 0 R 0 3 W 3.3 ESE 1.6 S 2.0 S 2.0 S N 0.6 S NNE 1.3 WNW 4.7 NNE 2.0 ENE 2.7 ENE	N I E I I I I I I I I I I I I I I I I I	mitte  G G  4 1.57  .0 1.7 2.0  .0 6 1.1  .0 9 2.2  .0 1.5 2.7  .1 2.4  .1 2.4  .1 2.7  .1 3.4  .1 2.6  .1 1.6  .2 1.6  .2 1.6  .3 2.7  .1 3.4  .5 2.7  .1 3.4  .5 2.7  .1 3.4  .5 2.7  .1 3.4  .5 2.7  .1 3.4  .5 2.7  .1 3.4  .5 2.7  .1 3.4  .5 2.7  .6 1.9  .7 2.1  .6 1.9  .7 2.1  .6 1.9  .7 2.1  .7 2.1  .8 2.0  .7 2.1  .8 2.0  .8 2.0  .9 2.0  .9 3.0
	R G  S 1.0  NW 1-1  NNE 0.5  S 1.1  NW 1-5  N 1-1  NW 1-5  NW 1-	R NW WSW S SSW WNW WNW NNE NNE NE N	G R  0.0 1.6 NNV 0.9 SSV 0.0 1.6 SSV 0.7 1.7 V 1.7 V 1.6 NI 1.6 NI 1.6 NI 1.7 NI 0.5 NNI 1.7 NI 0.5 NNI 1.7 NI 0.5 NV 0.9 WNV 1.2 V 0.4 0.5 SSV 0.4 0.9 WNV	8 0.2 7 2 1.0 8 0.2 7 2 1.1 8 0.2 7 2 1.1 8 0.2 8 0.2 8 0.2 8 0.2 8 1.2 8 0.2 8 1.2 8 0.2 8 1.2 8 1.0 8 1	18 <sup>k</sup>   R   G   S   0.9   N   2.9   S   W   0.4   N   0.5   S   1.1   S   W   0.7   N   2.3   ENE   3.2   ENE   1.7   ENE   2.0   N   0.9   ENE   0.9   ENE   0.5   S   1.0   N   W   0.4   W   0.6   S   1.0   N   0.5   1.0   N   0.5   1.0   N   0.5   1.0   S   0.5	R G  S 1.1 N 1.7 S W 0.3 N 0.3 N 0.6 N 2.6 N 2.6 N 2.6 S E 2.0 S E 2.0 S E 2.0 S E 2.0 S E 2.1 N 0.9 S 0.4 N 2.1 S S W 0.6 S W	22b R G SSW 2. N 1. WSW 1. S 3. SW 2. N 1. N 0. WSW 3. NNE 2. E 2. E 3. E 4. SSE 1. ENE 2. S 3. WNW 2. NNE 3. WNW 3.	8 SSW 4 SSW 5 SE SE SE SE SE SE SE NNEW NNEW NNE SSE SE SE SE NNEW NNE SSE SSE SSE SSE SNEW NNE SSE SSE SSE SSE SNEW NNE SSE SSE SSE SSE SSE SNEW NNE SSE SSE SSE SSE SSE SSE SSE SNEW NNE SSE SSE SSE SSE SSE SSE SSE SSE SSE	G 2.1 St. 1.9 NY. 1.8 4.6 2.1 1.6 NN 2.0 NY. 2.7 4.0 E 2.6 E 2.6 E 2.6 E 2.6 E 2.6 WN 1.6 2.5 3.0 WN 1.6 E 2.5 WN 1.6 WN	25 G SW 2.2 SW 1.9 SW 1.4 S 3.5 SE 2.1 SW 2.6 W 2.6 W 2.6 SE 3.4 SE 3.4	R G  SE 2.1 NNW 2.0 S 1.0 S 2.8 S 2.1 WNW 3.2 WNW 2.8 NNW 3.1 E 3.0 E 4.4 E 3.2 E SE 1.2 E SE	R G WNW 1 SSW 0 SE 1 5 3 N 2 NE 2 NW 2 X 3 ENE 2 E 3 E 4 E 5 E 5 NE 2 NNE 2	R 0  W 3.3  ESE 1.6  SE 2.0  S 2.0  S NE 1.3  WNW 4.7  NE 2.0  ENE 2.7  NE 2.0  ENE 2.7  NE 2.0  ENE 2.7  NE 2.0  ENE 2.7  ENE 2.0	R  N   E   1  S   E   1  SSE   C    NNW   1  ENE   C	mitte  G G  1.4 1.5 1.0 1.7 1.7 1.7 1.7 1.7 1.7 1.7 1.7 1.7 1.7
	R G  S 1.0 NW 1.2 NNE 0.5 S 1.1 0.6 N 1.1 NN 1.5 N	R NW WSW S SSW WNW WNW NNE NNE NE N	G R  0.0 0.9 SSV 0.0 0.9 SSV 0.0 1.6 SI 1.6 SI 1.6 SI 1.7 V 1.7 V 1.6 SI 1.7 SI 0.5 SI 0.2 V 0.9 SSV 0.2 V 0.9 SSV 0.9	66 / (7 ) S 0.2 Y 2.1 1 (7 ) S 0.2 Y 2.1 1 (7 ) S 0.2 Y 2.1 1 (7 ) S 1.2 E 0.2 E 1.0 E 2.0 E 1.0 E 2.0 E 1.0 Y 0.6 E 1.0 Y 0.6 Y 0.7 S 0.6 Y 0.8	18 <sup>k</sup>   R   G   S   O   O   N   2   O   S   N   2   O   S   N   O   O   O   O   O   O   O   O   O	R G  S 1.1 8 1.7 8	R G SSW 2. WSW 1. S 3. SW 2. N 1. N 3. N 1. N 1. N 1. S 3. SW 2. N 2. N 2. N 2. N 3. N 3. SW 2. N 4. SW 3. SW 4. SW 4. SW 4. SW 4. SW 4. SW 4. SW 5. SW 6. SW 6. SW 6. SW 7. S	8 SSW 8 SN 8 SSW 8	2.1 St. 1.9 N.2 1.9 N.2 1.8 4.6 1.8 4.6 1.8 2.4 N.2 2.5 N.2 2.7 N.2 2.	R G SW 2.2 SW 1.9 SW 1.4 S 3.5 SE 2.1 SW 3.0 SW 2.6 SW 2.6 SE 3.4 SE 3.4 SE 3.4 SE 2.4 NE 3.5 SE 2.4 NE 3.4 SE 2.4 SE 2.4	R G C SE 2.1 NNW 2.0 S 1.0 S 2.8 S 2.1 WNW 3.2 S NNW 3.1 E 3.0 E 4.4 S 2.5 ENE 4.0 SE 2.8 ENE 4.0 ENE 3.2 ENE 2.8 ENE 2.1 NNE 2.7 ENE 3.8 ENE 2.1 NNE 2.7 ENE 3.8 ENE 2.1 NNE 2.7 ENE 3.8 ENE 3.1 NNE 2.7 ENE 3.0 ENE	R G WNW 1 SSW 0 SS 1 S 3 N 2 NW 2 NW 2 NW 2 E 3 E 4 ESE 2 NNE 2 E 3 E 4 ESE 2 NNE 2 E 3 E 4 E 2 NE 3 W 2 E 2 NE 3 W 2 E 5 NW 2 NW 2 NW 2	R S G S S S S S S S S S S S S S S S S S	R	mitte  G G  1.4 1.5 1.0 1.7 1.0 1.7 1.0 1.7 1.0 1.6 1.6 1.6 1.6 1.9 2.2 1.8 2.7 1.3 2.7 1.1 2.4 1.9 1.9 1.9 1.9 1.9 1.9 1.1 2.1 1.1 2.1 1.1 2.1 1.2 2.1 1.3 2.7 1.3 2.7 1.3 2.7 1.3 2.7 1.3 2.7 1.3 2.7 1.4 2.0 1.9 1.
	R G  S 1.0  NW 1-1  NNE 0.5  S 1.1  NW 1-5  N 1-1  NW 1-5  NW 1-	R NW WSW S SSW WNW WNW NNE NNE NE N	G R  0.0 1.6 NNV 0.9 NSV 0.0 NSV 1.6 S 0.7 S 1.6 NN 0.7 S 1.6 NN 0.5 NN 1.7 N 0.5 NN 1.7 N 0.5 NN 0.2 V 0.0 NV 0.2 V 0.3 NV 0.2 V 0.4 O 0.5 SSV 0.2 V 0.0 NN 0.2 V 0.	66 / (7 ) 8 0 . 2 1 / (7 ) 1 /	18 <sup>b</sup>   R   G   S   O   O   N   2   O   S   W   O   O   O   O   O   O   O   O   O	R G  S 1.1 N 1.7 S W 0.3 N 0.3 N 0.6 N 2.6 N 2.6 N 2.6 S E 2.0 S E 2.0 S E 2.0 S E 2.0 S E 2.1 N 0.9 S 0.4 N 2.1 S S W 0.6 S W	R G SSW 2. N 1. SSW 2. N 1. SSW 2. N 1. NN W 3. NN 2. E 2. E 3. E 4. SSE 1. ENE 2. NN 2. NN 2. NN 3. NN 2. ENE 1. NE 1. NE 1. NN 2. ENE 1. E 1. NN 4. E 2. E 2. E 3. E 4. E 4. E 5. E 5. E 4. E 5. E 5. E 6. E 7. E 1. E 1	8 SSW 4 SSW 5 SE	G 2.1 S2 1.9 N2 1.8 4.6 1.8 1.6 N8 2.7 N. 2.	R G SW 2.2 SW 1.4 S 3.5 SE 2.1 SE 3.5 SE 3.5 W 1.1 W 2.6 SE 3.5 NE 3.5 SE 3.4 NE 3.5 SE 3.4 NE 3.5 SE 3.4 NE 3.5 SE 2.1 SE 4.7 SE 2.4 SE 4.7 SE 2.4 SE 4.7 SE 2.4 SE 4.7 SE 2.4 SE 4.7 SE 2.4 SE 4.7 SE 4.7 S	R G  SE 2.1 NNW 2.0 S 1.8 S 2.8 S 2.8 WNW 3.8 WNW 3.8 WNW 3.8 WNW 3.8 E 3.0 E 4.4 E 3.2 E SE 1.9 E NE 3.6 E NE 2.1 E NE 3.7	R G WNW 1. SSW 0. SE 1. S3. S 3. S 3. S 3. S 3. S 3. S 3. S	8 W 3.3 S E 1.6 S E 2.0 S E 2.0 S E 2.7 S E 2.0 E S E 2.7 S E 2.7 S E S E 2.7	R  N   E   1     C   S   2   S   S   C   C	mitte  G G  1.4 1.55 1.7 2.00 1.6 1.1 1.9 2.2 2.6 1.6 1.6 2.7 2.1 2.9 2.7 1.1 2.4 2.7 2.7 1.1 2.4 2.7 2.7 1.1 2.4 2.7 2.7 1.1 2.4 2.7 2.7 1.1 2.4 2.7 2.7 1.1 2.4 2.7 2.7 1.1 2.4 2.7 2.7 1.1 2.4 2.7 2.7 1.1 2.4 2.7 2.7 2.7 2.7 2.8 2.0 2.9 2.0 2.9 2.0 2.0 2.5
	N G  S 1.0  NW 1.5  NNE 0.5  S 1.1  0.6  S 1.1  0.6  N 1.1  NW 1.5  N 1.1  NE 0.6  ENE 1.5  ENE 1.6  ENE 0.8  ENE 0.8  ENE 0.8  ENE 0.8  SW 0.6  ESE 0.5  NW 3.4  NWW 3.4  NWW 3.4  NWW 3.4  NWW 3.4  ESE 2.5	R  NW WSW S SSW WNW NNE NNE NE N	G R  0.0 1.6 NNV 0.9 SSV 0.0 1.6 SI 0.7 V 1.7 V 1.7 N 0.5 NNI 1.7 N 0.5 ENI 0.	66 / (7 ) 8 0 . 2 (7 ) 1 . 0 (8 ) 1 . 0 . 0 (8 ) 1 . 0	S   S   O   S   N   O   S   N   O   S   N   O   S   N   O   N   O   S   N   O   S   N   O   S   O   S   O   O   S   O   O   S   O   O	20h R G S 1.1 N 1.7 SSW 0.8 NE 0.8 SSW 3.1 NW 0.6 N 2.6 WNW 4.3 N 3.0 ENE 2.8 ENE 1.4 ENE 1.4 ENE 2.4 ENE 2.4 ENE 2.4 ENE 2.5 SSW 0.6 SSW 0.6 SSW 0.6 ENE 2.8 ENE 0.8	R G SSW 2. N 1. WSW 1. SW 2. N 1. SW 2. N 1. SW 2. N 2. N 2. N 3. NNE 2. E 3. SSE 4. SSE 4. SSE 1. NNE 3. WSW 2. NNE 3. WSW 2. NNE 3. WSW 2. NNE 3. WSW 2. NNE 1. NE 1. NE 1. SSE 1. SSE 1.	R 6 SSW 8 SN 8 SW 5 S S S S S S S S S S S S S S S S S	G 2.1 St. 1.9 N. 1.8 St. 4.6 N. 1.8 St. 4.6 N. 1.6	25 R G  SW 2.2  SW 1.9  SW 1.4  SS E 2.1  WW 2.0  SS E 2.1  WW 3.0  SS E 3.4  E 3.4  E 3.4  SE 2.4	R G G S 1.0	R G WNW 1 SSW 0 SE 1 NE 2 NE 2 NE 2 NE 2 E 4 E 5 E 4 E 8 E 9 NE 2 NE 3	R 0 0 3.3 3 ESE 1.6 5 SE 2.0 5 SE 2.0 5 SE 2.7 5	R	mitte
1 2 2 3 3 4 4 5 5 5 7 7 7 8 3 3 3 4 4 5 5 5 7 7 7 7 8 3 3 3 3 4 4 5 5 5 7 7 7 8 3 3 3 3 4 4 5 5 5 7 7 8 3 3 3 3 3 4 4 5 5 5 7 7 7 8 3 3 3 3 3 4 4 5 5 5 7 7 8 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3	N G  S 1.0  NW 1.5  NNE 0.5  S 1.1  0.6  S 1.1  0.6  N 1.1  NW 1.5  N 1.1  NE 0.6  ENE 1.5  ENE 1.6  ENE 0.8  ENE 0.8  ENE 0.8  ENE 0.8  SW 0.6  ESE 0.5  NW 3.4  NWW 3.4  NWW 3.4  NWW 3.5  ESE 2.5  ESE 2.5  ESE 0.5  ESE 2.5  ESE 0.5  ESE 2.5  ESE 0.5  ESE 2.5  ESE 0.5  ESE 2.5  ESE 2.5  ESE 0.5  ESE 2.5  ESE 2.5  ESE 0.5	NW WSW NN NNE SEE SAW NN	G R  0.0 1.6 NNV 0.0 1.6 NNV 0.0 1.6 Si 0.7 1.6 Si 1.7 1.6 NN 1.7 1.6 NN 1.7 1.6 NN 1.7 1.6 NN 1.7 1.7 1.7 1.8 SW 1.7 1.9 1.9 1.9 1.9 1.9 1.9 1.9 1.9 1.9 1.9	66 / (3	S   S   C   S   C   S   C   S   C   S   C   S   C   S   C   S   C   C	20t R G  S 1.4 N 1.7 SSW 0.8 NE 0.8 SSW 3.1 N 4.3 N 4.	R G G SSW 2.  SSW 2. N 1. WSW 1. S 3. SW 2. N 1. N 0. N NNE 2. E 5. E 4. SSE 1. ENE 2. NNE 3. WNW 2. NE 1. NE 1. NNE 2. SSW 2. SSW 1.	R   SSW   S   S   S   S   S   S   S   S	2.1 St. 1.9 N. 1.8 4.6 4.6 4.6 4.6 4.6 4.6 4.6 7.1 1.6 N. 1.8 2.6 E. 2.7 4.0 E. 2.6 E. 2.6 E. 3.3 4.0 N. 1.6 3.5 N. 1.6 N	R G G SW 2.2 SW 1.9 SW 1.4 SE 2.4 SE	R G  NE 2.1 NNW 2.0 S 1.0 S 2.8 SE 2.1 WNW 3.2 WNW 3.2 WNW 3.5 E 4.4 E 5.0 E 4.8 E 7.2 E 8 2.8 E 8 2.8 E 8 3.2 E 8 6 1.9 E 8 3.2 E 8 6 1.9 E 8 3.2 E 8 6 1.9 E 8 6 3.2 E 8 6 1.9 E 8 6 1.0 E 1.0	R G  WNW 1. SSW 0. SSE 1. S 3.6 N 2. N 2. N 3. E 4. ESE 2. N 2. N 3. E 4. ESE 2. N 2. N 2. N 2. N 3. E 4. ESE 2. N 2. N 2. ESE 2. N 2. N 2. ESE 2. N 2. N 2. ESE 3. N 3. E 4. N 2. ESE 3. N 3. E 4. N 5. N 5. N 6. E 7. N 7. N 5. N 7. N 5. N 7. N 5. N 8. E 7. N 8. E 8. E 8. N 8. E	R 0 3-3 6 ESE 2-6 6 ESE 2-7 NNE 2-1 6 ESE 2-7 NNE 2-1 6 ESE 2-7 NNE 2-6 ESE 2-7 NNE 2-7 ESE 2-7 NNE 2-7 ESE 2-7 NNE 2-7 ESE 2-7 NNE 2-7 ESE 2-7 ESE 2-7 NNE 2-7 ESE 2-	R  N     E     S     SSE     N     SSE     N     N     E	mitte  G G  G 1.7  .0 1.7  .0 2.0  .0 1.1  .7 2.0  .0 6 1.1  .7 2.0  .8 2.4  .1 2.4  .1 2.4  .1 2.4  .1 2.4  .1 2.4  .1 2.4  .1 2.4  .1 2.4  .1 2.5  .7 2.1  .3 2.7  .
	R G  S 1.0  NW 1.5  NNE 0.5  S 1.1  NW 1.5  NW 0.6  ENE 0.5  SW 0.6  ESE 0.5  NW 0.6  ESE 0.5  NW 0.6  ESE 0.5  SW 1.5  SSW 1.5  SSW 1.5	AWWWWWWWWWWWWWWWWWWWWWWWWWWWWWWWWWWWWW	G R  0.0 1.6 NNV 0.0 9 NSV 0.0 NI 1.6 0.4 SI 0.7 V 1.7 V 1.6 NI 0.5 NI 1.7 NI 0.5 ENI 0.7 V 0.2 V 0.2 V 0.2 V 0.2 V 0.3 V 0.2 V 0.3 V 0.3 V 0.4 V 0.5 SSV 0.9 V 0.	66 / (3	186   R   G   S   S   O   O   N   C   O   S   N   O   O   O   O   O   O   O   O   O	20t R G  S 1.4 N 1.7 SSW 0.8 NE 0.8 SSW 3.1 N 2.6 N 2.	R G G SSW 2.  SSW 2.  N 1.  WSW 1.  S 3.  N 2.  N 1.  N NO 2.  E 3.  E 4.  SSE 1.  ENE 2.  NWW 2.  NE 1.  NE 1.  NE 2.  SSE 2.  WNW 3.  ESE 1.  SSE 2.  SSW 11.  SSE 3.  ESE 2.  SSW 11.  SSE 3.  ESE 2.  SSW 11.  SSE 1.  SSW 12.  SSW 12.  SSW 13.  SSE 15.  SSW 15.  SSE 15.  SSW 15.  SSE 15.  SSW 15.  SSE 15.	6 SSW N N S S S S S S N N N N S S S S S N N N N S S S S S N N N N S S N N N N S S N N N N S S N N N N S S N	G 2.1 SS 1.9 NN 1.8 S 2.1 S 1.9 NN 1.8 S 2.1 S 1.6 NN 1.8 S 2.1 I.6 NN 1.8 S 2.1 I.6 NN 1.8 S 2.9 E 2.5 S 3.0 NN 1.8 S 2.9 E 3.0 NN 1.8 S 3.1 S 2.9 E 3.0 NN 1.8 S 3.1 S 2.9 E 2.5 S 3.0 NN 1.8 S 3.1 S 2.9 E 2.5 S 3.0 NN 1.8 S 3.1 S 2.9 E 2.5 S 3.0 NN 1.8 S 3.0 S 2.2 S 2.	R G  SW 2.2 WW 1.9 WW 1.4 SSE 2.1 WW 3.0 WW 2.6 SSE 3.4 E 3.4 SSE 3.4 E 3.4 SSE 3.4 E 3.4 SSE 3.4 E 3.4 SSE 3.	R G  NE 2.1 NNW 2.0 S 2.8 S 2.1 NNW 2.0 S 2.8 S 2.1 NNW 3.2 WNW 3.2 E 4.4 E 3.2 E 58 1.2 E 78 1.3	R G WNW 1. SSW 0. SE 1. 5 3.0 N 2.1 NW 2.1 NE 2.6 NW 2.1 E 5.2 E 4.1 E 5.2 E 4.2 E 8.2 E 8.2 NW 2.2 NW 2.1 NW	8 W 3.3 SEC. 10 SEC. 1	N I I I I I I I I I I I I I I I I I I I	mitter  G G G G  G G  G G  G G  G G  G G  G
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						kte Ables	ingen				
	Luftd	lruck as	af of redu	ziert in Mil	lim. ==	700*** +		Luf	ttemperate	ar nach Celsi	ius
Tag	194		2h	9a		Tagesmittel	19	ph	2 <sup>h</sup>	9h	Tagesmitte
			0.0	44.7		61		2.1		26.2	26,90
1 2	44.9	1	46.7	47.4		44-53		6.1	34.4	26.0	28,17
3	48.9		49.7	30.3	- 1	49.03		1.5	27.7	23.8	24-33
3	50.7		48.9	47.6	- 1			0.8	28.3	24.9	
5	45.4		42.7	42.8	- 1	49.07		1.5	30.7	21.3	24.50
		i			- 1						38
6	40.0		39.9	43.7	- 5	41.20		2.3	24.9	16.0	21.07
7 8	46.0		45.9	47-4	- 1	46.43		7.0	20.7	16.1	17.93
	48.8		45.4	45.3	- 1	48.50	- 1	5.3	21.7	20.6	19,20
9	48.9		45.0	47.0		47-97		7 - 1	26.5	22.9	22.17
10	46.8		46.h	46.3	- 1	461.57	1	8.8	22.5	20.5	20,60
11	46.9		45-4	45.5	- 1	45.93		0.0	25.4	21.3	22.23
12	45.9		46.0	40.4	- 8	46.10		8.6	22.6	20.0	20,80
13	45.6		44.5	44.4	- 1	44.83	21	0.0	22.5	15.8	20,43
14	46.5		47.1	47.4	- 1	47.00	15	5.1	19.7	10.1	16, 97
15	47 - 4		40.3	45.9		46.53	1.	1-7	23.4	19.5	19.30
16	45.5		43.9	42.3	8	43.90	12	8.6	27.5	24.3	23.47
17	41.8		44.6	45.8	il	44.07		2.3	21.7	19.0	20, 33
18	45.5	- 1	42.5	40.7	- 1	42,90		7.6	25.0	19.0	20.53
19	41.9		43.1	43.3		42.77		4.3	10.6	14.1	15,00
20	44.8		45.3	45.8		45.30		4.2	10,6	15.2	15.33
21	45.5	- 1	45-4	45.2		45-37		.8	21.2	17.1	17.76
22	45.2	1	45.0	44.3		44.53		7.4	23.5	19.2	20.01
23	43.3	1	41.2	39.0		41.47		7.7	25.1	20.2	21.00
24	39.0	1	35.7	40.0		39.23		0.2	22.7	19.5	29.47
25	42.9		43.8	45.9		44.20		7.8	19.4	17.0	18.0
26	1			46.8							1
	46.3	1	46.3		- 1	46.47		3.5	25.1	19.5	21.0
27	47-4	- 1	46.1	45.0		46.17		5.5		21.4	21.50
29	43.9	i	41.8	42.3		42.67	- 1	0.0	17.5	17.0	18.17
30	44.8	- 1	41.7	42.6					28.6	22.6	
31	46.3		40.2	46.1	- 9	45.03		5-3	24.4	20.2	22.17
-		- 1			-						1
Mittel	45.33		44.80	45.05		45.06	12	5.42	24.35	20.03	20.93
Tag	Dun	stdruck	in Millin	etern	R	elative Fe	chtig	keit		und Stärke [Skala: o — 1	
	196	2 <sup>h</sup>	Ò,	Tages- mittel	19h	2 <sup>h</sup>	94	Tages- mittel	19h	2 h	94
		**	100				-				
	14.1	14.9	18.5	15.8	72	4.1	73	62	0	NE 2	*** 1
2	16.6	12.9	15.9	16.1	7.5	3.2	70	61	0	ENE 2	(
3	16.0	16.7	13.1	15.3	84	61	60	68	WSW 1	NNW 1	100
4	12.6	10.6	13.4	12.2	69	38	58	55	MAM. 1	N I	E
5	14.5	14.3	15.8	14.9	70	44	84		SSW 1	NNE I	WSW

Tag	Dur	stdruck	in Millin	etern	Rel	ative F	euchtig	keit	Richtung und Stärke des Winde [Skala: o - 10]					
	19h	2 h	Qh.	Tages- mittel	19h	2 <sup>h</sup>	94	Tages- mittel	196		24		94	
	157	14.9		15.8	72			62		0	NE			
	16.6	14.9	18.5	16.1	75	41	73	61		0	ENE	2 2		ő
3	16.0	16.7	13.1		84	3.2 6.1	60	65	WSW	ï	NNW	1		
4	12.6	10.7		15.3	60	38	58		WAW		N	1	E	
			13.4	12.2	70		84	55	SSW	1	NNE	1	WSH	
5	14.5	14.3	15.8	14.9		44	54	0.5	-			,		
6	13.0	12.6	9.5	11.7	65	54	70	63	SW	2	WSW	3	NNW	- 1
7	10.5	0.2	8.1	9.3	7.3	41	59	61	WSW	2	711	3	***	
8	9.2	8.2	10.7	9.4	7.1	4.3	59	1,8	SSW	1	WSW	2	NNW	- 1
9	11.3	7.7	11.1	10.0	78	30	54	54		0	N	1	***	
10	10.5	13.1	12.7	12,1	65	65	71	67	8	1		1	w	
11	12.6	12.1	12.7	12.5	72	50	68	63	WAW	,	W	2	w	,
12	12.4	12.6	14.1	13.0	72	62	51	72	NAW		SW	1	S	
13	12.4	12.5	12.6	12.5	72	62	78	71	SSE	1	NNE	2	W	4
14	7-7	8.0	7.7	7.8	60	47	57	5.5	3335	3	NW	2	NW	- 1
15	9.2	6.6	11.2	9.0	74	31	65	57	***	0	WAW	1	***	
16	4 11.5	12.4	13.1	12.3	72	45	58	58	***	0	-11	0	***	
17	11.4	12.0	12.4	11.9	64	62	76	67	NW	1	NW	2	NW	-
18	12.1	12.3	14.1	12.8	81	5.3	57	74		0	4	2	SSW	- 1
19	9.7	8.2	10.0	9.3	81	58	84	74	7.8.	2	MAN	2	SW	3
20	8.1	8,1	8.5	8.2 1	67	57	66	63	W	4	W	4	SW	1
21	8.9	8.5	10.9	9.4	71	46	75	64	W	3	WNW		SW	
22	10.5	10.4	13.4	11.4	71	49	81	67	WSW	1	2M.	2	***	
23	12.2	12.3	12.2	12.2	Si	£2	69	67	5	í	WSW	i	SW	-
24	12.3	11.1	12.4	11.9	74	54	74	67	SW	2		i	NW	i
25	12.1	10.3	10.9	11.1	80	61	76	72	WAR	2	311	2	***	-
26	11.3	9.9	12.0	f na	71	42	71	61	11		N	3	111	
	10.8		13.1	11.4	77	42	60	62		1	NE	2	***	
27 28		10-3	13.1	13.1	75	47	66	63	SSW	: 1	NAW	2 2	N	-
	12.3	14.7	11.8	13.4			82	87	211		N	2	Ñ	2
29	13.9	14.5			79	99	60	61	***	0	W	2	N	1
30	12.0	9.0	12.1	11.0		31			***	0	X	;	NE	ı
31	9.1	8.9	10.1	9-4	54	39	57	50	***	0		'	A E	
Mittel	11,6	11-1	12.2	11.7	73	50	70	64		1.2		1.8		

Tag		Bewöl	kung [	Skala: o d Wolk	= heite	1, 10 ==	trûb]		Nieder- schlag in		E	eme	rkuni	z e n	
	19		2	ь		3,	Tages	mittel	Milli- metern	[					
3 4	FS HS	3 ··· 7 ··· 9 ··· 3 ···	FHS FHS FHS HS FS	7 W 7 W 5	FS FBS FS FS	3 ··· 3 ···	5 2	·7 ·3 ·7 ·3	8.3  1.1 4.3	Morger os S Abend	Tropfen. s dunsti	nacht	ounst.  Cu. On its gegen from achts @	rüh /⋜ u.	
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25 26 27 28 29	HS I	3 ···	FHS FHS	5 NW 3 9 W	FS FB FBS	3	3 4	.0	0.7	Abend Morge Morgs	ls dunsti ns=,.△ Dunst.:	g. ,abends ,bds.dur	Bunst. [3 istig,≤ i. N Ba, 1 [1-2	Bu, SE, 2	ts 🕲 u. 🖟
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Mittel		7.0		7.4		6.8			S. 61.1						
					- L	) Auto	graph	ische	Aufze	ichnur	ngen				
Tag	126	14k	164	184					Aufzert in Mill			" +	Tages-	Max.	Min.
Tag	12 <sup>b</sup> 44.0 45.3 47.7 50.7 47-3	14 <sup>k</sup> 43.9 45.8 47.9 50.7 47.0	16 <sup>1</sup> 44.2 40.2 47.0 50.4 4b.2	18 <sup>th</sup> 44.5 46.6 49.3 50.6 45.6	Luft	druck	auf o° r	eduzie	rt in Mill	imetern	= 700°		Tages- mittel 44.33 46.67 49.18 49.44 43.98	Max. 45-3 47-7 50.7 50.7 48.2	Min. 43.9 45.3 47.0 47.3 38.4
1 2 3 4 5 6 7 8	44.0 45.3 47.7 50.7 47-3 40.5 45.4 48.5	43.9 45.8 47.9 50.7 47.0 40.8 45.5 45.7	44.2 46.2 47.6 50.4 4b.2 40.3 45.5 48.8	44.5 46.6 49.3 50.6 45.6 39.9 45.9	Luft 20h 44.9 47.0 48.8 50.6 45.6 40.5 46.0 48.9	44-5 47-4 49-9 50-3 44-6 46-0 48-9	auf o° r ob 44.6 47.2 50.4 49.7 43.9 40.5 45.8 48.7	2h 4+.0 46.7 49.7 48.9 42.7 39.9 45.9 48.4	4 4 1 46.9 49.3 18.2 40.8 40.7 45.8	43.9 46.8 49.3 47.7 39.8 41.9 46.2 47.8	8 <sup>4</sup> 44.1 46.6 49.7 47.6 40.2 43.3 46.9 47.8	10 <sup>4</sup> 45.2 47.7 50.6 47.9 42.0 44.2 48.0 48.4	mittel  44.33 46.67 49.18 49.44 43.98 41.09 46.08 48.50	45-3 47-7 50.7 50.7 48.2 45.4 48.5 49.0	43.9 45.3 47.0 47.3 38.4 39.9 45.4 47.8
1 2 3 4 5 6 7 8 9	44.0 45.3 47.7 50.7 47.3 40.5 45.4 48.5 48.7 47.1	43.9 45.8 47.9 50.7 47.0 40.8 45.5 45.7 45.7	44.2 40.2 47.6 50.4 4b.2 40.3 45.5 48.8 46.9	44.5 46.6 49.3 50.6 45.6 39.9 45.9 49.0 48.8 46.8	Luft  20h  44-9 47-0 48-8 50-6 45-6 40-5 46-0 48-9 48-9 48-9 46-8	22h 44-5 47-4 49-9 50-3 44-6 40-6 46-0 48-9 49-0 45-9	auf o* r ob 44.6 47.2 50.4 49.7 43.9 40.5 45.8 48.7 48.5 46.1	24 4+.0 46.7 49.7 48.9 42.7 39.9 45.9 48.4 48.0 46.6	44 · 1 44 · 1 46 · 9 49 · 3 48 · 2 40 · 8 40 · 7 45 · 8 48 · 5 45 · 9	43.9 46.8 49.3 47.7 39.8 41.9 46.2 47.8 47.9 46.0	8 <sup>6</sup> 44.1 46.6 49.7 47.6 40.2 43.3 46.9 47.8 47.8 46.0	10 <sup>4</sup> 45.2 47.7 50.6 47.9 42.0 44.2 48.0 48.4 47.2 46.4	mittel  44.33 46.67 49.18 49.44 43.98 41.09 46.68 48.50 48.40 46.45	45-3 47-7 50.7 50.7 50.7 48.2 45.4 48.5 49.0 49.0 47.1	43.9 45.3 47.0 47.3 38.4 39.9 45.4 47.8 47.8 47.0
1 2 3 4 5 6 7 8 9 10 ET 1 12 2	44.0 45.3 47.7 50.7 47.3 40.5 45.4 48.5 48.7 47.1	43.9 45.8 47.9 50.7 47.0 40.8 45.5 48.7 46.9 46.4 43.4	44.2 40.2 47.0 50.4 48.2 40.3 45.5 48.8 46.9 46.4 45.3	44.5 46.6 49.3 50.6 45.6 39.9 45.9 45.9 48.8 46.8 46.8	Luft zoh 44-9 47-0 48-8 50-6 45-6 40-5 46-0 48-9 48-9 46-8 47-2 46-3	22h 44-5 47-4 49-9 50-3 44.6 46.0 48-9 49-9 49-9 49-9 49-3 46-3	auf o* r ob 44.6 47.2 50.4 49.7 43.9 40.5 48.7 48.8 48.7 48.5 46.1	24 44.0 46.7 49.7 48.9 42.7 39.9 45.9 48.4 48.0 46.6 45.4	rt in Mill 4* 44. t 46.9 49.3 48.2 40.8 40.8 40.8 40.8 40.8 40.8 40.8 40.8 40.8 40.9 40.8 40.9 4	ma 43.9 46.8 49.3 47.7 39.8 41.9 46.2 47.8 47.8 47.9 46.2	85 44.1 46.6 49.7 47.6 40.2 43.3 46.9 47.8 46.9 47.8 46.0 45.3 46.1	10° 45.2 47.7 50.6 47.9 42.0 48.0 48.4 47.2 46.4 45.5	mittel  44.33 46.67 49.18 49.44 43.98 41.09 46.68 48.50 48.40 46.45 46.09	45-3 47-7 50.7 50.7 48.2 45.4 48.5 49.0 49.0 47.1 47.3 46.8	43.9 45.3 47.0 47.3 38.4 39.9 45.4 47.8 47.0 45.9 44.6
1 2 3 4 5 6 7 8 9 10 ET E2 13 14	44.0 45.3 47.7 50.7 47-3 40.5 45.4 48.5 48.7 47.1 46.5 45.8 45.8	43.9 45.8 47.9 50.7 47.0 40.8 45.5 45.7 46.9 46.4 45.4 46.1	44.2 40.2 47.0 50.4 48.2 40.3 45.5 48.8 46.9 46.4 45.3 45.3 45.3	44-5 46-6 49-3 50-6 45-6 39-9 45-9 48-8 46-8 46-7 45-8 45-5 45-9	Luft 20h 44-9 47-0 48-8 50-6 45-6 40-5 46-0 48-9 46-8 47-2 46-3 45-6 47-0	22 <sup>h</sup> 44-5 47-4 49-9 50-3 44-6 40-6 46-0 48-9 47-3 46-3 45-9 47-2	auf o* r ob 44.6 47.2 50.4 49.7 43.9 40.5 45.8 48.5 46.1 46.5 46.1 45.2 47.1	2h 4+0-0 46-7 48-9 42-7 39-9 45-4 48-0 46-6 45-4 46-0 44-7	rt in Mill 4* 44. t 46.9 49.3 48.2 40.8 40.7 45.8 48.1 48.5 45.9 44.8 45.8 44.9 45.8 45.9	43.9 46.8 49.3 47.7 39.8 41.9 46.2 47.9 46.0 45.1 45.9 44.2 46.8	86 44.1 46.6 49.7 47.6 40.2 43.3 46.9 47.8 47.8 46.0 45.3 46.1 44.2	45.2 47.7 50.6 47.9 42.0 44.2 48.0 48.4 47.2 46.4 45.5 46.5 44.4	mittel  44,33 46,67 49,18 49,44 43,98 41,09 46,68 48,50 48,40 46,45 46,09 45,92 45,17 46,49	45-3 47-7 59.7 59.7 48.2 45.4 48.5 49.0 49.0 47.1 47.3 46.8 46.8	43.9 45.3 47.0 47.3 38.4 39.9 45.4 47.8 47.0 45.9 44.8 45.3 44.0
1 2 3 4 5 6 7 8 9 10 t1	44.0 45.3 47.7 50.7 47.3 40.5 45.4 48.5 48.7 47.1 46.5 46.5 46.5 45.0 47.7	43.9 45.8 47.9 50.7 47.0 40.8 45.5 45.7 46.9 46.4 45.4 46.1 45.2 47.4	44.2 47.6 50.4 48.2 40.3 45.5 48.8 46.9 46.4 45.3 45.3 47.4	44-5 46-6 49-3 50-6 45-6 39-9 45-9 48-8 46-8 46-7 45-8 45-9 47-4	Luft  20h  44-9  47-0  48-8  50-6  45-6  40-5  46-0  48-9  48-9  46-3  47-2  46-3  47-0  47-3	22h 44-5 47-4 49-9 50-3 44-6 40-0 48-9 49-0 45-9 49-0 45-7 47-3 46-3 45-7 47-2 47-3	auf o <sup>b</sup> r  ob  44.6 47.2 50.4 49.7 43.9 40.5 48.7 48.5 46.1 46.5 46.1 47.1	44.0 46.7 49.7 49.7 48.9 45.9 45.9 48.4 48.6 46.6 45.4 46.0 44.5 46.3	rt in Mill  4*  44.1  46.9  49.3  48.2  40.7  45.8  48.5  45.8  45.8  44.0  46.0	66 43.9 46.8 49.3 47.7 39.8 41.9 46.2 47.8 47.9 46.9 46.9 46.9 46.8 45.8	86 44.1 46.6 49.7 47.6 40.2 43.3 46.9 47.8 46.9 47.8 46.0 45.3 46.1 44.2 45.7	10 <sup>6</sup> 45.2 47.7 50.6 47.9 42.0 44.2 48.0 48.4 47.2 46.4 45.5 46.5 44.4 47.4 46.1	mittel 44.37 46.67 49.18 49.44 43.98 41.09 46.68 48.50 48.40 46.45 46.09 45.92 46.19 46.79	45-3 47-7 50.7 50.7 48.2 45.4 48.5 49.0 49.0 47.1 47.3 46.8 46.8 47.7 47-7	43.9 45.3 47.0 47.3 38.4 39.9 45.4 47.8 47.0 45.9 44.8 45.3 44.0 45.3
1 2 3 4 5 6 7 8 9 10 t1 t2 13 14 15	44.0 45.3 47.7 50.7 47-3 40.5 45.4 48.5 48.7 47.1 46.5 45.8 45.8	43.9 45.8 47.9 50.7 47.0 40.8 45.5 45.7 48.7 46.0 46.4 45.4 40.1 45.2 47.4 45.6	44.2 40.2 47.6 50.4 48.5 49.5 48.8 46.9 46.4 45.3 45.8 45.3 45.3 47.4 45.5	44-5 46-6 49-3 50-6 45-6 45-6 45-9 49-0 48-8 46-7 45-8 45-5 45-9 47-4 45-5 45-5 45-9	Luft 20h 44.9 47.0 48.8 50.6 45.6 45.6 46.0 48.9 46.8 47.2 46.3 47.0 47.3 45.6 47.0	44-5 47-4 49-9 50-3 44-6 46-0 48-9 49-9 47-3 46-3 45-9 47-3 45-7 47-2 47-3 45-3 45-3 45-3 45-3 45-3 45-3 45-3 45	auf o* r ob 44.6 47.2 50.4 49.7 43.8 48.5 48.7 48.5 46.1 46.5 46.1 47.1 47.1	24 4+.0 46.7 48.9 42.7 39.9 45.9 48.0 46.6 45.4 46.0 41.5 47.1 46.3 43.9 44.6	rt in Mill  4*  44.1  46.9  49.3  40.8  40.7  45.8  48.1  48.5  45.0  46.0  46.0  42.0  45.2	metern  43.9  46.8  47.7  39.8  47.8  47.9  46.0  45.1  45.9  46.8  45.8  42.4  45.3	86 44.1 46.6 49.7 47.6 40.9 47.8 47.8 47.8 47.8 46.0 45.3 46.0 45.3 46.1 47.2 45.7 45.7	10 <sup>6</sup> 45.2 47.7 50.6 47.9 42.0 48.0 48.4 47.2 46.4 47.4 46.1	mittel 44.33 46.67 49.18 49.44 43.98 41.09 46.08 48.50 48.40 46.45 46.09 45.92 45.17 46.79 44.30	45-3 47-7 50.7 48.2 45.4 48.5 49.0 49.0 49.0 49.1 47.3 46.8 46.8 47.7 47.7 46.1	43.9 45.3 47.0 47.3 38.4 39.9 47.8 47.0 45.9 44.8 45.0 45.7 42.0
1 2 3 4 5 6 6 7 8 9 10 ET E2 13 14 15 16 17	44.0 45.3 47.7 50.7 47-3 40.5 45.4 48.5 48.7 47-1 46.5 45.8 45.0 47.7 46.8	43-9 45-8 47-9 50-7 47-0 40-8 45-5 48-7 48-7 46-9 46-4 45-4 46-1 45-2 47-4	44.2 40.2 47.6 50.4 48.2 40.3 45.5 48.8 48.8 46.9 46.4 45.3 45.3 45.8 45.8 45.8 45.8	44-5 46:6 49:3 50:6 45:6 45:9 49:0 48:8 46:8 46:7 45:8 45:5 47:4 45:5	Luft  20h  44-9 47-0 48-8 50-6 45-6 40-5 46-0 48-9 46-9 46-3 46-3 47-2 46-3 47-3 45-4	22h  44-5 47-4 49-9 50-3 44-0 40-6 46-0 48-9 49-0 45-9 47-3 46-3 45-7 47-2 47-3 45-3 45-3 45-3 45-3 45-3 45-3 45-3 45	auf o <sup>b</sup> r  o <sup>b</sup> 47.2 50.4 49.7 43.9 40.5 45.5 46.1 46.5 46.1 47.1 47.1 47.1 44.8 44.1 44.3	44.0 46.7 49.7 49.7 48.9 42.7 39.9 48.4 48.0 46.6 45.4 46.0 41.5 47.1 46.3 43.9 44.6 42.5 43.1	rt in Mill 4*  44-1 46-9 49-3 48-2 40-8 40-7 45-8 48-5 45-9 44-8 45-8 45-9 44-9 45-9 44-9 45-9 44-9 45-9 44-9 45-9 44-9 45-9 44-9 45-9 44-9 45-9 44-9 45-9 44-9 45-9 45	metern  43.9 46.8 49.3 47.7 39.8 41.9 46.2 46.0 45.1 45.9 46.8 45.8 47.9 45.1 45.9 46.8 45.3 41.5 43.2	85 44.1 46.6 49.7 47.6 40.2 43.3 46.9 47.8 47.8 46.0 45.3 46.1 44.2 47.2 45.3 49.3 49.4 49.4 49.4 49.4 49.4 49.4 49	10 <sup>6</sup> 45.2 47.7 50.6 47.9 48.0 44.2 48.0 48.4 47.4 46.4 47.4 46.1 42.2 46.1 47.2 47.4	mittel  44.33 46.67 49.18 49.44 43.98 41.09 46.68 48.50 48.40 46.49 46.49 46.49 46.49 46.30 43.52 43.82 42.61	45-3 47-7 50.7 48.2 45.4 48.5 49.0 49.0 49.0 49.1 47.3 46.8 46.8 47.7 47.7 46.1 46.1 46.1	43.9 45.3 47.0 47.3 38.4 47.8 47.8 47.8 47.8 45.9 45.9 45.9 45.3 44.0 45.7 42.0 40.5
1 2 3 3 4 5 5 6 6 7 8 9 10 til 12 13 14 15 16 17 18 19 20 21 22 3 3	44.0 45.3 47.7 50.7 47.3 40.5 45.4 48.7 47.1 46.5 46.8 45.5 46.8 47.7 46.1 40.0 42.2 43.2 45.7 45.5 44.8	43.9 45.8 47.9 45.8 47.9 47.0 40.5 45.5 45.7 45.7 46.4 45.4 46.1 45.2 47.4 45.8 42.2 47.4 45.8 43.3 45.8	44.2 40.2 47.0 50.4 48.2 40.3 45.5 48.8 48.8 46.9 46.4 45.3 47.4 45.3 47.4 45.5 43.4 44.0 45.3	44-5 46-6 49-3 50-6 45-6 39-9 49-0 48-8 46-7 45-8 46-7 45-8 45-9 47-4 45-5 41-2 45-5 44-4 45-5 44-4	Luft 20h 44.9 47.0 48.8 50.6 45.6 45.6 46.0 48.9 46.8 47.2 46.3 45.6 47.3 45.4 42.2 44.9 45.6 45.6 47.3	### druck ### 44-5 ### 44-5 ### 49-9 ### 40-0 ##	auf o <sup>b</sup> r  ob  44.6 47.2 50.4 49.7 43.9 40.5 48.7 48.7 48.7 46.1 46.1 45.2 47.1 44.8 44.1 44.3 43.5 45.4 45.6 45.4 45.6	24 49.00 40.77 40.77 42.77 39.99 45.99 45.94 46.0 41.53 43.44 45.00 42.5 43.43 43.44 45.00 44.55 43.43 45.44 45.00	4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	## ## ## ## ## ## ## ## ## ## ## ## ##	8b 44-1 46-6 47-7 47-8 46-9 47-8 46-9 47-8 46-9 47-8 46-9 47-8 46-9 47-8 46-9 47-8 46-9 47-8 46-9 47-8 46-9 47-8 46-9 46-9 47-8 46-9 46	10 <sup>h</sup> 45.2 47.7 50.6 47.9 47.0 48.0 48.4 47.4 46.4 45.5 46.5 44.4 47.1 42.2 46.1 43.2 45.1 43.2 45.2 45.3	mittet  44.33 46.67 49.18 49.18 49.44 43.98 41.09 46.06 48.50 48.40 46.45 46.49 45.17 46.49 44.30 43.52 42.61 44.38 44.88 44.88	45-3 47-7 50.7 50.7 50.7 45.4 48.5 49.0 49.0 49.0 49.1 47.3 46.8 47.7 46.1 46.0 43-5 45.9 45.9 45.9	43.9 45.3 47.0 47.3 38.4 39.9 47.8 47.8 47.0 45.3 44.0 45.7 42.0 40.5 40.9 43.8 30.6
1 2 3 4 5 6 7 7 8 9 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 23 24 25	44.0 45.3 47.7 50.7 40.5 45.4 48.5 48.5 47.7 46.5 45.8 45.7 46.1 42.1 40.0 42.2 43.2 45.7 44.2 45.7 45.2 39.7	43-9 45-8 47-9 50-7 47-0 40-8 45-5 48-7 46-4 45-4 40-1 45-2 47-4 45-8 41-5 41-5 43-3 45-2 43-3 45-2 43-3 45-2 43-8 39-3 41-2	44.2 40.2 47.0 50.4 46.2 40.3 45.5 48.8 45.8 45.8 45.3 45.3 47.4 45.3 47.4 45.3 47.4 41.0 44.0	44-5 46-6 49-3 50-6 45-6 39-9 49-8 48-8 46-8 46-7 45-8 45-9 47-4 45-5 41-2 44-4 45-5 45-5 45-5	Luft 20h 47.0 47.0 48.8 50.6 45.0 45.0 48.9 46.8 45.6 45.0 47.0 47.3 45.4 45.4 45.4 45.6 45.6 45.6 45.6 45.6	## 226 #4-5 #7-4 #9-9 \$0-3 #4-6 #0-6 #0-6 #0-6 #0-6 #0-9 #0-9 #0-3 #0-3 #0-3 #0-3 #0-3 #0-3 #0-3 #0-3	auf o° r ob 44.6 47.2 50.4 49.7 43.9 40.5 45.8 46.5 46.1 46.5 46.1 47.1 47.1 44.8 44.3 43.5 45.4 44.3 43.5 45.4 45.4 45.6 45.4 45.6	24 44.0 44.0 44.0 49.0 42.7 39.9 42.7 39.9 48.4 48.0 45.4 40.6 45.4 41.6 43.4 45.3 41.6 45.3 41.6 45.3 41.6 45.3 41.6 45.3 41.6 45.3 41.6 45.3 41.6 45.3 41.6 41.6 41.6 41.6 41.6 41.6 41.6 41.6	rt in Mill 4* 44.1 45.9 40.3 45.2 40.7 45.8 45.9 44.8 45.9 44.8 45.9 44.8 45.9 44.8 45.9 44.8 45.9 44.8 45.9 44.8 45.9 44.8	## 1.5 ##	8b 44.1 46.6 47.6 40.7 47.6 40.9 47.8 46.9 47.8 46.0 45.1 44.2 45.7 45.7 42.3 45.7 45.7 45.7 45.7 45.7 47.6	10 <sup>6</sup> 45.2 47.7 50.6 47.9 42.0 48.4 47.2 48.6 46.5 44.4 47.4 46.1 42.2 45.8 45.8 45.8	mittet  44.33 46.67 49.18 49.44 43.98 41.09 46.08 48.50 48.40 46.45 46.09 45.92 46.79 44.30 43.52 42.61 44.76 45.38 44.88 42.03 39.14	45-3 47-7 50.7 50.7 50.7 48.5 49.0 47-1 47-3 46.8 46.8 46.8 47-7 47-7 46.1 46.0 47-7 46.1 46.0 47-8 46.1 46.0 47-7 47-7 46.1 46.0 47-8 47-8 47-8 47-8 47-8 47-8 47-8 47-8	43.9 45.3 47.0 47.3 38.4 39.9 45.4 47.8 47.0 45.9 44.0 45.7 42.0 40.9 43.2 45.0
1 2 3 4 5 6 7 8 9 10 11 14 15 16 17 19 20 21 22 23 24	44.0 45.0 45.7 47.7 47.3 40.5 45.4 48.5 48.7 47.1 46.5 45.6 45.6 45.6 45.6 45.7 47.1 40.2 43.2 43.2 43.2 43.2 43.2	43.9 45.8 47.9 50.7 47.0 40.8 45.5 48.7 46.0 46.4 45.4 45.2 47.4 45.6 41.5 42.2 43.8 45.4 45.2 43.8	44.2 46.2 47.0 50.4 48.2 40.3 45.5 48.8 46.9 46.4 45.3 45.3 47.4 45.5 41.0 44.0 45.3 47.4 41.0 44.0	44-5 46-6 49-3 50-6 45-6 39-9 49-8 46-8 46-8 46-7 45-5 45-5 45-5 45-5 41-2 44-4 45-5 41-2 44-4 45-5 45-1 43-1 38-8	Luft 20h 44-9 47-0 48-8 50-6 45-6 45-6 46-0 48-9 46-3 45-6 47-0 47-3 45-4 42-5 44-9 45-2 44-9 45-2 43-1 39-0	### druck #### 44-5 #### 44-5 ###################################	auf o* r oh 44.6 47.2 50.4 49.7 43.5 45.5 46.1 45.5 46.1 47.1 47.1 47.1 44.1 44.1 44.1 44.1 44	24 44.0 46.7 49.7 49.7 49.7 49.7 45.9 45.4 46.6 45.4 46.8 47.1 46.3 45.3 45.4 45.6 45.4 45.2 45.3 45.4 45.2 45.3 45.4 45.2 45.2 45.2 45.2 45.2 45.2 45.2	rt in Mill  4*  44. 1  46.9  49.9  40.8  40.7  45.8  46.1  48.9  44.8  45.9  44.8  45.9  44.8  45.9  44.8  45.9  44.8  45.9  46.0  42.9  45.2  45.8  45.9	metern  43.9 46.8 49.3 47.7 39.8 41.9 46.2 47.9 46.1 45.9 46.8 45.8 45.8 45.3 41.5 45.3 41.5 45.3 45.3 45.3 45.3 45.3	8b 44.1 46.6 49.7 47.6 40.9 47.8 46.9 47.8 46.1 44.2 45.3 46.1 44.2 45.3 46.1 44.2 45.7 45.3 40.1 40	10 <sup>5</sup> 45.2 47.7 50.6 47.9 42.0 48.4 47.2 46.4 45.5 44.4 46.1 42.2 45.8 45.8 45.8 45.8	mittet  44.33 46.67 49.18 49.44 43.98 41.09 46.08 48.50 48.40 46.45 46.09 45.92 43.82 43.82 44.76 45.38 42.61 45.88 42.03	45.3 47.7 50.7 50.7 48.2 45.4 48.5 49.0 47.1 46.8 46.8 46.8 47.7 47.7 46.1 46.1 46.1 46.1 46.5 45.8 45.8	43.9 45.3 47.0 47.3 38.4 39.9 45.4 47.8 47.8 47.8 45.9 44.8 45.0 45.0 41.0 40.9 43.2 45.3 83.6 38.6

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T.,,						L	ufttem	peratu	r nach	Celsius					
Tag	12 <sup>h</sup>	14 <sup>h</sup>	16h	18h	301	32 <sup>6</sup>	0%	2 <sup>h</sup>	40.	65	80	10 <sup>b</sup>	Tages- mittel	Max.	Min.
1	22.7	31.6	20.1	20.5	a5.2	29.0	30.9	32.4	34.4	33.		26,1	27.09	34.1	20,1
3	24.5	22.9	21.8	22.5	26.2	29.9	32.0	34.4	32.6	26.		25.2	27.19	34.7	21.0
4	21.3	20.5	19.4	19.4	23.2	26.0	37.1	28.3	29.5	28.		24.2	24.51	30.2	18.8
5	22.5	21.3	21.1	20.1	23.3	26.1	28.9	30.7	31.1	28.		21.0	25.07	31.3	19.9
7	15.5	15.5	20.8	21.6	18.8	19.6	23.3	24.9	20.7	18,		15.6	20.78	25.0	15.4
8	14.5	14.6	14.2	14.4	17.3	20.1	21.5	21.7	22.9	24.	4 22.0	19.9	18.46	24.4	14.0
10	18.2	16.8	15.7	15.8	20.2	23.0	25.4	36.5	27.2	28.	25.0	21.5	21.98	28.5	15.3
11	20.0	19.7	19.2	17-3	20.6	27.1	27.5	22.5	24.5			20.4	21.58	26.9	17.1
12	19.4	19.2	10.0	19.7	20.8	22.9	22.4	25.4	23.3	24.	5 21.1	19.5	21.10	24.2	18.7
13	18.7	18.7	18.7	18.9	20.7	21.8	22.2	22.5	24.6	19.	6 19.7	18.4	20.37	25.3	18.2
14	18.2	17.1	16.5	14.8	15.3	17.3	18.2	19.7	20.0	23.		15.1	17.38	20.3	14.5
16	18.3	17.4	16.4	17.2	20.8	24.8	26.7	27.5	25.0	27.		23.4	22,82	28.8	16.4
17	21.8	20.3	18.9	19.8	23.1	23.0	22.4	21.7	20.9	21.	9 25.4 19.8	18.6	20.90	23.8	17.6
18	17.6	16.7	16.2	16.6	18.9	21.6	23.6	25.0	19.6	20.	19.5	14.8	19.18	25.0	14.8
19	15.6	15.4	14.9	14.4	14.7	16.8	15.6	16.6	17.4	14.		14.7	15.32	17.9	13.2
21	13.6	12.4	12.1	13.1	17.3	18.8	18.8	21.2	21.1	19.		17.1	16.87	21.4	12.1
22	16.1	16.0	15.3	16.3	19.8	21.3	22.5	23.5	23.8	21.	20.6	18.7	19.61	24.3	15.1
23	18.0	17.3	16.6	16.7	18.7	18.8	24.7	25.1	25.6	20.		19.8	20.38	26.0	16.4
25	18.1	17.4	17.1	19.1	17.2	17.7	18.4	19.4	19.9	19.4		16.5	18.07	20.4	16.2
26	16.2	16.9	16.8	17.0	19.6	32.5	23.6	25.1	25.4	24.		18.6	20.66	25.4	16.2
27	17.0	15.8	15.0	15.2	19.2	23.5	25.6	26.6	26.8	26	23.2	20.6	21.24	27.0	14.7
28	19.1	18.4	17.6	17.7	20.8	25.2	25.7	30.1	19.9	19.	23.9	20.9	23.11 19.39	30.3	16.1
30	16.1	15.3	14.3	14.9	16.6	20.7	25.0	28.6	28.2	26.		21.1	21.00	28.6	14.3
31	20.7	20.3	19.0	18.4	20.4	23.1	23.3	24.4	25.2	24.6	5 21.8	19.1	21.61	25.4	17.5
M.M.	18.58	17.95	17-32	17.53	19.57	23.23	23.55	24.35	24.53	23.	8 21.25	19.26	20.82	25.66	16.40
-	-									_	-	-	_		-
Tag			Rich	tung		schwind	ligkeit	(G) des	Wind	es in	Sekunde	in Meter	rn,		Tages
	12 <sup>h</sup> R G	R 14 <sup>h</sup>	g   R	g	181 R G	20 <sup>1</sup> R G	22h R	$G = R^{0^k}$		2h R G	R G	8 a	8"     R   G	10 <sup>h</sup>	G G
1	0.	S	0.7		NE 0.5	ESE a.8	SE 1	.4 SE	2.2 5	SE 1.5	E 3.0	ESE 4.4	ESE O.		.2 1.2
3	S 1.	SSW	0.4 WSW		VXW 2 1	NAW O.S	ENE :	.o NNE	2.7 2.2 X	NE 2.3	NNE 2 6	NAW O.	9 NNW 1.	I NNW	.4 1.1
4	NNW 1.	W.K.C	0.2 1151	1.0	SSW 0.2	NW O. S	ENE 1	1.6 NE	1.9 N	NE 2.0	NNE 1.5	ESE 1.5	o ESE 1.	\$ 6	1.1 10.0
5	E 0.			4.9	W 3.5	SW 2,2		1.1 WAW	1.2 3	NE 2.0	E 3.2		9 WNW 3.		.8 2.1
6	NNW 2.	SW	1.3 WSW	1.4	SW 2.1 SW 1.3	WSW 3.8	WAW 4	.o WSW	3.5 11	SW 5.0	AW 4.5	N 3.	NNE 4.	9 N 1	.2 3.2
7 8	N 1.	WNW	0.4 SSW	0.6	SSW 0.4	W 2.1	NNE 1	.s NXW	1 0 3	XE 3.0	3 1.4	NNE 3.	AW O.	61 0	.4 2.2
9	WSW 0.	WSW	0.0 551	0.8	5 0.6	SE 0.7	WAM C	1.4 NW	1.8	NE 1.4	NNE 1.8	N 1.3	2 ESE 1.	1 0	.0 0.9
10		SSW			S 0.7	SSE 1.2				W 2.6			4 W.Y.W. 2.		.7. 2.0
11	WYW O.	WAW	3.9 WNW	2.5 4	NW 3.4	NW 2.4	W 2	. O W	2.0	W 2.6	NW 3.3	NW o.	WYW 3.	WNW I	.9 2.7
12	S 1.	1 8	1. tl SSE	0.7	S 1.2	WNW 1.8	WNW I	OWNW	2.7 WD	W 3.7	WAI 4.8	NW 2.1	W. N.W. 2.	S WNW 4	.3 2.5
14	WNW 2.3	2 3	1.6	1.5 N	NW 4.8	NAW 4.6	NNW 3	.7 N	2.1 5	NE 2.6	3 3.6	3 4.0	TAW 1.	S WSW o	.0 3.9
15	N 0.4		1 .		SSW 0.8	N 1.9		o NW		W 3.0					
16	SW 1.0		0.7	0.2	5 1.0	WNW 2.3	NE o	7 NNW	3.2 N	NE 0.5	SSW 1.0	ENE 2.4	SE o.	SSW 1	.5 0.8
18	SSW o.	884	1.8 8	0.4 5	0.0 466	5 0.2			1 6 8	8 . 116	88E 1 0	SSW T	45.15	WYM 3	S 1.1
	WSW 1.6	11.	3.0 W	2.6	NW 3.2	NW 4.2	WYW &	HAH AL	4.6 W	W 6,0	WNW 7.5 WNW 5.7	WAW 4.3	WAN 3.0		.1 4.1
**			S.O.WXW												-5 5.1
21	W 1.8	WAW	2.2 SSW 1.5 WSW	2.2 1	SW 2.7	W 2 2	14 1	.6 WNW	3.5 NA	W 2.6	WAW 2.0	WYW L.I	15 NW 1.	NW o	.0 2.3
23	SSE 1.1	S	1.5 SSW	2.2	\$ 1.4	5 2.t	WSW 2	.2 W	3-7	W 1.6	*) 1 2	4) 1.5	WSW 2 4	11 SW 3	.2 2.3
24	W NW 2.4	HSH	2. 8 W NW	3.0 1	SW 3.5	NW 4.1	11 11 11 5	.0 NW	3.4	N 2.6	NYW 4.1	WNW 1.4	1 0.1	S OW 1	0 2.8
25		WSW							-	- 1	N 4.0	Y 2.6			.2 2.3
20	SSW O.S	SSW	0.6 5	0.5	5 0.5	5 0.9	SSW 1	Wall D.	3.1	E 2.4	ESE 1.0	NNE o. 6	ENE o.	Eo	.2 0.9
28	0.0	***	0.0 E	0.2	E 0.4	SSW 1.0	5 0	.2 5	2 1 53	11 0. 2	SE 0.9	SSW 1.2	N 3.1	E o	.9 1.1
30	WNW 3.1	SW	0.6 ANW	0.8	S 0.6	SSW 2,0	WYW 1 SSW 2	.9 W	2.7 AN	W 3.5	NNE 3.0	NNE 2.6 WNW 3.6	W X W 2.		3 3.2
31	WNW o.5	WAR	1.9 338	1.0	N 0.8	N 1.0	N I	.4 N	1.5	S 1.7	£ 2.8	NE 2.2	ENE 2.	N I	4 1.0
LM.	1.38		.40	1.52	1.63	2.09			2.71	2.85	2.89	2.35	1.65		36 2.04
							2.								

## August

1905

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Tag	196		21:	94		[agesmittel	19		27	94	Tagesmitte
,				41.8	-	t.m.	16		25.2	21.4	21,07
2	45.5	- 7	43.6	44.9		43.63	19.	6	23.9	17.7	20.47
3	44.1		42.2	41.5	1	42.70	15		25.7	21.6	21.07
4	42.6		41.8	40.1		41.50	19	- 4	32.0	25.1	24.97
5	40.4	1	39.5	39.8		40.00	21.	4	32.0	20.6	24.67
6	42.1		43.4	42.9	- 1	42.80	19.	.0	18.6	14.6	17.40
3	43.5		46.1	48.0		45.87	15.	. 0	13.8	13.2	14.03
	48.7		48.6	48.6	- 1	48.63	13.		21.2	17.4	17.47
9	49.8		45.4	47.8	- 1	48.67	16.		25.8	20.3	20.73
10	47.2		44.5	43.8		45-17	19		29.6	19.3	22.63
11	43.5		45.2	44.4		44-37	18.		18.4	19.0	18.53
12	47 - 3 52 - 7		49.4 52.1	52.5		49.17 52.43	15.		20.3	15.8	16.57
14	52.5	4	31.4	50.5		51.47	15.		20,2	17.0	17.40
15	50.2	1	48.6	47.6	- 1	48.50	14	2	22.6	17.9	18.23
16	46.3		44.0	44.2	- 10	45-13			25.1	19.8	-
17	44.7		40.0	40.9		45.87	17.	.0	19.8	16,6	17.80
18	47.0		47.6	47.1	- 1	47-53	15.	.6	21.7	18.4	18.57
19	46.0		43.5	45.8	1.6	45.10	17.	2	26.2	17.4	20.27
20	48.3		45-5	44.2	- 1	46.00	14-		22.8	17.8	18.27
21	47 6		48.7	45.2		45.07	17.	2	20.6	16.9	18.23
22	47-9	- 1	46.1	45.0		46.33	14.	8	24.3	19.6	19.57
23	43-7	- 1	43.1	44-4		43.73	17.	3	26.6	20.6	21.50
24 25	46.1		44.7	44.6		45.13	16,		22.5	17.7	18.27
26	41.6		43.3		- 1	43.53	16.		24.8	19.0	
26	41.6		40.8	39.5		43.03	16.		21.5	17.4	19.97
28	43.4	- 1	39.6	34.4		39.13	14.		21.9	17.3	17.97
29	32.8		31.4	30.6	- 1	31.60			17.2	13.4	14.53
30	30.5		33.4	35.2	- 5	33.03	12		16,8	15.2	14.93
31	39-7		44.8	46.7		13-73	14.	2	15.6	14.6	14.80
Mittel	44.64		44.26	44.15	- 5						. 0 0)
			44.20	111.13		44.35	10,	19*)	22.42	17.92	18.79°)
			in Millin			lative Fe			1	u. Stärke ([Skala: 0 — 1	tes Winder
Tag			-			-			1	u. Stärke	tes Winder
Tag	Dun 19 <sup>h</sup>	stdruck 2h	in Millin	Tages- mittel	R e	elative Fe	uchtigi 9h	Tages- mittel	Richtung	u. Stärke ( [Skala: o — i	des Winder
Tag	Dun 19 <sup>h</sup>	2h	in Millin	Tages- mittel	R e	ab SS	9h	Tages- mittel	Richtung	u. Stärke e [Skala: o — i	tes Winde
Tag	Dun 19 <sup>h</sup>	2h 12.9 13.5	in Millin	Tages- mittel	R e	elative Fe	uchtigi 9h	Tages- mittel	Richtung	u. Stärke e [Skala: 0 — 1 2h SE 2 0 ESE 2	des Winde
Tag	19 <sup>h</sup>	2h 12.9 13.5 14.2 16.7	9 <sup>t</sup> 14.2 12.9 16.1 14.1	Tages- mittel	72 90 86 87	2b   35   61   59   52	9h 75 86 84 60	Tages- mittel	Richtung	SE 2 SE 2 NE 1	es Winde
Tag	Dun 19 <sup>h</sup>	2h 12.9 13.5	9 <sup>6</sup>	Tages-mittel	72 90 86	2b   35   61   59	9h 75 86 84	Tages- mittel	Richtung	u. Stärke e [Skala: 0 — 1 2h SE 2 0 ESE 2	ene NNW I
Tag	19 <sup>h</sup>	2h 12.9 13.5 14.2 16.7 13.1	9 <sup>t</sup> 14.2 12.9 16.1 14.1	Tages- mittel 14.0 14.0 14.0 14.0	72 90 86 87	2b   2b   55   61   59   52   37   77	9h 75 86 84 60	Tages- mittel 67 79 76 66 64	19h  N   SSW   0 0 0 0 1 WXW	SE 2 NE 1 NE 2	es Winde
Tag  1 2 3 4 5 6 7	Dun  19 <sup>h</sup> 10.2 15.5 11.6 14.5 14.2 12.6 10.7	20 12.9 13.5 14.2 16.7 13.1 12.2	9 <sup>h</sup> 14.2 12.9 16.1 14.6 12.4 10.1	Tages-mittel  mn 12.4 14.0 15.1 14.0 15.2 12.4 10.7	72 90 86 87 75 77 84	26 26 26 27 27 27 26 26 26 27 27 26 26 27 27 26 26 27 27 26 27 27 26 27 27 26 27 27 27 26 27 27 27 26 27 27 27 26 27 27 27 26 27 27 27 26 27 27 27 27 26 27 27 27 27 27 27 27 27 27 27 27 27 27	9h  75 86 84 60 81	Tages-mittel  67 79 76 66 64 85	19h  N   SSW   0   S   1   WXW   1   N   2	SE 2  SE 2  NE 1  NE 1  NE 2  NE 3	es Winde
Tag  1 2 3 4 5 6 7 8	Dun 19 <sup>h</sup> 10.2 15.5 11.6 14.5 14.2 12.6 10.7 9.9	2h 12.9 13.5 14.2 16.7 13.1 12.2 11.2	9 <sup>4</sup> 14.2 12.9 16.1 14.1 14.6 12.4 10.1 12.1	Tages-mittel  mn 12.4 14.0 14.0 15.1 14.0 12.4 10.7 10.4	72 90 86 87 75 77 84	2b   2b   55   61   59   52   37   77   96   50   50	9h  75 86 84 60 81 100 90 82	Tages- mittel  67 79 76 66 64 85 90 72	Richtung   196	SE 2 SE 2 NE 1 NE 1 NW 3 NW 3	ene (NNW )
Tag  1 2 3 4 5 6 7 8 9	Dun 19 <sup>h</sup> 10.2 15.5 11.6 14.5 14.2 12.6 10.7 9.9 10.3	2h 12.9 13.5 14.2 16.7 13.1 12.2 11.2 9.3	9 <sup>t</sup> 44.2 12.9 16.1 14.6 12.4 10.1 13.3	Tages-mittel  m 12.4 14.0 15.1 14-0 15.1 10-7 10-4 11.5	72 90 86 87 75 77 84 85	2b   25   55   61   59   52   37   77   96   50   45	9h  75 86 84 60 81 100 90 82	Tages- mittel  67 79 76 66 64 85 90 72 65	19h  N   SSW   0 0 S   WNW   N   SSE	SE 2  SE 2  NE 1  NE 1  NE 2  NE 3	es Winde
Tag	Dun  19 <sup>h</sup> 10.2 15.5 11.5 14.5 14.2 12.6 10.7 9.9 10.3 10.7	2h 12-9 13-5 14-2 16-7 13-1 12-2 11-2 9-3 10-9 11-8	9 <sup>t</sup> 44.2 12.9 16.1 14.1 14.6 12.4 10.1 13.3 14.2	Tages-mittel  m 12.4 14.0 15.1 14.0 15.1 14.0 12.4 10.7 10.4 11.5 12.2	72 90 86 87 75 77 84 85 76 65	2b   25   55   61   59   52   37   77   76   50   45   38	9h  75 86 84 60 81 100 90 82 75 85	Tages-mittel  67 79 76 66 64 85 90 72 65 63	Richtung   19 <sup>h</sup>	SE 2  SE 2  SE 1  NE 1  NE 1  NE 1  NE 1  NE 1  NE 1  SE 2  NW 3  NW 4  SSE 1	ENE INNW IN
Tag  1 2 3 4 5 6 7 8 9 10 11	Dun  19h  10.2 15.5 11.6 14.5 14.2 12.6 10.7 9.9 10.3 10.7 13.8	2h 12.9 13.5 14.2 16.7 13.1 12.2 11.2 9.3 10.9 11.8	9 <sup>t</sup> 14.2 12.9 16.1 14.6 12.4 10.4 12.1 13.3	Tages- mittel  12-4 14-0 15-1 14-0 15-1 14-0 12-4 10-7 10-4 11-5 12-2 13-3	72 90 86 87 75 77 84 85 65 89	2b   2b   55   56   57   57   57   57   57   57	9h  75 86 84 60 81 100 90 82 75 85	Tages- mittel 67 79 76 66 64 85 90 72 65 63 84	Richtung  19h  N   SSW   0 S   WNW   SSE   SSE   0	SE 2 SE 1 NW 3 NW 1 SSE 1 NNW 1	ene Winde
Tag  1 2 3 4 5 6 7 8 9 10 11 12	Dun  19 <sup>h</sup> 10.2 15.5 11.6 14.5 14.5 14.7 12.6 10.7 9.9 10.3 10.7 13.8 9.1	2h 12.9 13.5 14.2 16.7 13.1 12.2 11.2 9.3 10.9 11.8	9 <sup>t</sup> 44.2 12.9 16.1 14.1 14.6 12.4 10.1 13.3 14.2	Tages-mittel  an 12.4 14.0 15.1 14.0 15.2 14.0 12.4 10.7 10.4 61.5 12.2 13.3 8.2	72 90 86 87 75 77 84 85 76 65 89	2b   25   55   61   59   52   37   77   76   50   45   38	9h 75 86 84 60 90 90 82 75 85 63	Tages-mittel  67 79 76 66 64 85 90 72 65 63	Richtung  19h  N   SSW   0 S   WNW   SSE   SSE   SSE   SSE   NW 3 SW 1	SE 2 SE 1 NW 3 NW 2 NNW 2	es Winde
Tag  1 2 3 4 5 6 7 7 8 9 10 11 12 13 14	Dun  19h  10.2 15.5 11.6 14.5 14.2 12.6 10.7 9.9 10.3 10.7 13.8	2h 12.9 13.5 14.2 16.7 13.1 12.2 11.2 9.3 10.9 11.8 12.4 7.2 7.8	9 <sup>h</sup> 14.2 12.9 16.1 14.1 14.6 12.4 10.1 13.3 14.2 13.8 8.4	Tages-mittel  an 12.4 14.0 15.1 14.0 15.1 10.7 10.4 (1.5 12.2 13.3 8.2 9.1 10.4	72 90 86 87 75 77 84 85 85 70 70 77	2b   25   55   61   59   52   37   77   96   50   45   38   79   46	9h  75 86 84 60 81 100 90 82 75 85 85 63 71	Tages-mittel  67 79 76 66 64 85 90 65 63 84 60 64 71	Richtung  19 <sup>h</sup> N   SSW   0 0 S   WNW   SSE   SSE   0 3 SW   NNE   NNE	SE 2 SE 2 SE 2 NE 1 NE 1 NW 1 NNW 2	9%  ENE   NNW   N   S   NNE   N   S   NNE   NNW   N   S   NNE   NNW   NN
Tag  1 2 3 4 5 6 7 8 9 10 11 12 13	Dun  19h  10.2 15.5 15.5 14.2 12.6 10.7 9.9 10.3 10.7 13.8 9.1	2h 12.9 13.5 14.2 16.7 13.1 12.2 9.3 10.9 11.8 12.4 7.2 7.8	9 <sup>h</sup> 14.2 12.9 16.1 14.6 12.1 14.6 12.1 13.8 8.4	Tages-mittel  14.0 14.0 14.0 15.1 14.0 12.4 10.7 10.4 11.5 12.2 13.3 8.2 9.1	72 90 86 87 75 77 84 85 85 70 70 77	2b   2b   55   61   59   52   37   77   66   50   45   38   79   46   44	9h  75 86 84 60 81 100 90 82 75 85 85	Tages-mittel  67 79 76 66 64 85 90 72 65 63 84 60 64	Richtung  19h  N   SSW   0 S   WNW   SSE   SSE   SSE   SSE   NW 3 SW 1	SE 2 SE 1 NW 3 NW 2 NNW 2	9%  ENE   NNW   N   S   NNE   N   S   NNE   NNW   N   S   NNE   NNW   NN
Tag  1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16	Dun  19 <sup>h</sup> 10.2 15.5 11.5 14.5 14.2 12.6 10.7 9.9 10.3 10.7 13.8 9.1 9.5 10.2	2h 12-9 13-5 14-2 16-7 13-1 12-2 11-2 9-3 10-9 11-8 12-4 7-2 7-8 10-2 8-7	9 <sup>t</sup> 14.2 12.9 16.1 14.1 14.6 12.4 10.1 13.3 14.2 13.8 8.4 10.1 10.8	Tages-mittel  an 12.4 14.0 15.1 14.0 15.1 10.7 10.4 (1.5 12.2 13.3 8.2 9.1 10.4	72 90 86 87 75 77 84 85 76 65 89 70	2b   25   55   61   59   52   37   77   96   50   45   8   79   46   44   45   77   77   77   78   78   78   78   7	9h  75 86 84 60 81 100 90 82 75 85 85 63 71	Tages-mittel  67 79 66 64 85 90 72 65 63 84 60 64 71 69	Richtung   19 <sup>k</sup>	U. Stärke (Skala: 0 - 1)  25  SE 2	SW   1
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Tag  1 2 3 4	12 <sup>h</sup> 46.5 40.5 45.1 42.1	14 <sup>k</sup> 46.2 40.0 44.6 42.3	45.7 39.7 44.1 42.4	18 <sup>b</sup> 45.7 40.0 44.1 42.4	45-3 40-5 44-1 42-8	b) tdruc  22 <sup>k</sup> 45.3 40.8 43.8 42.8	Autogr k auf of oh 11.6 41.6 41.3 43.3 42.2	raphis reduzio 2h 43.6 41.1 42.2 41.8	che Au ert in Mi  4h  42.8 41.8 42.0 40.9	6h 42.2 43.0 41.4	5 <sup>h</sup> 41.8 44.3 41.7 40.0	10 <sup>k</sup> 41.7 44.5 41.9 39.9	mittel 44.28 41.48 43.19 41.63	46.5 45.1 45.1 42.8	40. 39. 41. 39.
Tag	46.5 40.5 45.1 42.1 39.8 38.0	14 <sup>k</sup> 46.2 40.0 44.6 42.3 39.7	45.7 39.7 44.1 42.4 39.7 40.2	18 <sup>b</sup> 45.7 40.0 44.1 42.4 40.2	20 <sup>h</sup> 45.3 40.5 44.1 42.8 40.5 42.6	b) tdruc 22 <sup>k</sup> 25.3 40.8 43.8 42.8 40.4 43.1	Autogr k auf o° ob 44.6 41.3 43.3 42.2 40.3 43.4	raphis reduzie 2h 43.6 41.1 42.2 41.8 39.8 43.4	4k 4k 42.8 41.8 42.0 40.9 39.2 43.1	6h 42.2 43.0 41.4 40.1 40.0	6 <sup>h</sup> 41.8 44.3 41.7 40.0 39.8 42.7	10 <sup>k</sup> 41.7 44.8 41.9 39.9 39.5 43.6	mittel 44.28 41.48 43.19 41.63 39.91	46.5 45.1 45.1 42.8 40.5	40. 39. 41. 39. 38.
Tag  1 2 3 4 5	12 <sup>h</sup> 46.5 40-5 45-1 42.1 39-8 38.9 42.5 47-9 47-9	14 <sup>k</sup> mn 46.2 40.0 44.6 42.3 39.7 39.4 42.6 48.0 49.2	45-7 39-7 44-1 42-4 39-7 40-2 42-7 48-2 49-1	18 <sup>b</sup> 45.7 40.0 44.1 42.4 40.2 41.4 43.3 48.5 49.7	20 <sup>h</sup> 45·3 40·5 44·1 42·8 40·5 42·6 44·0 49·1 50·0	b) 't d r u cl 22 <sup>h</sup> 45.3 40.8 43.8 42.8 40.4 43.1 44.9 49.3	Autog:  44.6 41.3 43.3 42.2 40.3 43.4 45.8 49.1	raphis reduzio 2h 43.6 41.1 42.2 41.8 39.8 43.4 46.1 48.6 48.4	che Au ert in Mi 4 <sup>h</sup> 42.8 41.8 41.8 42.9 39.2 43.1 46.6 48.5 47.9	6h 42.2 43.0 41.4 40.1	5 <sup>h</sup> 41.8 44.3 41.7 40.0 39.8 42.7 47.5 48.6 47.7	10 <sup>h</sup> 41.7 44.8 41.9 39.9 39.5 43.6 48.1 48.7 47.9	mittel 44.28 41.48 43.19 41.63 39.91 42.02 45.08 48.56 48.76	46.5 45.1 45.1 42.8 40.5 43.6 48.1 49.3 50.0	39. 41. 39. 38. 38. 42. 47.
Tag  1 2 3 4 5 6 7 8 9 10 11 12	12 <sup>h</sup> 46.5 40.5 45.1 42.1 39.8 38.9 42.5 47.9 47.9 43.2 44.6	14 <sup>k</sup> mm 46.2 40.0 44.6 42.3 37.7 39.4 42.6 48.0 49.2 47.5 45.0 44.6	45.7 39.7 44.1 42.4 39.7 40.2 42.7 48.2 49.1 47.4 43.5 45.5	18 <sup>b</sup> 45.7 40.0 44.1 42.4 40.2 41.4 43.3 48.5 49.7 47.3 43.2 46.6	20 <sup>h</sup> 45-3 40-5 44-1 42-8 40-5 42-6 44-0 49-1 50-0 47-0	b) tdrucl 22h 45.3 40.8 43.8 42.8 40.4 43.1 44.9 49.3 49.7 46.6 44.8 48.7	Autogr k auf o° ob 44.6 41.3 43.3 43.4 45.8 49.1 49.0 45.6 45.3 48.8	raphin reduze 2h 43.6 41.1 42.2 41.8 39.8 43.4 46.1 48.6 48.4 44.5 45.2 49.4	che Au ert in Mi  4h  4h  42.8  41.8  42.0  40.9  39.2  43.1  40.6  48.5  47.9  43.4  44.7  49.8	8 mn 42.2 43.0 44.4 40.1 40.0 42.4 46.8 48.2 47.5 42.8 43.9 49.9	8 - 700° 84 41.8 44.3 41.7 40.0 39.8 42.7 47.5 48.6 47.7 43.6 44.4 50.6	10 <sup>k</sup> 41.7 44.8 41.9 39.9 39.5 43.6 48.1 48.7 47.9 43.5 44.3 51.3	mittel  44. 28 41. 48 43. 19 41. 63 39. 91 42. 08 45. 56 48. 76 45. 59 44. 29 48. 12	46.5 45.1 45.1 42.8 40.5 43.6 48.1 49.3 50.0 47.9	40. 30. 41. 39. 38. 42. 47. 47. 42.
Tag  1 2 3 4 5 6 7 8 9 10 11	12 <sup>h</sup> 46.5 40.5 45.1 42.1 39.8 38.9 42.5 47.9 47.9 43.2 44.6 51.7 52.5 50.5	14 <sup>k</sup> 46.2 40.0 44.6 42.3 39.7 39.4 42.6 48.0 49.2 47.5 45.0 52.0 52.4 50.3	45.7 39.7 44.1 42.4 39.7 40.2 42.7 48.2 49.1 47.4 43.5 45.5 51.9 52.3 50.0	18 <sup>b</sup> 45.7 40.0 44.1 42.4 40.2 41.4 43.3 48.5 49.7 47.3 43.2 46.6 52.4 52.4 52.4 50.0	20 <sup>h</sup> 45-3 40-5 44-1 42-8 40-5 42-6 44-0 49-1 50-0 47-0 44-0 47-0 52-9 52-4 50-3	b) tdruci 22 <sup>k</sup> 40.8 43.8 42.8 40.4 43.1 44.9 49.7 46.6 44.8 7 53.0 52.3 50.1	Autogram Aut	raphin reduzie 2h 43.6 41.1 42.2 41.8 39.8 43.4 46.1 48.4 44.5 45.2	che Au ert in Mi  4h  42.8 41.8 42.0 40.9 39.2 43.1 45.6 48.5 47.9 43.4 44.7	6h 42.2 43.0 41.4 40.0 42.4 46.8 48.2 47.5 42.8 43.9	64 41.8 44.3 41.7 40.0 39.8 42.7 47.5 48.6 47.7 43.6	10 <sup>k</sup> 41.7 44.8 41.9 39.9 39.5 43.6 48.7 47.9 43.5	mittel 44. 28 41. 48 43. 19 41. 63 39. 91 42. 02 45. 08 48. 56 48. 76 45. 59 44. 29	46.5 45.1 42.8 40.5 43.6 48.1 49.3 50.0 47.9	40. 30. 41. 39. 38. 42. 47. 42. 42. 44. 51.
Tag  1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18	12 <sup>h</sup> 46.5 40-5 45-1 42-1 39-8 38-9 47-9 47-9 47-9 43-2 44-6 51-7 52-5 47-3 44-4 47-3	14 <sup>1</sup> 46.2 40.0 44.6 42.3 39.7 42.6 48.0 49.2 47.5 45.0 44.6 52.0 52.0 52.1 50.3 46.9 44.5 47.5	45.7 39.7 44.1 43.4 39.7 40.2 42.7 48.2 49.1 47.4 43.5 45.5 51.9 52.3 50.0 46.6 47.5	18 <sup>b</sup> 45.7 40.0 44.1 42.4 40.2 41.4 43.3 48.5 49.7 47.3 43.2 46.6 52.4 52.4 52.4 52.4 52.4 52.4 52.4 52.4	20 <sup>h</sup> 45-3 40-5 44-1 42-8 40-5 42-6 44-0 49-1 50-0 47-0 47-0 47-0 52-9 52-4 50-3 46-4 45-0 48-2	b) tdruc 22h 45.3 40.8 43.8 42.8 40.4 43.1 44.9 49.7 46.6 44.8 48.7 53.0 52.3 65.1 46.3 45.4 48.4	Autog: k auf o° 44.6 41.3 43.3 43.3 43.3 43.8 49.1 45.8 49.1 45.6 45.3 48.8 52.6 51.9 49.4 45.5 48.8 49.1	raphis reduzie 2h 43.6 41.1 42.2 41.8 39.8 43.4 46.1 48.4 44.5 45.2 45.2 45.2 45.2 48.6 44.9 46.0 47.6	che Au ert in Mi  4h  42.8 41.8 42.0 40.9 49.2 43.1 46.6 48.5 47.9 44.7 49.8 50.7 47.9 44.1 45.6 47.1	6h 42.2 43.0 44.4 40.1 40.0 42.4 46.8 47.5 42.6 47.5 42.9 47.5 43.9 40.9 51.8 50.4 47.5 43.9 40.0	64 41.8 44.3 44.7 40.0 39.8 42.7 47.5 48.6 47.7 43.6 44.4 50.6 52.2 50.3 47.5 44.1 46.8	10 <sup>h</sup> 41.7 44.8 41.9 39.9 39.5 43.6 48.7 47.9 44.3 51.3 52.5 50.5 47.0 44.3 47.0	mittel 44-28 41-48 41-48 43-19 41-63 39-91 42-02 45-05 45-56 48-76 45-59 44-29 48-12 51-63 49-14 45-58 45-48 47-58	46.5 45.1 45.1 42.8 40.5 43.6 45.1 49.3 50.0 47.3 51.7 53.0 52.5 50.5	40. 39. 41. 39. 38. 42. 47. 42. 42. 44. 51. 50. 47.
Tag  1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20	12 <sup>h</sup> 46.5 40.5 45.1 42.1 38.9 42.5 47.9 47.0 47.9 43.2 44.6 51.7 52.5 50.5 47.3 44.4 47.3 47.4	14 <sup>1</sup> 46.2 40.0 44.6 42.3 39.7 39.4 42.6 49.2 47.5 45.0 52.0 52.0 52.0 46.9 44.5 47.9	45.7 39.7 44.1 42.4 42.7 40.2 42.7 48.1 47.4 43.5 45.5 51.9 52.3 50.0 44.6 47.5 46.9 44.6 47.5 46.9	45.7 40.0 44.1 42.4 40.2 41.4 43.3 48.5 49.7 47.3 43.2 46.6 52.4 50.0 46.3 44.5 47.8 46.1 48.4	20h 45-3 40-5 44-1 42-8 40-5 42-6 44-0 47-0 47-0 47-0 52-9 52-4 50-3 46-4 45-8 48-3	b) tdrucl 22 <sup>k</sup> 45.3 40.8 43.8 42.8 40.4 43.1 44.9 49.7 46.6 44.8 45.7 53.0 50.1 46.3 45.4 45.2 47.7	Autog: k auf o° oh 44.6 41.3 43.3 42.2 40.3 43.8 49.1 49.0 45.8 49.1 49.0 45.6 45.3 48.8 52.6 51.9 49.4 44.6 45.8 48.8 49.1 49.0 48.8 49.1 49.0 49	raphis reduzis 2h 43.6 41.1 42.2 41.8 39.8 46.1 48.6 44.5 45.2 41.8 52.1 51.4 48.6 44.9 47.6 43.5 45.5	che Au ert in Mi  4 <sup>h</sup> 42.8 41.8 42.0 40.9 39.2 43.1 45.6 48.5 47.9 43.4 44.7 49.8 51.8 50.7 47.9 44.1 45.5 47.1 43.6 44.6	6h 47.2 43.0 41.4 40.1 40.0 42.4 46.8 2 47.5 42.8 43.9 49.9 51.8 50.4 47.5 43.9 40.0 46.7 43.6 43.7 43.9 49.9 51.8 50.4 47.5 43.9 49.9 51.8 50.4 47.5 43.9 49.9 51.8 50.4 47.5 43.9 49.9 51.8 50.4 47.5 43.9 49.9 51.8 50.4 47.5 43.9 49.9 51.8 50.4 47.5 43.9 49.9 51.8 50.4 47.5 43.8 43.9 49.9 51.8 50.4 47.5 43.8 43.9 49.9 51.8 50.4 47.5 50.4 43.8 50.9 49.9 51.8 43.8 43.8 60.0 46.7 40.0 46.7 40.0 40.0 40.0 40.0 40.0 40.0 40.0 40	64 41.8 44.3 41.7 40.0 39.8 42.7 47.5 48.6 47.7 43.6 44.4 50.6 52.2 47.5 44.1 44.4 45.0 44.4 46.8 47.1 46.8 47.1 45.0 44.4	10 <sup>h</sup> 41.7 44.8 41.9 39.9 43.6 48.1 48.7 47.9 43.5 44.3 51.3 52.5 50.6 47.0 47.1 46.6 43.7	#44.28 44.28 41.48 43.163 41.63 39.91 42.62 45.08 45.56 45.56 45.59 44.29 48.12 52.24 51.63 45.48 47.52 45.48 47.52 45.38	46.5 45.1 42.8 40.5 43.6 45.1 49.3 50.0 47.9 45.3 51.7 53.0 52.5 47.3 48.4 47.1	40. 39. 36. 38. 47. 47. 42. 42. 44. 51. 50. 47. 43. 44.
Tag  1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18	12 <sup>h</sup> 46.5 40-5 45-1 42-1 39-8 38-9 47-9 47-9 43-2 44-6 51-7 52-5 50-5 47-3 44-4 47-3 47-1	14 <sup>k</sup> 46.2 40.0 44.6 42.3 39.7 39.4 42.6 48.0 44.6 52.0 52.4 50.3 46.9 44.5 47.5	45.7 39.7 44.1 42.4 42.7 40.2 42.7 48.1 47.4 43.5 45.5 51.9 52.3 50.0 44.6 47.5 46.9	18 <sup>b</sup> 45.7 40.0 44.1 42.4 40.2 41.4 43.3 48.5 49.7 47.3 46.6 52.4 50.0 46.3 47.8 46.5	20 <sup>h</sup> 45.3 40.5 44.1 42.8 40.5 42.6 44.0 47.0 47.0 47.0 47.0 47.0 47.0 47.0	b) tdrucl 22 <sup>k</sup> 45.3 40.8 43.8 42.8 40.4 43.1 44.9 49.7 46.6 45.2 45.4 45.4 45.4 45.2	Autog: k auf o° oh 44.6 41.3 42.3 42.3 42.3 49.1 49.0 45.8 49.1 49.0 45.8 49.1 49.0 45.8 49.1 49.0 45.8 49.1 49.0 45.8 49.1 45.8 45.8 45.8 45.8 45.8 45.8 45.8 45.8	raphis reduzie 2h 43.6 41.1 47.2 41.8 39.8 43.4 46.1 48.6 44.5 45.2 49.4 52.1 51.4 48.6 44.9 46.0 47.6 43.5	che Au ert in Mi  4 <sup>h</sup> 42.8 41.8 42.0 40.9 39.2 43.1 40.6 48.5 47.9 43.4 44.7 49.8 51.8 50.7 47.9 44.1 45.5 47.1 45.5	6h 42.2 43.0 41.4 40.1 40.0 42.4 46.8 48.2 47.5 43.9 49.9 51.8 50.4 47.5 43.9 49.9 49.9 49.9 49.9 49.9 49.9 49.9	64 41.8 44.3 41.7 40.0 39.8 42.7 47.5 48.6 47.7 43.6 44.4 50.6 52.2 50.3 47.5 44.1 46.8 47.1 46.8	10 <sup>h</sup> 41.7 44.7 44.7 44.9 39.9 43.6 48.1 48.7 47.9 43.5 44.3 51.3 52.5 50.5 47.0 47.1 40.6	mittel 44-28 44-28 44-28 41-48 43-19 41-63 39-91 42-62 45-65 48-76 45-59 44-29 48-12 52-24 51-63 49-14 45-58 45-48 47-52 45-31	46.5 45.1 45.1 42.8 40.5 43.6 49.3 50.0 47.9 45.3 51.0 52.5 50.5 47.3 47.3 48.4 47.1	40.0 40.0 41.399.386.38.42.47.42.44.51.50.47.42.44.51.43.44.44.64.45.43.43.44.45.43.43.44.45.43.43.44.45.43.43.44.45.43.43.44.45.43.43.44.45.43.43.44.45.43.43.44.45.43.43.44.45.43.43.44.45.43.43.44.45.43.43.44.45.43.43.43.44.45.43.43.43.43.43.43.43.43.43.43.43.43.43.
1 2 3 4 4 5 6 7 7 8 9 10 11 12 13 14 15 16 17 19 20 12 22 23 24	12 <sup>h</sup> 46.5 40.5 40.5 45.1 42.1 39.8 38.9 47.9 47.9 43.2 47.3 44.6 51.7 52.5 50.5 47.3 44.4 47.3 47.1 44.9 48.3 45.4	14 <sup>1</sup> 40.0 46.2 40.0 44.6 42.3 39.7 39.7 48.0 48.0 47.5 45.0 52.0 47.5 52.4 47.3 47.3 47.3 47.3 47.3 47.3 47.3 47	45-7 39-7 44-1 42-4 39-7 48-2 49-1 47-4 43-5 45-5 51-9 52-3 50-0 44-6 47-5 46-3 48-2 46-3 48-2 46-3 47-9 44-7 45-7	18 <sup>b</sup> 45.7 45.7 40.0 44.1 40.2 41.4 40.2 41.4 40.2 41.4 40.2 41.4 52.4 47.3 43.3 43.5 52.4 47.8 46.6 52.4 47.8 47.8 43.4	20 <sup>h</sup> 45-3 40-5 44-1 42-8 40-5 44-0 47-6 52-9 47-0 44-0 47-6 52-9 45-0 48-2 45-0 48-3 47-7 43-9 40-2	b) b) mm 45.3 mm 45.3 mm 45.4 mm 45.8 mm 45.8 mm 47.8	Autogr k auf o° ob 44.6 41.3 42.2 40.3 43.4 45.8 49.1 49.0 45.8 49.1 49.0 45.6 51.6 51.6 45.8 49.1 45.6 41.3 44.6 45.8 49.1 45.6 45.8 49.1 45.6 45.8 49.1 45.6 45.6 45.8 49.1 45.6 45.8 49.1 45.6 45.8 49.1 45.6 45.8 49.1 45.6 45.8 49.1 45.6 45.8 49.1 45.6 45.8 47.0 47	raphii reduzie  26  43.6  41.1  42.2  43.4  44.8  43.9  43.4  44.5  45.2  45.2  45.2  46.0  47.0  48.6  44.9  45.5  45.1  46.0  47.0  48.4  44.7  48.4  44.7	che Au ert in Mi  4 <sup>h</sup> 2.8 41.8 42.8 41.8 42.0 40.9 39.2 43.1 46.6 48.5 47.9 44.7 49.8 50.7 47.9 44.1 43.6 48.3 45.5 43.0 44.0	6h 47.2 43.2 43.4 40.1 40.0 42.4 46.8 46.8 47.5 42.4 47.5 42.4 47.5 42.4 47.5 42.4 47.5 42.4 47.5 42.4 43.9 49.9 51.8 50.4 47.5 43.6 44.0 45.8 44.0 46.0 46.0 46.0 46.0 46.0 46.0 46.0	84.8 44.8 44.3 41.7 40.0 39.8 42.7 47.5 48.0 47.7 43.6 52.2 44.1 46.8 47.1 46.8 47.1 46.8 47.1 46.9 44.4 47.9 44.4	10 <sup>h</sup> 41.7 44.8 41.9 39.9 39.5 43.6 48.7 47.9 43.5 44.3 51.3 52.5 50.5 47.0 47.0 47.0 48.7 48.7 48.7 48.8	mittel  44.28 41.48 43.19 41.63 39.91 42.62 45.66 48.76 45.59 44.29 48.12 51.63 49.14 45.58 45.58 46.75 46.39 47.57 46.75	46.5 45.1 42.8 40.5 43.6 45.1 49.3 50.0 47.9 45.3 58.7 58.7 47.3 48.4 49.2 49.3 45.3 45.4 46.2	Min 100 100 100 100 100 100 100 100 100 10

							-	tudes:								1905
						L	ufttem	perati	ar na	ch Celsi	us					
Tag	12h	144	16)	183	203	22h	O.L	23-	46	64	81		10 <sup>h</sup>	Tages- mittel	Max.	Min.
1	17.5	16.0	16.2	16,0	17.6	19.8	23.1	25.2	25.	7 24	3 22		1.0	20.44	25.7	15.6
2	20.5	19.8	19.5	19.8	20.5	23.6	21.9	23.9	21.	5 18.	7 18	.1 1	17.2	20.42	24.6	16.5
3	16.5	15.9	15.4	18.6		21.1	23.4	30.4	31.	3 30.		.2 1	24.4	20.45	26.3	18.2
3	22.5	21.5	20.5	20.4		28.6	30.5	32.0	27.	3 23.	3 22	3	20.3	24.45	31.6	20.0
6	20.0	20.2	19.6	18.2	19.1	19.0	18.8	18.6	16.				14.6	18.00	20.3	14.5
7	14.5	14.2	14.5	14.8	14.8	13.6	13.7	13.8	13.	8 13.	9 13	.8	13.5	14.08	15.1	13.1
	13.6	13.6	13.6	13.7	14.8	17.5	19.9	21.2	21.	6 20.	9 18	.8	16.9	17.19	21.7	13.6
9	15.9	15.2	17.6	14.8		25.3	24.3	25.8	25.	7 24.			19.6	19.99	25.8	14.5
	18,4	16.8	17.3	17.7		18.6	19.1	18.4	19.				19.1	18,66	20.5	16.7
12	18.4	17.2	16.3	15.5	15.3	16,5	17.6	18.6	18.	5 18.			14.9	16.94	18.6	14.5
13	14.5	14.6	14.4	14.5	15.0	17.6	19.6	20.3	20.	5   19.		.6	10.3	17.05	20.9	14.4
14	15.4	14.9	14.4	14.7		18.4	21.6	20.2	20.				16.1	15.15	20.7	13.5
15						21.0							10.6		1	
17	15.5	14.4	13.7	13.0		18.0	23.9	25.1 10.8	25.	0 23.				19.36	25.2	13.5
18	15.6	15.4	15.4	15.3	16.4	18.3	20.1	21.7	22.			.3	15.9	18.35	22.9	1 15.3
19	16.9	16.1	15.7	16.1		23.1	25.1	26,2	23.	8 20.	7 18	.7	7 - 4	19.87	26.2	15.5
20	16.1	15.3	14.0	13.4		19.7	21.9	22.5	22.				17-4	18.32	22.9	13.3
21	16.6	16.4	16,4	16.1	17.7	18.2 20.1	19.6	20.6	24.				16.2	18,13	20.8	15.2
23	15.2	14.5	16.3	15.0		24.3	26.7	26.6	25.		5 23		19.5	21.28	26.0	14.3
24	15,2	16.4	15.6	15.0	17.6	19.6	21.2	22.5	22.	5 20.	1 16	.8	16.0	18.51	22.8	15.5
25	15.8	15.2	14.3	13.2		18.4	20,2	21.4	21.				17-5	17.72	21.7	13.2
26	16.5	16.0	15.3	15.5	17.3	20.8	23.1	24.8	24.	5 22.		4	18.9	19.52	25.3	14.8
27	18.1	17.5	17.2	17.3	19.1	19.8	21.6	21.5	21.	8 20		9	16.7	18.26	22.0	16.7
29	17.0	16.2	14.1	12.0	13.4	14.7	10.5	17.2	18.	0 15	8 16	.7	12.6	15.43	18.0	12.2
30	12.2	12.7	12.7	12,4		14.8	16.7	16.8	17.	4 16.	3 15	.6	14.8	14.67	17.6	12.2
31	14.9	14.5	13-7	13.6	5 14.6	14.6	15.5	15.6	15.	5 14.	7 14	-7	14-5	14.70	15.7	13.5
d.M.	16.89	16.29	15.71	15.5	17.22	19.72	21.46	22.42	22.	19 20.	90 18	.89	7-49	18.73	22.94	14.9
			Disk		(R), Ges	ch wind	intrale.	(C) den	Mr:	des in	Calena	de la				1
Tag	12 <sup>h</sup>	1				204	226			des m	1 SCAU	ide in			101	Tag
	R G	R 14 <sup>th</sup>	$G \mid R$	G	R G	R G	R (	7 R	6	R G		0 1	6 k G	R St	7 R	G G
	NNW 1.	NYW .	0.9 NNW		N 1.0	N 1.4	N o	. S ESE	1.2	ESE 1.	8 ESE	3.3 E	SE 2.1	ESE I	.4 ENE	
3	E o.	S XW	0.5	0.0	S 0.5	SW 1.4 SSE 0.4	ESE 2	.o ESE	2.6	SSE 1.	NW ENE	5.0 N	SE L	N I	, O A	0.7 1.
4	··· 0.	0 (	0.0	0.0	*** 0.0	E 0.2	ENE 1	. 4 ENE	2.6	E 2.	SSE :	2.1 S	SE 1.3	ESE 1	.o. SW	0.7 1.4
5	SSE o.				SSW 0.5	SSE 0.8			1,8	ENE 2.	1	4.5 767	W 5.0	Л а		3.3 1.9
6	X 2.	NW .	3.2 NXW	2.3	NNW 3.1	WNW 2.0	N 3	.o NNE		NNE 3.	6 N	3.6	N 5.7	N 4	.4 NNE	2.1 3.1
3	WSW 1.	SSW	O E WSW	3.0	N 4.2 WSW 1.0	N 4.6	WSW 0	O NNW	3.7	NNW 3.	WXW	2.7	SE 0.	WNW 2		0.0 0.
9	SE o.	7 8	1.4 851	0.4	SSE 0.4	SSE 0.7	SSW I	.9 SW	2.1	S 2.	4 S	1.1 8	SE 1.1	SSW o	. 4	0.0
10	SSW 1.				SSW 1.6	\$ 2.8				S 2.		2.5 WN				
11	N 2.	MAM.	4.9 881	1.2	NNE 1.2	WSW 2.1	₩ 2	. 5 WSW	2.3	NNW 2.	2 NW	0.2 8	SE o.8	NNW I	WXW O.	1.4 1.7
13	NNW o.	S NAW	2.3 NNI	2.5	WSW 0.6	NNW 3.6 SSW 0.6	SSW o	8 11	1.8	NNW 3.	NNW	3.5	W 2.1	NNE o	O NNE	0.5 2.4
14	0.1	0 *** 6	0.0 111	0.2	*** 0.0	NNE o.8	NE L	.o ENE	1.8	SE 2.	ESE	1.0 E	SE 1.6	ESE I	.0	0.0 0.1
15	ESE o.			0.5	SSE 0.3	SSE 0. 2		-3 E	2.0	NNE 1.	NNE	1.7 E	NE 1.5	0		0.2 0.1
16	SSE 1.	SSE I	1.0.	0.5	× 0.5	SSW 1.4	SSW L		2.0	S 1.	WSW	. o WS	W o.:	0		1.8 1.
17	N 2.0	NNW a	0.9	0.7	NAW 1.3	NNW 1.6	ENE 1	S NNE	1.2	NE 3.	NE NE	1.1 N	E 3.0	NNE 1	-7 N	0.4 1.3
19	SSE O.	S	0.8. 2	1.60	8 0.6	SSE 1.8	SSW 2	.2 515	2.3	W 2.	WAW	. 4 WX	W 1.8	NW 3	. 2 NW	2,2 2.0
20	WNW 2.	WNW :	2.5 SSW	1.6	SSE 0.6	\$ 1.0	WSW 2	. 5 W	2.5	NSW 2.			W 1.4	10	.9 SSW	2.3 1.9
21	NNW o.	WWW :	3.5 WYW	2.4	WNW 2.8	XXW 3.0	NE 2	.6 N	2.0	VXW 2.	NNE :	1.4	N o.6	NNE o	.6 NNE	0.4 1.5
22	SSE o.	SSE	0.4 WSW	0.4	E 1.3	ENE 1.7 SSE 1.6	ENE I	4 SSE	1.6	SSE 1. W 2.	NAW :	.9	SE 2.0	SSE I	O SSE	2.6 1.6
23	WAW 4.1	WYW :	2.0 SSW	1.0	SSW 0.61	WNW L.I	NAW L	SWSW	2.1	W 2.		AWN	W 2.1	WNW 2	T W.A.M.	1.0 1.5
25	SSW 1	SSW	LO WSW	0.4	SSW 1.5	SSW 0.7	WSW 1	O NNW	0.7	NNW I.	WSW	.1	E 2.2	Eo	.5	
26	E o	ENE o	o.9 ENE	1.4	ENE 0.6	ENE 1.3	NNE 1.	. 2 NW	1.1	ENE o.	ESE I	.3 E	SE o. s	WNW 4	WKH O.	0.4 1.2
27	W 0.		2.0 1	2.5	W 2.9	W 4.5	WYW 5	8 1	4.5 V	NW 5.	H 4	0.1	W 4.1	WSW I	,1 WSW	
28	WNW 3.	SSW :	2.4 NI	2.7	SSW 1.5 WSW 2.4	WSW 3.2	WSW 2.	S SW	4.1	SW 4.	WSW 4	0 55	W 0.6	WSW 2	. s SW	2.8 3.2
30	WSW 3.0	SW	1. 1 WSW	4.7	WSW 5.5	W 4.S	WSW 4	. 81 W	5.6 V	VAN 7.1		. 2	W 5.3	W 4	. I WSW	3.7 4.8
31	W 6.	W	5-5 1	4.6	W 3.8	W 5.5	W 5.	. 5 W	5.2 V	VNW 4-	W.Z.M.	. 5 W.N	W 2.1	W 2	.5 WXW	3.0 4.4
.м.	1.50	1.	.63	1.45	1.39	1.80	2.7	11	2.51	2.5	. 2.	53	2 10	1.	49 1	22 1.8
- 1		1 "	~				, ,,,		9.1		1		- /-			

			a) I	Direkte Ablesus	ngen			
	Luftdru	ck auf o' redu	riert in Millim.	= 700° +	I.	ufttemperat	ur nach Cel	sius
Tag	19 <sup>h</sup>	21	94	Tagesmittel	19 <sup>h</sup>	2 h	94	Tagesmitte
	546	46.8	46.0	46.50	. 1	15.8	13.6	
1	46.7	42.6	40.2		14-3	15.2	13.6	14.57
2	44.1 39.2	39.3	36.9	42.30 35.47	13.0	16.3	15.4	14.00
3 4	38.0	44.7	47.6	43.43	17.0	17.5	14.5	
		45.8	48.8					16.33
5	49.7	45.5		49.10	14.2	20.5	13.5	16.73
6	45.2	45.7	44.5	46,13	14.4	23.0	18.6	18.67
7	44.8	43.7	42.6	43.70	16.3	25.8	18.9	20.33
8	45.7	45.9	48.3	46.63	18.8		15.7	21,30
9	50.6	49.7	47.6	49.30	16.1	19.8	16.1	17.33
10	45.7	44.3	44.1	44.70	15.0	21.7	18.9	18.53
11	46.4	46.6	47.0	46,67	18.2	25 5	19.2	20.97
12	45.1	45.7	50.3	47.03	15.7	25.5	16.2	19.43
13	\$1.4	51.5	51.4	51.43	13.6	15.7	13.8	14.37
14	48.4	45.7	45.1	46,40	14.2	16.9	14.8	15.30
15	45.4	47.1	47.8	46.77	12.0	14.4	13.3	13.23
16	46.6	46.7	47.8	47.03	12.4	14.2	13.2	13.27
17	53.0	51.5	52.1	51.37	5.0	14.0	10.2	11.50
18		51.3	50.2	51.50		15.1	10.8	10.30
10	48.1	44.9	44.1	45.70	6.7	18.2	12.9	12.60
20	43.7	43.6	44.1	43.80	9.2	16.0	13.9	13.03
21	45.3	46.0	47.2	46.17	11.7	16.2	12.2	13.37
22	47.5	46.6	46.4	46.83	7.5	11.8	10.5	9.93
23	44.7	43.5	45.2	43.80	8.0	12.4	8.5	9.63
24	41.6	40.6	40.6	40.03	9.2	16.3	13.0	12.83
25	39.1	39.9	41.2	40.07	11.8	16.4	12.1	13.43
26	41.3	41.8	42.3	41.80	10.4	17.5	13.3	13.83
27	49.3	37 - 7	37 - 9	38,63	9.4	18.1	14.6	14.03
28	40.2	49.6	41.5	40.77	11.7	17.9	12.9	14.17
30	41.9	41.3		41.37	11.3	17.0	13.2	13.80
30	39.1	37-7	36.3	37.70	11.8	14.1	7.9	11.27
dittel	45.08	44.73	44.80	44.87	12.44	17.88	14.02	14.78

Tag	Dun	stdruck	in Million	etern	Re	lative F	euchtig	keit	Rich	tung	u. Stär Skala: o	ke d	es Win	des
	19 <sup>h</sup>	2 <sup>h</sup>	94	Tages- mittel	19 <sup>h</sup>	24	9h	Tages- mittel	19		21		96	
1	9.4	7.0	7.7	N.0	78	53	67	66	W	3	W	3	SW	- 3
2	8.1	8.3	9.2	8.5	7.3	64	79	73	SW	3	NW	í	WSW	3
3	9.9	10,1	10.4	10.1	84	7.3	80	79	3.11	1	W	3	XW	4
4	9.6	9.4	8.8	9.3	67	63	7.2	67	W	3	WNW	4	W	2
5	8.5	9.9	11.6	10.0	71	55	88	71	W	2	***	0	***	ō
6	10.0	11.4	12.4	11.3	81	55	78	72	SE	,	ESE		SSE	
	11.9	12.3	13.4	12.5	80		81	73	SSH		SW	3	SW	i
7 8	12.6	10.5	10.3	11.1	78	50	64	1 61	S	i	11	1	NW.	i
9	11.6	10.3	11.5	1 11 1	85	60	84	76	W		SSW		SW	i
10	10.1	10.9	12.4	16.1	80	57	76	71	8	i l	SW	2	***	ò
11	12.3	12.7	13.5	12.8			82	1 '			SW	2		0
12	12.0	13.5	11.4	12.8	79	53	82	7.	WSW	i	NW	1		1
13	9.2	9.8	10.3	9,8	90 80	53	88	75	3311	2	ANE		411	0
14	10,6	11.4	11.3	11.1	S8	74 80	90	86	NE	1	NE	i .	ANW	3
15	9.4	9.4	9.2	9.3	91	77	81	83	XW	3	N	4		3
16	9.3	9.6	9.1	9.3	88	So		83	NNE	1	N	1	W	
17	0.9	6.1	6.7	6.6			81	66	WNW	i 1	W		WAW	3
18	6.1	6.1	6.7	6.3	74	52 48	72	71	SW	i 1	ENE	3		0
19	5.6	5.2	6.2	5.7	94 77	33	70		ENE	: 1	SE	3	E	2
20	5.0	6.8	7.7	6.8	68	50	65	55	E	i	NE	i	NW	÷
				9					EXE		SSE		ENE	
21	7.8	6.8	6.5	7.0	76	50	62	63	ALA.	:	NE	3	NE	1
22	6,3	5-7	6.5	6.2	8.2	56	69	69	NW	2	SE	1	E	1
23	6.3	5.9 8.6	6.5	6.2	79	55 62	78	71	ENE	1	SE	2	NE	
24	7-3	10.3	9.2	8.4	84		83	76	BAB.		76	0	.415	0
25				9.8	91	74	94			-		-		-
26	8.3	8.4	9.7	8.8	59	56	86	77	***	0	NNW	2	***	0
27	5.4	12.0	11.4	10.6	96	77	92	88	49.5	0	ENE	1	***	0
28	8.5	7.8	9.1	8.5	84	51	83	73	991	0	511	1	***	0
29	8.8	11.1	10.1	10.0	80	77	90	85	SSE	0	SH	1	AW	0
30	9.2	9.6	8.0	8.9	90	80	100	90	351.	1	511	3	3.11	3
Mittel	9.0	9.2	9.6	9.3	82	60	79	74		1.2		1.8		1

Tag	F	Bewölk	ung [S	kala; o: I Wolk	neiter enzug	, 10 = 1	rūb]		Nieder- schlag in		В	c m c	rkung	en	
	19	,	2			gli	Tages	mittel	Milli- metern						
1 2 3 4 5	HS I	0 W	HS I HS I	0 W 0 W 0 W 9 NW 7 W	IS FS FHS	10 W 10 ··· 10 ··· 9 ···		.0	3.3 3.5 0.2	Abends	zeitw.st		D. chmittags	⊕,-⊜,,n	achts @.
6 7 8 9	FHS I	5 9 W 9 W	FHS I	0 W 7 SW 9 W	FS HS FHS HS	7 SW 10 ··· 8 ···	9	.3 .0 .7 .7	5 - 5	Morgen Morgen Abenda	5		s ■ s ■ S¹·⊗, nac	thts gegen	früh 🧔.
11 12 13 14	FS FHS HS	3 3 10 NE	HS I	4 W 0 NW	5	10	5 7 10	.0	11.7 0.6 8.0	Morgen	s = , ,	und 66	M <sub>6</sub> .  4 <sup>1</sup> ♠ und  4 <sup>1</sup> ♠ und  5 <sup>1</sup> ←  ags dunsti  pfen.	d ▲, ፫⊆. ) <sub>j</sub> , g,9ʰ⊕ <sub>c</sub> , n	aclits ().
16 17 18 19	FHS FS S	3	HS I	0 W	FHS	9	1	.7	1.1	Morgen Morgen Morgen	s u. abe	ends ==,	, vormitt.	(2 mit )	
21 22 23 24	HS HS	10 ··· 10 ··· 9 §	FHS HS HS	9 10 10 SE	FS	7 ··· 10 ··· 2 ··· 7 ···	8 10 7 9	.7		Morgen Morgen Abends Morgen	s und a	bends =	is		
25 26 27 28 29	FHS S FHS	9 ··· 10 ··· 5 ···	FIIS FIIS FS	0 W 0 SW 2	FHS FHS FS S	6 ··· 10 ··· 3 ···	8 10 3 10	.3		Morger Morger	s = 1, 2	a, abend	inst.aben  Is = a. I  s = a. H. a. H., z  a. abend  old O.	H., A.	tags 🖦 "
30 Mittel	Ŭ.	8 W	115	6 W		7.2	1	.9	6,3 S. 40.6	Morger	is	A, 23;"-	-01" @	8f=-10= 5	∌.—⊕ <sub>1</sub> .
Tag	12 <sup>h</sup>	145	164	186	Lufte 20h	lruck s	oh oh	eduzier 2 <sup>h</sup>	t in Milli	metern 6a	700 <sup>mm</sup>	10p	Tages- mittel	Max.	Min.
1 2 3 4 5	47.3 45.4 38.8 36.2 48.8	47.0 45.0 38.2 36.0 49.3	46.8 44.8 38.4 36.1 49.3	46.5 44.0 38.7 37.3 49.5	46.9 43.9 39.2 39.0 49.9	47.0 43.9 39.6 41.5 49.9	47.1 43.3 39.6 43.5 49.4	46.8 42.6 39.3 44.7 48.8	46.4 41.7 39.2 45.0 48.7	45.9 40.9 37.9 45.9 48.3	46.1 40.3 37.4 47.3 48.5	45.6 39-5 36.5 48.0 48.6	46.62 42.94 38.57 41.71 49.08	47-3 45-4 39.6 48.8 49-9	45.4 38.8 36.2 36.0 48.3
6 7 8 9	48.6 44.6 42.5 49.0 46.7	48.3 44.4 42.8 49.9 40.2	47.9 43.9 43.9 50.2 45.8	48.1 44.4 44.9 50.2 45.6	48.1 44.5 46.0 51.1 45.6	47.7 44.7 46.5 51.3 43.6	46.9 44.1 40.3 50.8 45.0	45.7 43.7 45.9 49.7 44.3	45.0 42.8 46.0 48.7 43.7	44.2 42.6 46.5 47.9 43.6	44-5 42.6 47.8 47-9 44-0	44.4 42.6 48.8 47.0 44.2	46.62 43.74 45.66 49.48 45.03	48.6 44.9 49.0 51.3 46.7	44.2 42.5 42.5 40.7 43.6
11 12 13 14 15	44.4 46.4 51.2 51.2 44.9	44.8 45.6 51.4 50.5 44.7 47.4	45.4 44.9 51.4 49.3 45.0	46.0 44.8 51.4 48.7 45.3	46.3 45.1 51.8 48.2 45.8	46.8 45.8 52.0 47.8 46.7	46.8 45.5 51.8 46.8 47.0	46.6 45.7 51.5 45.7 47.1	46.2 46.7 51.4 45.0 47.1	46.1 47.8 51.2 44.9 47.3	46.7 50.2 51.4 45.1 47.7	47.0 50.4 51.5 45.1 45.0	46.09 46.58 51.50 47.36 46.38	47.0 51.2 52.0 51.2 48.0	44.5 51.2 44.9 44.7 46.4
16 17 18 19 20	47.7 47.8 52.3 50.1 44.2	47.4 48.2 52.4 49.6 43.9	49.0 52.3 48.7 43.6	46.5 49.9 52.4 48.1 43.4	46.7 50.6 53.0 47.7 44.0	47.0 51.2 52.8 47.1 44.0	47.1 51.5 52.1 45.8 43.7 46.3	46.7 51.5 51.3 44.9 43.6	46.4 51.6 50.7 44.0 43.3	46.0 51.7 50.2 44.0 43.5	47.4 52.0 50.2 44.2 14.0	48.0 52.2 50.5 44.1 44.2	47.03 50.60 51.68 46.53 43.78	52.3 53.0 50.1 44.3	47.8 50.1 44.0 43.3
22 23 24 25	47.5 46.2 43.1 39.6	47.4 45.6 42.4 39.0	47.4 44.9 41.9 38.9	47.3 44.7 41.5 38.4	45.5 47.7 44.5 41.6 39.1	47.8 44.6 41.3 40.0	47.1 43.9 40.9 40.0	46.6 43.3 40.6 39.9	46,2 43.1 40.9 39.9	40.0 46.2 42.9 40.5 40.1	47.0 46.4 43.2 40.8 40.8	47.2 16.4 43.2 40.4 40.9	45.75 47.00 44.19 41.33 39.72	47.5 47.8 46.2 43.1 40.9	46.2 42.9 39.6 38.4 40.9
27 28 29 30	42.2 38.3 41.7 40.3	41.4 38.8 41.8 39.8	41.2 38.9 41.9 39.2	40.3 39.6 41.9 39.0	40.6 40.6 41.9 39.1	39.8 40.8 42.0 38.8	39.0 40.8 42.1 38.9	37.7 40.6 41.3 37.7	41.5 37.2 40.6 40.9 36.8	37.5 40.9 41.0 35.8	37.7 41.3 41.1 35.3	38.1 41.5 40.8 36.7	39.34 40.23 41.53 38.12	42.2 41.7 42.1 40.3	37.2 38.3 49.3 35.3
Mittel	45.07	44.91	44.77	44.82	45.16	45.41	45.17	44.7	44.42	44.36	44.71	44.78	44.86	46.76	42.97

							SEI	TEMB	- K						1905
Tag						I	ufttem	peratu	r nac	h Celsiu	15				
	1 2 h	14 <sup>h</sup>	16h	18p	20 <sup>h</sup>	22h	Ob.	2h	411	64	81	101	Tages- mittel	Max.	Min
1	14.3	14.1	13.9	13.7	14.5	14.1	15.7	15.8	14.	7 14	5 13.8	13.3	14.37	15.8	13.2
2	13.2		13.3	12.8	13.1	14.7	15.0	15.2	15.	5 14.	3 13.9	13.7	13.95	15.8	12.7
3 4	13.0	10.4	16.8	16.4	17.2	18.4	16.0	17.5	15.			15.3	16.54	18.4	13.3
5	13.5	13.6	13.7	14.0	15.3	10.5	19.5	20.5	20.	7 19.		15.1	16.49	20.7	13.5
6	14.4		13.9	13.9	15.5	19.1	22.0	23.0	23.			17.8	18.19	23.4	13.7
7 8	16.2	15.4	17.8	15.1	17.9	20.9	24.6	25.8	24. 25.	5 22		19.3	19.70	25.8	14.9
9	16.2	15.9	15.8	16.0	16.7	19.0	19.5	19.8	19.	9 18.	\$ 16.6	15.5	17.45	20.1	14.8
10	14. 8		14.3	14.2	16.3	20.3	21.2	21.7	22.	0 20.	5 19.0	20.0	18.21	22.3	14.0
11	20.7	20.6	17.3	17.4	19.2	23.5	24.9	25.5	24.			18.5	21.33	25.5	17.0
13	17.6		15.5	13.3	17.2	14.1	25.2 15.1	26.4 15.7	18.	3 18.		13.8	18.80	15.7	15.0
14	13.6	13.7	13.7	13.8	14.5	15.7	16.5	16.9	16,	9 15.		14.6	15.03	17.0	13.6
15	14.1		12.5	11.8	13.7	13.2	14-1	14.4	14.	3 13.	9 13.4	12.5	13.35	14.6	11.8
16	12.5	12.4	12.1	12.1	13.3	14.0	13.9	14.2	13.			12.8	13.07	14.4	11.8
17	9.1	7.9	6.9	5.8	6.1	11.7	13.0	14.0	13.	1 13.		10.1	11.86	15.2	5.0
19	8.4	7.3	6.4	6.2	8.3	12.6	16.9	15.1	18,	1 15.	0 13.9	11.8	11.99	18.3	6.2
20	10.2	9.2	8.5	8.4	9.8	11.9	13.9	16.0	17.	0 15.	6 14.6	13.9	12.42	17.2	8.3
21	13.4		12.6	8.11	12.4	13.6	15.7	16.2	16.		7 13.2	11.4	13.70	16.6	9.5
22	9.5	9.2	8.5	8.1	8.0	9.1	10.4	11.8	11.	7 11.		7.9	9.64	11.8	7.2
24	7.2	7.1	7.4	S. 4	9.7	11.5	14.4	16.3	16.	1 14.	8 13.5	12,6	11.58	16.3	7.0
25	12.4		11.9	11.7	12.1	13-5	15.4	16.4	17.		,	11.5	13.46	17.0	11.3
26 27	11.2	10.4	10.4	10.4	11.1	18.5	15.4	17.8	17.		4 13.6	12.5	13.16	17.8	10.3
28	14.4	13.2	9.3	9.4	11.0	14.7	15.4	17.9	17.	5 15.	3 14.9 S 13.6	12.5	13-33	18.0	9.3
29	12.6		0.11	11.0	11.9	13.7	15.4	17.0	17.	5 15.	0 13.4	12.9	13.60	17.7	11.0
30	12.5	11.9	11.7	11.4	12.8	13.6	13.2	14.1	14.	8 13.	1 12.0	8.4	12.63	15.8	7.9
M.M.	13.25	12.76	12.25	12.13	13.1	15.24	16.87	17.88	17.	50 16.	12 14.63	13.66	14.62	18.20	11.4
_					-12	-		-	_	_				MIL	1
Tag			Richti	ung (h	), Ges	chwind	igkeit	(G) des	Win	des in	Sekunde	in Meter	n		Tage
	12h R G	14h	16 <sup>1</sup>	a l	18h	20 <sup>h</sup> H G	R (	R	G G	R = G	R G	R G	R G	R G	mitt
,	W 3.5	www .	WNW		W 2.5			1	- 1	VNW S.	1	WNW L	-	W ?	1
2	W 3.6	W 4.	, W	2 8 WS	W 2 4	W a				W 4.3	WSW 3.9	WSW 4.	WSW 1.8		7 4.0
3	17 5.2	W 5.	WNW	3.8 WN	W 5.0	WSW 3.	o W 3	.s W		VNW 6.1	W 3.5	W 5.	W 5.3	W 6.	4 4.8
5	WNW 2.1	W 2.	S W	5.5 3.1 WN	1 3.5	W 2.	WSW 2	S WAT	3.3	NW 5.5	NNW 0.2	ESE L	WNW 3.0		8 5.0
6	S 0.6		SSE	0.4 5	SE 0.2	SSE 1.	SW 2			S 1.5	SE 2.3	SE 2.	SE o.		il
7 8	*** 0.0	0.	SSE	0.3	S 0.3	SSW 1.	SSW I	S WSW	3.2	WSW 3.4	WSW 2.4	SW *)-	SW -	S -	
8	WNW 2.2	SW 1.	NNE	- S	SE -	SSW -		WNW		SSW 1.0	WSW 1.5	NNW 4.	WSW o.	NNW 2.	5 0.9
10	SW o.	S 0.	SSW	1.9 58	W 2.4	S 1.	WSW 4	WSW	4.1	WSW 2.1	WSW 4.4	W 1.	WSW o.	WSW 2	5 2.1
11	W 4.7				W 0.5	SSW 1.	WSW &	. 5 11		WSW 1.0	WNW 1.9		0.0	0	0 2.1
12	*** 0.0	NW o.	S N	1.6 NN	W 0.4	0.0	NW I	. 2 1	0.5	N 1.2	N 1.4	N 2.1	NNE 2.5	NNE 2.	9 1.3
13	NNE 2.8 N 1.1	NNW 1.	N N	2.1 1.0 N	N 2.5	ENE 1.	N I	8 NE	2.0	NNE 0.9 ENE 2.9	NNII 1.9	NNW 5	NNW 1.	NNW 1.	9 1.8
15	NNW 2.3	NNW 2.	S N	3.5	N 3.3	N 4.	N 4	2 NNE	3.2	NNE 4.1		NNE 1.	Y 1.	N z	1 2.9
16	WNW o.f	NNW o.	NNW	0.9 NX	W 0.7	NNE 1.	ESE I	4 1	1.0	N 1.6	N 1.0	NNW o.	WNW 1.5	WNW 2.	2 1.2
17	WYW 2.1	NW 2	WNW	4. 2 W.N	W 3.7	NW 1.	B NNW 2	A NAW	2 . N V	VAW 2 6	NYW 2.1	AW L.	NNW O.8	NW 1.	0 2.7
18	ENE 1.9	WSW o. NE 1.	NE NE	0.6 5	W 0.8	SW o.	ESE 1	8 SE	6.5	ESE 4.0	ESE 5.0	ESE 2.	SE 2.5 ESE 2.5	SE 1. ESE 1.	2 2.9
20	NE 0.6	NE 1.	NE.	0.4 B	E 0.5	ENE 1.	N I	5 NNE	1.2	NE 1.4	ENE 1.0	NNE o.	N 2.9	No	8 1.1
21	N o.6	NNE 1.	E	1.0 !	Œ 1.4	NE 1.	6 E 1	9 ENE		ENE 4.0	NE 2.2		E 2.	ENE 1.	7 2.0
22	E 1.0	NE 1.	N N	1 0	N 0.4	NW 0.	NNW 1	.5	2.2	NE 2.5	N 0.0	ESE 1.0	2 377 1 1 1		3 1.4
23	NNE o.	No. Eo.	NNW	0.2	E 0.6	SE 2.		. 1 SE	2.3	ESE 2.1	ESE 3.1	ESE 2.	ESE 2.9	NNE o.	3 1.7
25	ESE o,	ENE o.	WSW	0.2 XX	W 0.3	SE 2.		.5 SH	1.1	W o.	SSW 0.7	SSW o.	0.0	0.	0.4
26	0.0	NW o.	WSW	0.6 WS	W 0.3	SSE o.	NNW o	4 3	2.1	NNW 1.2	NNE 1.4	NNW o.	0.0	NNW o.	4 0.8
27	WSW o.	SW o.	- SW	A 1	N 0 2	NE o.	NE o	.6 ENE	1.5	ENE 1.0	E 1.9	E o.	0.0		3 0.7
28	WNW 2.1	NNE o.	2 3	2.2 WS	W 2.5 VE 0.7	W I.	NNW 1	4 NAW	0.0	W 1.4	1.11 0.4	N.311 0.:	WSW O.	SSW o.	2 0.6
					101	SSW 2.	divers .	Well	. 2 .	wew .	WSW 4.2	SW 3.3	W 4.0	W 4.	1 2.8
30	55W 0.2	S 0.	3	1.6 S	SE 1.0	55W 2.	1 11311 3	.4 11.511	3.0	11.711 4.0	11.511 4.2	3.0	414	41	
			1				1								
30	55W 0.3		1	.63	1.56	1.8	1		2.57	2.5					4

						OKTOBER					1905
					a) Dir	ekte Ables	ungen				
1	Luft	druck a	uí o' redu	ssiert in M	illim. =	= 700** +		Lui	ttemperatu	r nach Celsiu	9
Tag	19h		2h	96		Tagesmittel	11	94	21.	94	Tagesmitte
	38.2		38.3	17 f		18.00	. 7	°,	13.0	9.2	9.93
2	37.2	1	35.6	37 - 5 34 - 8		35.87	9	. 2	12.8	9-4	10.47
3	34.0		35.1	35,5		35-97	1 7	.7	10.8	7.4	8.63
4	41.3		39.5	35.1	. 1	36.63		.6	13.7	9.8	9.27
5	31.4				- 2	31-33		. 8		8.5	10.67
6	34-3	- 1	35.0	38.3		35.87	8	.0	10.6	7.5	9.00
7 8	40.1		43.0	44.4		42.50		.0	7-3	6.4	6.57
	46.6		47.4	49.2		47-73	0	.4	7.8	6.5	6.90
9	43.8		46.6	48.3		46.23		. 2	7.5	7.0	6.57
	46.7		46.1	1					6.6		
11	48.1	1	46.1	47.5		46.77	3	.6	7.5	5.9	6.70
13	43.5		39.5	35.9		39.63	1 6	.7	8.1	5.8	6.87
14	39.1	- 1	40.0	41.4		40.17	3	.6	6.6	4.3	4.83
15	35.7	1	32.8	38.7		33.40	4	-7	7.1	7.6	6.47
16	34.7		37 - 7	40.6	: [	37.67	3	.5	6.8	3.5	4.60
17	43.6	- (	43.8	44.8		44.07	3	- 3	7.8	4.5	5.20
18	45.3	1	45.5	47.5	5 8	46.10		.9	6.4	4.2	4.90
19	48.4	- 1	48.0	47-4		47-93		-9		2.8	3.70
20	46.1	1	46.3	47.2		46.53		-4	4.0	2.4	2.60
21	46.5	1	45.6	45.6		45.90		.6	5.3	3.8	3-57
22	45.2	- 1	44.5	45.2		44.97		.0	7.0	4.3	4.43
23	45-9	- 1	45-5	47.9		47.63		.6	4.2	2.4	3,60
25	47.6		46.6	47.7		47.30	- i	.6	3.3	2.0	1.23
26	50.0	1	50.7	53.1		51.27		.7	3.8	1.8	2.10
27	53.0		51.0	49.5		51.17		.7	5.9	4.0	3.27
28	46.9	- 1	46.2	47.3		46.77		.4	7.1	5.8	6.43
29	45.5	!	43.6	42.4		43.83	3	.9	7.9	5.6	5.80
30	41.3		40.2	39.4	. 1	40.30	5	.0	10.6	7-1	7-57
31	39.3		38.5	38.8	١,	38.87	5	. 2	8.7	5.8	6.57
Mittel	43,12	2	42.80	43.0	3	42.98	1	-44	7.79	5-49	5.91
Tag	Dun	stdruck	in Millim	etern	F	ciative Fe	uchtig	kelt	Richtung	u. Stärke o [Skala: o — 10	les Windes
	10,	24	94	Tages- mittel	191	2 <sup>h</sup>	98	Tages- mittel	19 <sup>h</sup>	34	94
	5.8	5.4	6,3	5.8	74	48	72	65	SW 3	W 2	SW 3
2	6.5	5.4	6.5	6.1	75	49	74	65	SW 2	W	SW I
3	6.5	5.1	5.9	5.8	75 83	53	77 68	71	WNW 2	W 1	SSW 3
4	5.7	5.0	6.4	5.6	78	49		65	SSW 1	WSW 3	
5		5-7			73	49	77				
6	5.8	5.3	5 - 3	5.5	68	56	69	64	SW 3 W 1	WSW 6	
7 8	4.9 5.6	5.6	5.3	5.3	7º 78	73 76	73	72 77	W 3	W 3	WNW 3 W 2
9	5.8	5.4	5.6	5.6	81	67	83	77	WNW 2	WNW 3	W 3
10	0.2	6.0	5.9	6.0	94	77	78	83	NNW 2	Ni	N I
11	5.4	5.6	6.2	5.7	80	77	90	82	N 3	N a	N 2
12	0.4	6.4	6.4	5.7 6.4	94	83	85	87	NW 1	NW 3	SW 2
13	6,1	6.2		6,3	83	77	06	85	SW 3	W 4	W 3
14	4.3	4.1	4.3	4.2	73	57	70	67	SW 3	W 3	SSW 4
15	3.9	5.5	5.7	5.0	60	73	73	69			
16	5-4	5.1	4.9	5.1	92	70	83	82	NW I	W	SW 2
17	4.7	5.1	4.8	4.9	82	64	76	74	SW I	WsW I	SSE 1
18		4.0 5.2	4.4 5.0	4.4	86 86	72	71 89	69 82	SE 1	SW 3	NW 1
20	4.5	4.2	4.1	4.3	91	69	75	78	NNW I	NE 3	N I
21	4.2	4.2	5.1		82	63	85		*** 0	SW 2	SSW 2
22	4.7	3-7	4.5	4.5	8q	40	73	77	0	W	SW 1
23	4.5	4.4	4.7	4.5	84	62	85	77	SSW #	SW 1	S
24	4.6	3.9	4.5	4.3	82	63	80	75 81	WSW 1	NW 1	0
25	4.0	3.3	4.7	4.0	98	56	89	81	SSW 1	NE 1	N s
26	3.8	3.0	4.0	3.6	78	49	77	68	W 1	NNW t	N I
27	3.8	3-4	3.7	3.6	83	49	61	64	WSW 2	SW 4	W 3
28	4.9	5.2	5.2	5.1	81	69	76	76	SW 3	WSW 5	WSW 4
29	5.1	6.5	6.4	6.1	84 81	63	73 86	73	WSW I	SSW 1	SW 2 SSE 1
31	5.5	6.4	6.4	6.0	8;	76	90	79 83	SSE 1	SW I	35E 1
				1		1 1					1
Mittel	5.2	5.0	5.3	5,2	82	63	78	74	1.7	2.2	2.

Tag		Bewôl	kung [	Skala: o I Woll	- heite	er, 10 =	trāb]		Nieder- schlag in		F	eme	rkuns	z e n	
	19	,.	2			9h	Tages	mittel	Milli- metern						
1				9 W		10	6	-7							
3	HS I		118 1		FRS	6 W	10	.7	0.7	Morge	as und .	abends	olh O,,	th to Tr	84
4	FHS	0 W	FRS P	0 W	FHS	to W	9	.7	0.2	75 und	S1 30				
5	HS I			9 SW	FHS	3 SW	7	-3	***	Morge	15 = <sub>6</sub> , 1		u. 51 🖜 .	, 21 🔘 Tı	ropfe
6		S W	HS I		FHS	7 XW	9	.3	1.4	2h 🔘 4	und sti	-5} .			
7 8	HS I	0 '41		o #.		7 NW		.7	1.5					opf., nach	its @
9	HS I		HS I			10 W	10			3" 00	311-8	. O. n	achts .		
10	1		140				10		2.6						
11	IIS I		HS I			10 W	10	.0	2.2	Monre	t m	ends =	, 5h, 7h u.1	Troof, n	@ Ir
13	fis	s W	HS I	o W	5	10	9	. 3	2.0	Morge	ns 🖦 , 2	3 Trop	of., 45-95	@ O	nacht
14		9 W	FHS HS 1	g W		10 W	10	-3	2.0	20" (9)	. 23" 🛋	u. 😝 1	ropf., oh	* LIOCKO	n.
15	HS I			o W	11	1			0.4			abends		[n	achts
17	HS t	o XW	HS 1	o W	FR	2	7	-3 [	***	Morge	ns 📟 ,	aben	ds a.		
18		8 W	HS I		Fils	5	9	.3		Morge	ns 📻 :	_ aben	ds m		
20	N I			0		19	10			Morge	ns man.	a mitta	gs = , 2 <sup>3</sup>	U. 5h @	Trot
21	8 1	o		8 8		10	1 9	.3	***	Morge	ns und	abends	-,		
22	HS I			7 W		10	9	.0	***	Morge	ns == , .	a, aben	ds =.		
23	08		FHS	o SW	S	10		-7	***	Morge	ns und	abends	ds =, ←	211" (D.	
25	S			6	S	10	1 8	.7	**1	Morge	ns =,	mitta	igs ==,, al	pends =0	
26		8		0		10 W		- 3		Morge	ns und	abends	=.		
27		9 W		7	FIIS			.0	0.3	Morge	ns me,	Troofe	opfen, nac	chts @.	
29	FifS	8 NW	HS I	o SW	FIIS	6 SW	8	.0	***	Morge	ns 🖃	13.			
30		o	FHS 1	o sw	FS FS	9	10	.0	***	Morge	ns 👄 ,	mittags l	Dunst am dunstig, a	Horiz., ab	ends
Mittel	1	8.9		9.5		8.6	1		S. 19.7	1	41				
									eichnu						
Tag	125	143-	169	186	Luft 20h	druck	auf o*	eduzie 2h	t in Mill	imetern	700°°	100	Tages-	Max.	M
-			nn l			-	-			1010	Mile	-	mittel	-	
	37.4	37.6	37.9	38.0	38.3	38.7	38.6	38.3	37.8	37-5	37.6	37.3	37.92	38.7	37
3	37.2	37.0	37.1	37.0	37.4	37 - 3	36.5	35.6	35.1	34.8	34.8	34.7	36,21	37.4	34
4	40.0	40.3	49.5	41.0	41.6	41.7	41.3	39.5	35.0	37.2	35.7	34.2	39.25	41.7	32 30
5	32.5	31.2	31.2	31.2	31.7	32.2	32.1	31.6	30.4	30.7	31.0	31.6	31.45	32.5	
6	32.1	33.3	32.7	33.6	34.5	34.8	34.7	35.0 43.0	35-5	36.7	37.8	38.4	34.84	38.4 44.8	32
5	44.8	45.3	45.6	46,1	46.9	47.5	47-5	47.4	47.5	48.3	49.0	49.3	47-10	49.5	44
9	49.5	49.9	41.8	50.4 42.8	50.3	49.6	48.6	40.7	45.1	43.5	42.5	48.2	47.35	50.4 48.4	41
10	45.2	47.7	47-1	46.9	46.5	46.4	46.3	40.0	46.5	47.0	47.3	47.6	46.98	48.4	46
12	47.7	47.6	47-4	47-7	45.2	48.6	48.6	48.1	47.6	47.6	47.3	46,7	47.76	45.6	46
13	46.1	45.6 37.8	38.4	43.9	43.5	42.1	40.8	39.5	37.5	36.3	35-3	36.5	40.98	46.1	35
11				35.8	39.7	33.8	40.3 33.3	32.8	32.5	32.5	32.1	31.9	39.78	41.5	37
1.4	40.5	39.3	35.0	36.6			33.3								
14 15 16		39.3	35.0	36.6	35.6	36.5	37.6	37.7	38.0	39.0	49.0	41.0	36.25		-
14 15 16	40.5 31.7 41.3	39.3 31.8 41.6	35.0 32.0 42.0	34.1 43.0	35.6	36.5	37.6 44.1	37.7 43.8	43.8	44.5	49.0 44.8	41.0	36.25 43.54	41.3	31 41
14 15 16	40.5 31.7 41.3 45.3	39.3 31.8 41.6 45.4 45.4	35.0 32.0 42.0 45.3 45.1	34.1 43.0	35.6 44.1 45.5	36.5 44.3 45.9 48.8	37.6 44.1 45.8 48.9	37.7 43.8 45.5 48.0	43.8 45.8 47.5		49.0 44.8 47.2	41.0	36.25 43.54 45.94 48.15	41.3	31 41
14 15 16 17 18	40.5 31.7 41.3	39.3 31.8 41.6 45.4	35.0 32.0 42.0 45.3	34.1	35.6	36.5 44.3 45.9 48.8 46.3	37.6 44.1 45.8 48.9 46.5	37.7 43.8 45.5	43.8	44.5	49.0 44.8	41.0 45.2 47.8	36.25 43.54 45.94	41.3 45.3 48.1	31 41 45 46
14 15 16 17 18 19 20 21	40.5 31.7 41.3 45.3 48.1 46.8 47.0	39.3 31.8 41.6 45.4 45.4 46.2 46.8	35.0 42.0 45.3 45.1 40.2	34.1 43.0 45.3 48.3 46.2	35.6 44.1 45.5 48.9 46.2	36.5 44.3 45.9 48.8 46.3 46.6	37.6 44.1 45.8 48.9 46.5	37.7 43.8 45.5 45.0 46.3	43.8 45.8 47.5 46.6 45.3	44.5 40.5 47.7 47.1 43.5	49.0 44.8 47.2 47.5 47.3 45.6	41.0 45.2 47.8 47.3 47.1 45.9	36.25 43.54 45.94 48.15 46.57	41.3 45.3 48.1 48.9 47.3	31 41 45 46 46
14 15 16 17 18 19 20 21	40.5 31.7 41.3 45.3 48.1 46.8 47.0 45.5	39.3 31.8 41.6 45.4 48.4 46.2 46.8 45.4	35.0 42.0 45.3 45.1 40.2 40.6 45.3	34.1 43.0 45.3 48.3 46.2 40.5 45.2	35.6 44.1 45.5 48.9 46.2 46.4 45.3	36.5 44.3 45.9 48.8 46.3 46.6 45.2 40.3	37.6 44.1 45.8 48.9 46.5	37.7 43.8 45.5 45.0 46.3 45.6 44.6	43.8 45.8 47.5 46.6 45.3 44.5	44.5 40.5 47.7 47.1 43.5 44.7	49.0 44.8 47.2 47.5 47.3 45.6 45.1	41.0 45.2 47.8 47.3 47.1 45.9 45.3	36.25 43.54 45.94 48.15 46.57 46.18 45.08	41.3 45.3 48.1 48.9 47-3 47.0 45.5	31 41 45 46 46 45 44
14 15 16 17 18 19 20 21 22 23 24	40.5 31.7 41.3 45.3 48.1 46.8 47.0 45.5 45.4	39.3 31.8 41.6 45.4 46.2 46.8 45.4 45.6 47.3	35.0 42.0 45.3 45.1 40.2 46.6 45.3 45.4 47.2	34.1 43.0 45.3 48.3 46.2 40.5 45.7 47.1	35.6 44.1 45.5 48.9 46.2 46.4 45.3 46.1 47.6	36.5 44.3 45.9 48.8 46.3 46.6 45.2 40.3 48.1	37.6 44.1 45.8 48.9 46.3 45.0 46.2 48.2	37.7 43.8 45.5 48.0 40.3 45.6 44.5 45.3 47.8	43.8 45.8 47.5 46.6 45.3 44.5 45.7 47.3	44.5 40.5 47.7 47.1 43.5 44.7 40.0 47.0	49.0 44.8 47.2 47.5 47.3 45.6 45.1 46.6 47.9	41.0 45.2 47.8 47.3 47.1 45.9 45.3 46.8 47.9	36.25 43.54 45.94 48.15 46.57 46.18 45.08 45.08 45.94 47.59	41.3 45.3 48.1 48.9 47.3 47.0 45.5 47.1 48.2	31 41 45 46 46 46 45 47
14 15 16 17 18 19 20 21 22 23 24 25	40.5 31.7 41.3 45.3 48.1 46.8 47.0 45.5 45.4 47.8	39.3 31.8 41.6 45.4 48.4 46.2 46.8 45.4 45.6 47.3 48.1	35.0 42.0 45.3 45.1 40.2 46.6 45.3 45.4 47.2 47.6	34.1 43.0 45.3 48.3 46.2 40.5 45.7 47.1 47.6	35.6 44.1 45.5 48.9 46.2 46.4 45.3 46.1 47.6 47.8	36.5 44.3 45.9 48.8 46.3 46.6 45.2 40.3 48.1 45.0	37.6 44.1 45.8 48.9 46.5 46.3 45.0 46.2 48.2 47.5	37.7 43.8 45.5 45.0 40.3 45.6 44.5 45.3 47.8 40.6	43.% 45.8 47.5 46.6 45.3 44.5 45.7 47.3 46.6	44.5 40.5 47.7 47.1 43.5 44.7 46.0 47.6 46.9	49.0 44.8 47.2 47.5 47.3 45.6 45.1 40.6 47.9 47.4	41.0 45.2 47.8 47.3 47.1 45.9 45.3 46.8 47.9 47.7	36.25 43.54 45.94 48.15 46.57 46.18 45.08 45.08 47.59 47.47	41.3 45.3 48.1 48.9 47.3 47.0 45.5 47.1 48.2 48.1	31 41 45 46 46 45 44 45 47 46
14 15 16 17 18 19 20 21 22 23 24 25	40.5 31.7 41.3 45.3 48.1 40.8 47.0 45.5 45.4 47.8 47.8 48.8	39.3 31.8 41.6 45.4 48.4 46.2 46.8 45.4 45.6 47.3 48.1	35.0 42.0 45.3 45.1 40.2 40.6 45.3 45.4 47.2 47.6 48.5	34.1 43.0 45.3 48.3 46.2 40.5 45.7 47.1 47.6	35.6 44.1 45.5 48.9 46.2 46.4 45.3 46.1 47.6 47.8	36.5 44.3 45.9 46.8 46.3 46.6 45.2 40.3 48.1 45.0 50.7	37.6 44.1 45.8 48.9 46.5 46.3 45.0 46.2 48.2 47.5	37.7 43.8 45.5 48.0 40.3 45.6 44.5 45.3 47.8 40.6 50.7	43.% 45.8 47.5 46.0 45.3 44.5 45.7 47.3 46.6 51.3	44.5 40.5 47.7 47.1 43.5 44.7 46.0 47.6 46.9 52.1	49.0 44.8 47.2 47.5 47.3 45.6 45.1 46.6 47.9 47.4	41.0 45.2 47.8 47.3 47.1 45.9 45.3 46.8 47.9 47.7	36.25 43.54 45.94 48.15 46.57 46.18 45.08 45.94 47.59 47.47 50.50	41.3 45.3 48.1 48.9 47.3 47.0 45.5 47.1 48.2 48.1	31 41 45 46 46 45 44 45 47 46 48
14 15 16 17 18 19 20 21 22 23 24 25 26 27 28	40.5 31.7 41.3 45.3 48.1 46.8 47.0 45.5 45.4 47.8 47.8 47.8 47.8	39.3 31.8 41.6 45.4 46.2 46.8 45.4 45.6 47.3 48.1 48.5 53.1 48.5	35.0 42.0 45.3 45.1 40.2 40.6 45.3 45.4 47.6 48.5 53.0 47.4	34.1 43.0 45.3 48.3 46.2 40.5 45.7 47.1 47.6	35.6 44.1 45.5 48.9 46.2 46.4 45.3 46.1 47.6 47.8 50.5 53.1	36.5 44.3 45.9 48.8 46.3 46.6 45.2 40.3 48.1 48.0 50.7 52.8 47.0	37.6 44.1 45.8 48.9 46.5 46.3 45.0 46.2 48.2 47.5 51.1 52.3 40.7	37.7 43.8 45.5 45.5 46.3 45.6 44.5 47.8 40.6 50.7 51.0 46.2	43.% 45.8 47.5 46.6 45.3 44.5 45.7 47.3 46.6	44.5 40.5 47.7 47.1 43.5 44.7 40.0 47.6 46.9 52.1 50.4 46.8	49.0 44.8 47.2 47.5 47.3 45.6 45.1 40.6 47.4 53.1 49.2 47.1	41.0 45.2 47.8 47.3 47.1 45.9 45.3 46.8 47.9 47.7 53.1 49.3	36.25 43.54 45.94 48.15 46.57 46.18 45.08 45.08 47.59 47.47	41.3 45.3 48.1 48.9 47.3 47.0 45.5 47.1 48.2 48.1	31 41 45 46 46 45 47 46 48 49
14 15 16 17 18 19 20 21 22 23 24 25 26 27 28	40.5 31.7 41.3 45.1 46.8 47.0 45.5 45.4 47.8 47.8 47.8 47.8	39-3 31,8 41.6 45-4 45.4 46.2 46.8 45.6 47-3 48.1 48.5 53.1 48.5	35.0 32.0 42.0 45.3 45.1 40.6 45.3 45.4 47.2 47.6 48.5 53.0 47.4 46.2	34.1 43.0 45.3 46.2 46.5 45.2 45.7 47.1 47.6 49.4 53.0 47.0 45.0	35.6 44.8 45.5 48.9 46.2 46.4 45.3 46.8 47.6 50.5 53.1 47.0 47.0	36.5 44.3 45.9 48.8 46.3 46.6 45.2 40.3 48.1 45.0 50.7 52.8 47.0	37.6 44.1 45.8 48.9 46.5 46.3 45.0 46.2 47.5 51.1 52.3 46.7 44.6	37.7 43.8 45.5 48.0 40.3 45.6 44.5 45.3 47.8 40.6 50.7 51.0 46.2 43.6	43.8 45.8 47.5 46.6 45.3 44.5 45.7 47.3 46.6 51.3 50.9 46.4 43.3	44.5 40.5 47.7 47.1 43.5 44.7 40.0 47.0 46.0 52.1 50.4 46.8 42.6	49.0 44.8 47.2 47.5 47.3 45.6 45.1 46.6 47.9 47.4 49.7 47.1 49.6	41.0 45.2 47.8 47.3 47.1 45.9 45.3 46.8 47.9 47.7 53.1 49.3 47.2 42.3	36.25 43.54 45.94 48.15 46.57 46.18 45.08 45.08 47.59 47.47 50.50 51.81 47.17 44.63	41.3 45.3 48.1 48.9 47.3 47.0 45.5 47.1 48.2 48.1 53.1 53.1	31 41 45 46 46 45 47 46 48 49 46 42
14 15 16 17 18 19 20 21 22 23 24 25 26 27 28	40.5 31.7 41.3 45.3 48.1 46.8 47.0 45.5 45.4 47.8 47.8 47.8 47.8	39-3 31.8 41.6 45.4 45.4 46.2 46.8 45.4 45.4 45.4 45.3 45.4 45.3 46.6 47.3 48.1 48.5 48.1 48.2 46.6	35.0 32.0 42.0 45.3 46.2 46.6 45.3 45.4 47.6 48.5 53.0 47.4 46.2 41.6	34.1 43.0 45.3 46.2 46.5 45.7 47.1 47.6 49.4 53.0 47.0 45.0 41.4	35.6 44.1 45.5 48.9 46.2 46.4 45.3 46.1 47.6 47.8 50.5 53.1	36.5 44.3 45.9 48.8 46.3 46.6 45.2 40.3 48.1 48.0 50.7 52.8 47.0	37.6 44.1 45.8 48.9 46.5 46.3 45.0 46.2 48.2 47.5 51.1 52.3 40.7	37.7 43.8 45.5 48.0 40.3 45.6 44.5 45.3 47.8 40.6 50.7 51.0 46.2 43.6	43.8 45.8 47.5 46.6 45.3 44.5 45.7 47.3 46.6 51.3 50.9 46.4 43.3 40.1	44.5 40.5 47.7 47.1 43.5 44.7 40.0 47.6 46.9 52.1 50.4 46.8	49.0 44.8 47.2 47.5 47.3 45.6 45.1 46.6 47.9 47.4 53.1 49.2 47.4 53.1 49.2 47.6 39.2	41.0 45.2 47.8 47.3 47.1 45.9 45.3 46.8 47.9 47.7 53.1 49.3	36.25 43.54 45.94 48.15 46.57 46.18 45.08 45.94 47.59 47.47 50.59 51.81 47.17 44.63 40.84	41.3 45.3 48.1 48.9 47.3 47.0 45.5 47.1 48.2 48.1 53.1 53.1 49.0 47.0	31 41 45 46 46 45 47 46 48 49 46 42 39
14 15 16 17 18 19 20 21 22 23 24 25 26 27 28	40.5 31.7 41.3 45.3 48.1 40.8 47.0 45.5 45.4 47.8 48.1 53.1 49.0 47.0	39-3 31,8 41.6 45-4 45.4 46.2 46.8 45.6 47-3 48.1 48.5 53.1 48.5	35.0 32.0 42.0 45.3 45.1 40.6 45.3 45.4 47.2 47.6 48.5 53.0 47.4 46.2	34.1 43.0 45.3 46.2 46.5 45.2 45.7 47.1 47.6 49.4 53.0 47.0 45.0	35.6 44.1 45.5 48.9 46.2 46.4 45.3 46.1 47.6 47.8 50.5 53.1 47.0 45.4	36.5 44.3 45.9 48.8 46.3 46.6 45.2 48.1 48.0 50.7 52.8 47.0 45.4	37.6 44.1 45.8 48.9 46.5 46.3 45.0 46.2 47.5 51.1 52.3 40.7 44.6	37.7 43.8 45.5 48.0 40.3 45.6 44.5 45.3 47.8 40.6 50.7 51.0 46.2 43.6	43.8 45.8 47.8 46.6 45.3 44.5 45.7 47.3 46.6 51.3 50.9 46.4 43.3 40.1 38.3	44.5 40.5 47.7 47.1 43.5 44.7 40.0 47.0 46.9 52.1 50.4 46.8 42.6 39.7	49.0 44.8 47.2 47.5 47.3 45.6 45.1 46.6 47.9 47.4 49.7 47.1 49.6	41.0 45.2 47.8 47.3 47.1 45.9 45.9 46.8 47.9 47.7 53.1 49.3 47.2 42.3 39.4	36.25 43.54 45.94 48.15 46.57 46.18 45.08 45.08 47.59 47.47 50.50 51.81 47.17 44.63	41.3 45.3 48.1 48.9 47.3 47.0 45.5 47.1 48.2 48.1 53.1 53.1	31 41 45 46 46 45 47 46 48 49 46

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. a.g	12h	14 <sup>h</sup>	164	185	20 <sup>h</sup>	225	OF	24	43	6h	86	10h	Tages- mittel	Max.	Min.
1	7.9	7.5	6.8	6.7	8.6	10.7	11.1	13.0	11.9	10.7	9.5	9.2	9.47	13.0	6.6
3	8.5	7.9	9.1 8.2	7.9	8.0	9.6	8.3	12.8	10.4	8.5	7.8	7.1	8.58	12.8	8.5
4	6.9	5.9	6.5	6.3	7.5	9.4	10.7	11.4	11.2	9.9	9.7	9.9	8.79	11.7	5.8
5	10.7	11.5	10.4		9.8	11.0	12.3	13.7	13.1	9.4	8.5	8.4	10.72	13.7	8.2
6	8.9	9.0	8,9	8.5	9.2	10.6	11.0	10.6	9.8	8.7	7.8	7.2	9.18	11.3	6.4
7 8	6.4	5.4	5.5	5.8	6.5	7.0	8.0	7.3	7.4	7.0	6.6	6.5	6.58	8.2	5.0
9	5.7	6.5	6.5 5.8	6.3	6.6	8.4	8.2	8.0	7.0	6.1	5.3	5.4	6,73	8.4	5-3
10	5.5	5.6		5-3	4.9	5.6	6.1	7-5	7-9	7.5	7.2	6.9	6.32	8.1	4.9
11	6,6	5.7	5.7	5.6	5.6 5.8	5.9	5.9	6.6	7.6	6.4 7.5	6.0 7.1	5.8	6.10	7.9	5.4
13	6.4	6.4	6.3	6.5	7.3	8.2	8.8	7-5	8.1	7.7	7.4	5.1	7.19	8.8	4.7
14	4.9	4.5	4.0	3-4	4.1	5.1	6.2	7.1	7.6	4.6 7-7	4.3	7.8	4.85 5.90	8.0	2.7
16	8.0	8.1	7-7	3.9	3.9	4.8	6.0	6.8	6.4		7.5	1.0	5.76	8.1	
17	3.1	2.8	2.5	2.9	3.8	5.2	7.1	7.8	7.3	5.4	4.4	3.5	4-62	8.1	2.5
18	3.1	2.5	2.6	2.6	3.3	5.4	6.3	7.6	6,1	5.8	5.0	4-1	4.56	7.6	2.6
19	3.6	3.2	3.0	1.4	1.6	3.9	4.8	6.4	3.8	3.4	3.0	2.3	3.69	4.0	1.9
21	2.0	1.6	1.2	1.3	2.0	3.1	4.6	5.3	5.3	4.3	3.8	3.6	3.19	5.4	1.2
22	3.3	2.8	2.6	2.I	2.2	3.9	6.0	7.0	0.0	4.9	4.6	4.1	4.13	7.0	2.0
23 24	3.7	2.8	2.4	2.5	2.5	3.3	4.8 3.1	6.2	3.8	3.9	2.5	2.3	3.42	6.2	1.8
25	1.4	0.5	0,1	- 1.5	- 1.4	- 0.7	1.3	3.3	3.3	2.7	2.2	1.8	1.08	3.4	- 1.6
26	1.3	1.0	0.5	0.5	0.8	1.8	3.1	3.8	3.4	2.7	1.8	1.9	1.88	3.8	0.3
27	1.6	1.1	0.5	0.1	0.8	2.8	4.6	5.9	5.8	5.0	4.5 5.8	4.2	3.08	6.3	- 0.4
28	3.9	5.7	5.4	3.6	4.0	5.1	6.4	7.1	7.0	5.9	5.8	5.4	5.07	7-3	3.1
30	4.5	4.7	4.8	4.7	5.3	7.6	7·5 9.8	10.6	10.3	8.6	7.5	7.0	7.12	10.9	4.5
31	0.0	6.0	5.4	5.1	5.2	6.2	7.4	8.7	S.4	7-7	6.6	5.1	6.53	8.7	4.0
LM.	5.17	4.90	4.71	4.36	4.76	5.95	6.95	7.79	7.40	6.39	5-7	4 5.30	5.79	8.07	3.7
ag	124	144		tung (	R), Ge	schwine 20 <sup>b</sup>	digkeit	(G) des		s in 1 3	Sekunde	in Met	ern Xa	106	Tage
_	R G	R	G R		g G	R=G	R G		G R		R = G	R C	R G		G
1	WSW 3.	3 W	1.0		W 5.2	W 4.9	WNW 6.	OWNW	4.6 WNV	0.5	W 4.1	WSW 3	2 SW 2.	9 SW 4.	4 4.5
3	WSW 3.	WEN	WYN	2 8 W N		WSW 2.5 W 3.2	W 3.	4 WNW	5.2 V 4.5 WAV	V 4.3 W	SW 2.6	WXW 2	8 WSW 2. 5 WNW 3.	8 WSW 3.	2 3.
4	WNW 3.1	2 W .	1. 3	1.9	W 2.7	W 3.5	W 3.	8 W	1. 5 WSV	4.5	SW 5.2	SSW 3	ol SSW 4.	o SSW 3.	5) 3.8
5	SSW 4.:		1.9 W	0.7		WSW 3.1	WSW 5.		6.1 WSW		₩ 5.9				
6 7	WNW 5	WSW 4	. S WSW	3.5 WS	W 6 5	W 5.3	W 6.	6 WAW	S. I WNV	7.6 W	NW 7.1	WANT 5	1 W 3.		
8	n 5.	1179.79 4	. 4 17.7 11	3.2 77 (7	3.5	man 4.4	11.111 2.	2,11,111	3.0 11.11	3.7	W 4.0	311 2	3 11.111 1.	7 WNW 2.	5 3-1
9	WNW 2.			2.5 WN	W 2. II		WSW 3.	o W				WSW 4	2 WSW 5.	1 W 3.	9 3.5
	11 .	SW	6 VYI	2 .	N . K	N a 6	NXV .	- XE	4.4 V	4.6 W	N 2 5		O X 2	N 2	9 3.3
- 1	W 2.	SWo	.6 NYW	6.8	N 1.8	N 2.6	NNE 1.	7 NE	3.1 NNI	5 2.6	N 2.5	NNE 3	O N 2.	N 2.	5 2.2
1	N 3.2	SW o	.6 NNW	6.8 0.4 NN	N 6.2 W 0.5	N 2.6	NNE 1.	7 NE 2 NNE 2 NNE	S. I NNE	6 2.6 6 4.1 N	N 2.5	NNE 1.	5 N 2.	N I.	5 2.2 6 4.1
12	N 3.4 N 1.6 SW 2.3	SW o	. NNW	2.1 6.8 0.4 NN 3.5 WS	N 6,2 W 0.5 W 3.6	N 2.6	NNE 1.	7 NE 2 NNE 2 NNE	S. I NNE	6 2.6 6 4.1 N	N 2.5	NNE 1.	5 N 2.	0 N 1. 2 WSW 1. 5 WNW 2.	5 2.5 6 4.5 9 1.6
11 12 13 14	N 2.1 N 3.2 N 1.0 SW 2.2 W 4.0	WSW 2	. NNW	2.1 6.8 0.4 MN 3.5 WS	N 6.2 W 0.5 W 3.0 W 4.2	N 2.6	NNE 1.	7 NE 2 NNE 2 NNE	S. I NNE	6 2.6 6 4.1 N	N 2.5	NNE 1.	5 N 2.	N 2. N 1. 2 WSW 1. 5 WNW 2.	5 2.2 6 4.2 9 1.6 4 4.4 2 4.5
12	W 2.1 N 3.2 N 1.6 SW 2.2 W 4.6 W 4.5	WSW 2	.6 NNW .1 NNW .1 SW .6 WNW .4 W	2.1 6.8 0.4 NN 3.5 WS 4.0 5.2 WS	N 6.2 W 0.5 W 3.0 W 4.2 W 6.2	N 2.6 N 7.2 NNW 1.1 SW 3.5 W 4.1 SW 8.5	NNE 1. NNE 5. NNW 0. WSW 5. WSW 6.	7 NE 2 NNE 7 NNW 8 WSW 6 WNW 5 W	3.1 NNE 5.1 NNE 5.9 W.NW 7.2 W.SW 6.1 W.NW 7.5 W	5 2.6 E 4.1 N 7 1.0 V 5.0 W 7 6 1 W 7 7.6 W	N 2.5 NE 2.9 W 0.6 SW 6.5 NW 5.1 SW 5.5	NNE 1. WSW 6. WSW 6. WSW 6.	N 2. N 2. SW 2. WSW 5. WSW 4.	N 2. N 1. 2 WSW 1. 5 WNW 2. N W 5. 8 WSW 6.	5 2.2 6 4.1 9 1.6 4 4.4 2 4.2 4 6.2
13 14 15 16 17	W 2.1 N 3.2 N 1.6 SW 2.3 W 4.6 W 4.5 WSW 6.8	WSW 3	.6 NNW .1 NNW .1 SW .6 WNW .4 W	2.1 6.8 0.4 NN 3.5 WS 4.0 5.2 WS 4.0 NN	N 6,2 W 0,5 W 3,0 W 4,2 W 6,2 W 1,9	N 2.6 N 7.2 NNW 1.1 SW 3.5 W 4.1 SW 8.5 W 1.5 SSE 1.2	NNE 1. NNE 5. NNW 0. WSW 5. WSW 6. WNW 2.	7 NE 2 NNE 7 NNW 8 WSW 6 WNW 5 W	3.1 NNE 5.1 NNE 5.9 W.NW 7.2 W.SW 6.1 W.NW 7.5 W.SW	6 2.6 E 4.1 N V 1.0 V 5.0 W V 6.1 W V 7.6 W	N 2.5 NE 2.9 W 0.6 SW 6.5 NW 5.1 SW 5.5 SW 3.0	NNE 1. WSW 6. WSW 6. WSW 6. WSW 6.	N 2. N 2. SW 2. WSW 5. WSW 4. WSW 4. WSW 4.	N 2. N 1. 2 WSW 1. 5 WNW 2. N 5. WSW 6. 9 WNW 2.	5 2 6 4 9 1 4 4 2 4 4 6 5 3 6 2
13 14 15 16 17 8	W 2.1 N 3.2 N 1.0 SW 2.3 W 4.0 W 4.5 WSW 6.8 W 2.5	WSW 3 WSW 3 WSW 3 WSW 5 SW 2	.6 NNW .1 NNW .1 SW .6 WNW .4 W .8 WNW .2 SW	2.1 6.8 0.4 NN 3.5 WS 4.0 5.2 WS 4.0 NN 2.1 S	N 1.8 N 6.2 W 0.5 W 3.6 W 4.2 W 6.2 W 1.9 W 2.7 W 0.5	N 2.6 N 7.2 NNW 1.1 SW 3.5 W 4.1 SW 8.5 W 1.5 SSE 1.2	NNE 1.  NNE 5.  NNW 0.  WSW 5.  WSW 6.  WNW 2.  WNW 4.  WSW 1.	7 NE 2 NNE 7 NNW 8 WSW 6 WNW 5 W	3.1 NNE 5.1 NNE 5.2 WNW 7.2 WSW 6.1 WNW 7.5 WSW 1.7 WSW	5 2.6 6 4.1 N 7 1.0 7 5.0 W 7 6.1 W 7 7.6 W 6 2.5 W	N 2.5 W 0.6 SW 6.5 NW 5.1 SW 5.5 SW 3.0 W 2.7	NNE 1. WSW 0. WSW 6. WSW 5. WSW 6. WSW 2.	N 2.  N 2.  N 2.  N 2.  N 3.  N 3.  N 5 4 115 11 3.  N 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	N 2. N 1. 2 WSW 1. 5 WNW 2. 8 WSW 6. 9 WNW 2. WSW 1.	3 2.2 6 4.4 9 1.6 4 4.4 2 4.2 4 6.2 5 3.1 6 2.6
3 4 5 6 78 9	W 2.1 N 3.2 N 1.0 SW 2.3 W 4.0 W 4.3 WSW 6.8 W 2.3 WSW 1.0	WSW 3 WSW 3 WSW 3 WSW 5 SW 2	.6 NNW .1 NNW .1 SW .6 WNW .4 W .8 WNW .2 SW .9 SE .9 SSE	2.1 6.8 0.4 NN 3.5 WS 4.0 NN 2.1 S 1.3 SS 0.7 SS	N 1.8 N 6.2 W 0.5 W 3.0 W 4.2 W 6.2 W 1.9 W 2.7 W 0.5 E 0.8	N 2.6 N 7.2 NNW 1.1 SW 3.5 W 4.1 SW 8.5 W 1.5 SSE 1.2	NNE 1.  NNE 5.  NNW 0.  WSW 5.  WSW 6.  WNW 2.  WNW 4.  WSW 1.	7 NE 2 NNE 7 NNW 8 WSW 6 WNW 5 W 2 WSW 1 WNW 9 WNW	3.1 NNE 5.1 NNE 5.2 WNW 7.2 WSW 6.1 WNW 7.5 WSW 6.1 WSW 6.5 WSW	5 2.6 6 4.1 N 7 1.0 7 5.0 W 7 6.1 W 7 7.6 W 6 2.5 W 7 2.8 7 3.1 W 7 1.0 W	N 2.5 W 0.6 SW 6.5 NW 5.1 SW 5.5 SW 3.0 W 2.7	NNE 1. WSW 0. WSW 6. WSW 5. WSW 6. WSW 2.	N 2. N 2. SW 2. SW 3. WSW 4. WSW 4. WSW 4. SWSW 4. SWSW 4.	1 N 2. 2 WSW 1. 5 WSW 2. 6 W 5. 8 WSW 6. 9 WSW 2. 9 WSW 1. 9 SSW 0. 2 WSW 0.	3 2.2 6 4.2 9 1.6 4 4.4 2 4.2 4 6.2 5 3.1 6 2.6 6 1.9
13 14 15 6 7 8 9	W 2.1 N 3.2 N 1.6 SW 2.3 W 4.6 W 4.5 WSW 6.8 W 2.5 WSW 1.7 0.6	WSW 2 WSW 2 WSW 3 WSW 3 WSW 5 SW 2 SW 0 WSW 0	.6 NNW .1 NNW .1 SW .6 WNW .4 W .8 WNW .2 SW .9 SE .9 SSE .4 NW	2.1 6.8 0.4 NN 3.5 WS 4.0 WS 4.0 NN 2.1 S 1.3 SS 0.7 SS 1.0	N 1.8 N 6.2 W 0.5 W 3.0 W 4.2 W 6.2 W 1.9 W 2.7 W 0.5 E 0.8 N 1.5	N 2.6 N 7.2 NNW 1.1 SW 3.5 W 4.1 SW 8.5 SSE 1.2 WSW 0.9 SSW 1.0 NNE 1.4	NNE 1.  NNE 5.  NNW 0.  WSW 5.  WSW 6.  WNW 2.  WNW 4.  WSW 1.  NNE 2.  SSE 1	7 NE 2 NNE 7 NNW 8 WSW 6 WNW 5 WSW 2 WSW 1 WNW 9 WNW 9 NNE	3.1 NNE 5.1 NNE 5.1 WNW 7.2 WSW 6.1 WNW 7.5 WSW 1.7 WSW 1.7 WSW 1.8 WSW 2.1 NNE	5 2.6 E 4.1 N V 1.0 V 5.0 W V 7.6 W V 7.6 W V 2.5 W V 2.8 V 3.1 W V 3.5 E	N 2.5 W 0.6 SW 6.5 NW 5.1 SW 5.5 SW 2.7 SW 2.0 NW 1.5 NE 2.3	NNE 1. WSW 0. WSW 6. WSW 6. WSW 2. WSW 2. WSW 2. WSW 2. WSW 2. WSW 2. ESE 1.	N 2. N 2. N 2. N 2. N 3. N 3. N 4 WSW 3. WSW 4. WSW 4. WSW 4. N 4 WSW 2. N 1. WSW 1. N 1. N 1.	N 2. N 1. 2 WSW 1. 5 WSW 5. 8 WSW 6. 9 WSW 1. 9 WSW 1. 9 WSW 1. 9 WSW 1. 9 WSW 1. 9 WSW 1. 9 WSW 1.	3 2.2 6 4.2 9 1.0 4 4.4 2 4.2 4 6.2 4 6.2 6 2.0 6 1.9 7 1.5
3 4 5 6 7 8 9 0 1 2	W 2.5 N 3.2 N 1.6 SW 2.5 W 4.6 W 4.3 WSW 6.8 W 2.5 WSW 1.0 WSW 1.0 WSW 1.7	SW 0 N 1 N 1 WSW 2 WSW 3 WSW 3 SW 2 SW 2 SW 0 SW 0 WNW 0	.6 NNW .1 NNW .1 SW .6 WNW .4 W .8 WNW .2 SW .9 SE .9 SSE .9 SSE .9 NW .5 NW	2.1 6.8 0.4 NN 3.5 WS 4.0 WS 4.0 NN 2.1 S 1.3 SS 0.7 SS	N 1.8 N 6.2 W 0.5 W 3.0 W 4.2 W 6.2 W 1.9 W 2.7 W 2.7 W 2.7 W 0.5 W 2.7 W 0.5 W 0.5	N 2.6 N 7.2 NNW 1.1 SW 3.5 W 4.1 SW 8.5 W 1.5 SSE 1.2 WSW 0.9 SSW 1.0 NNE 1.4 ESE 1.6 SSW 0.6	NNE 1.  NNE 5.  NNW 0.  WSW 5.  WSW 6.  WNW 2.  WNW 4.  WNW 1.  NNE 1.  NNE 2.  SSE 1.	7 NE 2 NNE 7 NNW 8 WSW 6 WNW 5 WSW 1 WNW 9 WNW 9 WNW 1 NNE 1 S	3.1 NNE 5.1 NNE 5.1 WNW 7.2 WSW 6.1 WNW 7.5 WSW 1.7 WSW 4.5 WSW 4.5 WSW 2.1 NNE	5 2.6 5 4.1 N 5 5.0 W 7 7.6 W 7 7.6 W 7 2.5 W 1 2.5 W 1 2.5 W 1 2.5 W 2 3.1 W 3 3.1 W 3 3.5 E	N 2.5 W 0.6 SW 6.5 SW 5.1 SW 5.5 SW 2.7 SW 2.7 SW 2.0 W 1.5 NE 2.3 SW 0.9	NNE 1. WSW 0. WSW 6. WSW 2. WSW 3.	N 2. N 2. N 2. N 2. N 3. N 3	1	3 2. 6 4. 9 1. 9 4. 4 6. 2 4. 4 6. 5 3. 6 2. 6 1. 7 1. 1 1. 7 1. 1 1.
1 2 3 4 5 6 7 8 9 0 1 2 3	W 2.1 N 3.2 N 1.0 SW 2.3 W 4.0 W 4.5 WSW 6.8 WSW 1.7 0.0 S 1.0 SSW 1.4 S 1.0	SW 0 N 4 N 1 WSW 2 WSW 4 WSW 3 WSW 5 SW 2 SW 0 WSW 0 SSW 1	.6 NNW .1 NNW .1 SW .6 WNW .6 WNW .2 SW .9 SE .9 SSE .4 NW .5 NW .5 NW .1 WSW	2.1 6.8 0.4 NN 3.5 WS 4.0 WS 2.1 S 2.1 S 2.1 S 7.7 SS 1.0 0.6	N 1.8 N 6.2 W 0.5 W 3.0 W 4.2 W 1.9 W 2.7 W 0.5 E 0.8 N 1.5 W 0.2 SE 0.2 S 0.2	N 2.6 N 7.2 NNW 1.1 SW 3.5 W 4.1 SW 8.5 W 1.5 SSE 1.2 SSW 1.0 NNE 1.4 ESE 1.6 SSW 0.6 SW 1.0	NNE 1.  NNE 5.  NNW 0.  WSW 5.  WSW 6.  WNW 2.  WNW 4.  WSW 1.  NNE 2.  SSE 1.  SSW 1.  SSW 1.  SSW 1.  WNW 2.	7 NE 2 NNE 7 NNW 8 WSW 6 WNW 5 WSW WNW 9 WSW WNW 9 NNE 1 S 1 SW 1 WSW	3.1 NNB 5.1 NNB 7.2 WSW 7.2 WSW 7.5 WNW 7.5 WSW 4.5 WS	6 2.6 6 4.1 N 7 1.0 7 5.0 W 7 7.6 W 7 7.6 W 7 7.6 W 7 2.5 W 7 2.8 W 7 3.1 W 7 1.9 W 7 3.5 E	N 2.5 NE 2.9 W 0.6 SW 6.5 SW 5.1 SW 5.5 SW 2.0 W 2.0 SW 2.0 SW 1.5 NE 2.3 SW 0.9 W 1.1 S 0.5 SW 0.9	NNE 1. WSW 0. WSW 6. WSW 5. WSW 2. WSW 3. WSW 0. SEE 1.	N 2. N 2. N 2. N 2. N 3. N 3	N 2. N 1. 2 WSW 1. SWNW 2. SWW 6. SSW 0. 2 WSW 6. SWW 6. SWW 1. SWW 0. SWW 1. S	3 2.6 6 4.2 9 1.0 9 1.0 4 4.5 2 4.1 4 6.2 6 2.0 6 1.9 7 1.9 5 1.0 7 1.9
1 2 3 4 5 6 7 8 9 0 1 2 3 4	W 2.1 N 3.2 N 1.0 SW 2.2 W 4.0 W 4.0 WSW 6.8 WSW 1.0 WSW 1.0 SSW 1.0 SSW 1.0 W 0.0	SW 0 N 4 WSW 3 WSW 5 SW 2 SW 0 WSW 5 SW 2 SW 0 WSW 5 SW 1 SSW 0	.6 NNW .1 NNW .1 NNW .1 NNW .6 WNW .6 WNW .8 WNW .2 SW .9 SE .4 NW .5 NW .5 NW .1 WSW .3 SSW	2.1 6.8 0.4 NN 3.5 WS 4.0 NS 2.1 S 1.3 SS 1.3 SS 1.0 NS 1.0 NS 1.	N 1.8 N 6.2 W 0.5 W 3.0 W 4.2 W 1.9 W 2.7 W 0.5 S 0.5 W 0.2 S 0.5 W 0.9	N 2.6 N 7.2 NNW 1.1 SW 3.5 W 4.1 SW 8.5 W 1.5 SSE 1.2 WSW 0.9 SSW 1.0 NNE 1.4 ESE 1.6 SSW 0.6 SW 1.0 SW 2.4 SSW 0.8	NNE 1.  NNE 5.  NNW 0.  WSW 5.  WSW 6.  WNW 2.  WNW 4.  WNW 4.  WNW 1.  NNE 2.  SSE 1.  SSW 1.  SW 1.	7 NE 2 NNE 7 NNW 8 WSW 6 WNW 5 WSW 1 WSW 1 WSW 1 WSW 2 WSW 1 WSW 3 NNE 1 SW 2 WSW 4 SSW	3.1 NNM 3.1 NNM 0.9 WNW 2.2 WSW 6.1 WNW 7.5 WSW 4.5 WSW 4.5 WSW 4.5 WSW 4.6 WSW 2.2 NNM 3.6 WSW 2.2 WSW 4.5 WSW 4.5 WSW 4.6 WSW 4.6 WSW 4.6 WSW 4.6 WSW 4.7 WSW 4.7 WSW 4.8	6 2.6 6 4.1 N 7 1.0 W 7 0.1 W 7 0.1 W 7 7.6 W 8 2.5 W 7 2.8 W 7 1.9 W 7 1.9 W 8 1.5 S 8 1.5 S 8 1.5 S 8 1.2 S 8 1.3 W 8 1.3 W 8 1.3 W	N 2.5 NE 2.9 W 0.6 SW 6.5 SW 5.1 SW 5.1 SW 2.7 SW 2.0 SW 2.0 SW 2.0 SW 1.5 SW 0.9 W 1.1 S 0.5 SW 0.7 NE 0.7	NNE 1. WSW 0. WSW 6. WNW 5. WSW 6. WSW 2. WSW 2. WSW 2. WSW 2. WSW 1 SW 1 N 1.	N 2. N 2. N 2. N 2. N 2. N 3. N 3	1	3 2.6 6 4.1 9 1.6 9 1.6 4 4.2 4 6.2 4 6.2 6 1.9 1 1.6 7 1.1 1 1.3 1 1.3
3 4 5 6 7 8 9 0 1 2 3 4 5 6	W 2.1 N 3.2 N 1.0 SW 2.2 W 4.0 W 4.5 WSW 6.8 WSW 1.7 SSW 1.4 S 1.0 SSW 1.4 S 1.0 N 0.6 N 1.1	SW 0 N 4 N 1 WSW 2 WSW 3 WSW 5 SW 2 SW 0 WNW 0 SW 1 SSW 1 SSW 1	.6 NNW .1 NNW .1 SW .6 WNW .4 W .8 WNW .2 SW .9 SE .4 NW .5 NW .2 SSE .4 NW .1 WSW .3 SSW .3 SSW	2.1 6.8 0.4 NN 3.5 WS 4.0 5.2 WS 4.0 NN 2.1 S 1.3 SS 0.7 SS 1.0 0.6 S	N 1.8 N 6.2 W 0.5 W 4.2 W 6.2 W 1.9 W 2.7 W 2.7 N 1.5 W 0.2 SE 0.2 S 0.2 N 0.9 N 0.9	N 2.6 N 7.2 NNW 1.1 SW 3.5 W 4.1: SW 8.5 W 1.5 SSE 1.2 WSW 0.9 SSW 1.0 NNE 1.4 ESE 1.6 SW 1.6 SW 1.0 SW 1.0 SW 1.0	NNE 1.  NNE 5.  NNW 0.  WSW 5.  WSW 6.  WNW 2.  WNW 1.  NNE 2.  SSE 1.  SSW 1.  WNW 2.  SW 0.	7 NE 2 NNE 7 NNW 8 WSW 6 WSW 1 WSW 9 WSW 1 WSW 1 SW 2 WSW 1 SSW 2 WSW 1 SSW	3.1 NNB 3.1 NNB 3.1 NNB 3.2 WSW 5.1 WSW 5.5 WSW 5.5 WSW 5.5 WSW 5.5 WSW 5.5 WSW 5.5 WSW 5.5 WSW 5.5 WSW 5.6 WSW 5.6 WSW 5.6 WSW 5.6 WSW 5.6 WSW 5.7 WSW 5.8	6 2.6 6 4.1 N 7 1.0 W 7 0.1 W 7 0.1 W 7 7.6 W 8 2.5 W 7 2.8 W 7 3.1 W 7 1.9 W 8 1.5 S 8 1.5 S	N 2.5 NE 2.9 W 0.6 SW 6.5 SW 5.5 SW 2.7 SSW 2.0 YW 2.7 SSW 2.0 YW 1.1 SSW 2.0 YW 1.1 SSW 0.9 W 1.1 SSW 0.5 SSW 0.9 W 1.1 SSW 0.5 SSW 0.9 W 1.1 SSW 0.5 SSW 0.5 SSW 0.6 SSW 0.6 SS	NNE 1. WSW 0. WSW 6. WSW 6. WSW 2. WSW 2. WSW 2. WSW 2. WSW 1	N 2. N 2. N 2. N 3. N 3	N 2. N 1. N 1. N N 1. N N 1. N N 1. N N 2. N S W 5. N W S W 5. N W S W 2. N N 0. N N 0. N N 0. N W 0.	3 2.6 4 4.2 9 1.0 9 4 4.2 4 5 4.1 6 5 2.6 6 2.6 6 1.9 6 1.1 7 1.1 1 1.3 1 1.3
1 2 3 4 5 6 7 8 9 0 1 2 3 4 5 6 7 7	W 2.1 N 3.2 N 1.6 SW 2.3 W 4.6 W 4.5 W 5.0 W 5.0 W 5.0 W 6.0 SSW 1.6 SSW 1.6 N 1.1 SW 6.6	SW 0 N 1 WSW 2 WNW 4 WSW 3 WSW 5 SW 0 SW 0 WNW 0 SSW 1 SSW 0 SSW 1	.6 NNW .1 NNW .1 NNW .1 NNW .1 SW .6 WNW .4 W .8 WNW .9 SE .9 SSE .4 NW .5 NW .5 NW .5 NW .5 SSW .1 WSW .3 SSW .1 WSW .3 SSW	2.1 6.8 0.4 NN 3.5 WS 4.0 WS 4.0 NN 1.3 SS 0.7 SS 1.0 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0	N 1.8 N 6.2 W 0.5 W 4.2 W 6.2 W 1.9 W 2.7 W 2.7 W 0.2 E 0.5 N 1.5 W 0.2 E 0.2 W 0.9 N 1.0 W 0.2	N 2.6 N 7.2 NNW 1.1 SW 3.5 W 4.1 SSE 1.2 WSW 0.9 SSW 1.0 NNE 1.4 ESE 1.6 SW 1.0 SSW 0.6 SW 1.0 SSW 0.9 SSW 0.9	NNE 1. NNE 5. NNW 0. WSW 5. WSW 6. WSW 4. WSW 1. WNW 2. SSE 1. SSW 1. SW 0. N 2. SW 0.	7 NE 2 NNE 7 NNW 8 WSW 6 WSW 1 WSW 1 WSW 1 WSW 1 WSW 1 WSW 1 SW 2 WSW 3 NW 4 SSW	3.1 NNB 5.1 NNB 5.1 NNB 9 WNW 7.2 WSW 6.1 WNW 7.5 WSW 4.5 W	6 2.6 6 4.1 N 7 5.0 W 7 5.0 W 7 7.6 W 8 2.5 W 7 2.8 W 7 3.1 W 7 5	N 2.5 NE 2.9 W 0.6 SW 6.5 SW 5.5 SW 5.5 SW 3.0 W 2.7 SW 2.7 S	NNE 1, WSW 0, WSW 6, WSW 6, WSW 2, WSW 2, WSW 2, WSW 1, WS	N 2, N 2, N 2, N 2, N 3, N 4 WSW 5, WSW 3, N 8 WSW 2, N 1, N 5 WSW 0, N 1, N 8 WSW 0, N 1, N 8 WSW 1, N 8 WSW 1, N 8 WSW 1, N 8 WSW 1, N 1, N 8 WSW 1, N 1, N 8 WSW 1, N	N 2.  N 1.  W N 1.  W N 1.  W S 1.  W N 5.  W S 6.  W S 6.  W S 7.  W S 7.  W S 7.  W S 8 W 1.  S S W 0.  S W 1.  S S S W 1.  S S S W 1.	3 2.6 4 4.2 9 1.6 9 4.6 2 4.1 4 6.2 4 6.2 6 2.6 6 1.1 7 1.1 1.3 1.3 1.3 1.3 1.3 1.3 1.3 1.3 1.3
11 12 13 14 15 16 17 8 9 9 11 12 13 14 15 16 17 18 19 19 19 19 19 19 19 19 19 19 19 19 19	W 2.1 N 3.2 N 1.6 SW 2.2 W 4.6 W 4.5 WSW 6.8 WSW 1.7 O.0 W 0.9 SSW 1.4 SW 0.6 N 1.1 SW 0.6 WSW 2.2 W 3.2 W 3.2 W 3.2 W 3.2 W 3.2 W 3.2	SW 0 N 1 WSW 3 WSW 5 SW 0 WNW 0 WNW 0 SSW 1 SSW 0 N WNW 0 SSW 1 SSW 0 N WNW 0	.6 NNW .1 NNW .1 NNW .1 NNW .1 NNW .2 SW .9 SE .9 SSE .9 S	2.1 6.8 0.4 NN 3.5 WS 4.0 VS 4.0 NS 2.1 S 0.7 S 1.3 SS 0.7 S 1.0 S 0.6 S 0.6 S 0.6 S 0.6 S 0.6 S 0.6 S 0.7 SS	X 1.8 X 6.2 W 3.0 W 4.2 W 1.7 W 0.5 E 0.8 N 0.2 E 0.8 N 0.2 E 0.8 N 0.2 E 0.8 N 1.5 N 0.2 E 0.8 N 1.5 N 0.5 N 1.5 N 0.5 N	N 2.6 N 7.2 NNW 1.1 SW 3.5 W 4.1 SSE 1.2 WSW 0.9 SSW 1.0 NNE 1.4 ESE 1.6 SSW 1.0 VNW 2.4 SSW 0.8 VNW 2.4 SSW 0.8 VNW 4.1 SSW 0.8	NNE 1. NNE 5. NNW 0. WSW 5. WSW 6. WNW 4. WNW 4. WSW 1. NNE 2. SSE 1. SSW 1. SW 0. N 2. SW 0. N 2. SW 3.	7 NE 2 NNE 7 NNW 8 WSW 6 WWW 1 WNW 9 WNW 1 WNW 1 SW 2 WSW 3 WW 4 SSW 4 SSW 4 SSW 4 SSW 6 WW 6 WW 6 WW 6 WSW 6 WS	3.1 NNB 5.1 NNB 5.1 NNB 6.1 WNW 7.5 WN 6.1 WNW 7.5 WSW 4.5 WSW 4.5 WSW 4.5 WSW 4.5 WSW 4.5 WSW 4.6 WSW 4.6 WSW 4.7	6 2.6 8 4.1 N 7 5.0 W 7 5.0 W 7 7.6 W 7 7.6 W 7 7.6 W 7 2.8 W 7 2.8 W 7 2.8 W 7 2.8 W 7 2.8 W 7 2.8 W 7 3.1 W 7 5 W	N 2.5 NE 2.9 W 0.6 SW 6.5 SW 5.5 SW 3.0 W 2.77 SW 2.7 SW 2.7 SW 2.7 SW 2.7 SW 2.7 SW 2.7 SW 2.7 SW 2.7 SW 2.7 SW 6.7 SW 6.7	NNE 1. WSW 0. WSW 6. WNW 5. WSW 6. WSW 2. WSW 2. WSW 2. WSW 1 0. SW 1 0. SW 1. NNW 0. SW 1. WNW 4. WSW 1.	N 2. N 2. N 2. N 3. N 3	N 2. WSW 1. SWW 2. SWW 4. SWW 6. SWW	3 2.6 4 4.2 9 1.6 4 4.2 4 5 5 3.1 6 1.5 6 1.5 6 1.5 7 1.5 7 1.6 7 1.5 1
11 13 13 14 15 16 17 8 9 9 19 19 19 19 19 19 19 19 19 19 19 19	W 2.1 N 3.2 N 1.6 SW 2.2 W 4.0 W 4.2 WSW 6.8 WSW 1.7 O.0 SSW 1.4 S 1.0 S 1.0 S 1.0 S 1.0 S 1.1 S 1.0 S 1.2 S 2.2 S 5.2 S 5	SW 0 N 1 WSW 3 WSW 3 SW 2 SW 0 WNW 0 SW 1 SSW 1 SSW 1 SSW 1 SW 3 WNW 5	.6 NNW .1 NNW .1 SW .6 WNW .4 W .6 WNW .2 SW .9 SE .4 NW .5 NW .5 NW .1 WSW .1 SSW .1 WSW	2.1 6.8 0.4 NN 3.5 4.0 5.2 WS 4.0 NN 5.2 1.3 5.0.7 8.0.6 1.9 0.6 1.9 0.6 0.6 1.9 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6	X 1.8 X 6.2 W 3.6 W 4.2 W 4.2 W 1.9 W 0.5 E 0.8 N 1.5 E 0.8 N 1.5 W 2.5 W 2.5 W 2.5 W 2.5 W 3.6 W 4.1 W 3.6 W 4.2 W 4.1 W 3.6 W 3.6	N 2.6 N 7.2 NNW 1.1 SW 3.5 W 4.1 SW 9.5 W 1.5 SSW 1.0 NNE 1.4 SSW 0.6 SW 1.0 VNW 2.4 SSW 0.8 VNW 2.4 SSW 0.8 VNW 1.1 SW 2.8 W 4.1 SW 1.8 SSW 0.6	NNE 1.  NNE 5.  NNW 0.  WSW 5.  WSW 5.  WNW 2.  WNW 4.  WSW 1.  WNW 1.  SSE 1.  SSW 1.  SW 2.  SW 3.  SW 3.  SW 3.	7 NE 2 NNW NW WSW WSW WSW WSW WSW WSW WSW WSW	3.1 NNB 5.1 NNB 9 WNW 7.2 WSW 6.1 WNW WSW 4.5 WSW 4.5 WSW 4.5 WSW 4.5 SW 8.6 WSW 2.1 NNB 6.6 WSW 2.1 NNB 6.6 WSW 2.2 NNB 6.6 NNB 6.6 WSW 2.2 NNB 6.6 N	6 2.6 W 7 5.0 W 7 5.0 W 7 6.1 W 7 7.6 W 7 7 6.1 W 7 7 6 W 7 7 6 W 7 7 6 W 7 7 6 W 7 7 6 W 7 7 1 7 7 1 7 1 7 1 7 1 7 1 7 1 7 1 7	N 2.5 NE 2.9 W 0.6 SW 6.5 SW 5.1 SSW 5.5 SSW 3.0 W 2.7 SSW 2.0 W 2.7 SSW 2.0 SSW 0.9 W 1.1 S 0.5 SSW 0.7	NNE 1. WSW 0. WSW 6. WSW 6. WSW 6. WSW 2. WSW 2. WSW 2. WSW 2. NNE 2. ESE 1. W 0. SW 1. NNW 0. SW 1. WSW 4. WSW 1.	N 2. N 2. N 2. N 3. N 3	N 2. N 1. S W N 1. S W N 2. S W N W 2. S W N W 2. N S W N W 2. N W O. S W W	3 2.6 6 4.6 9 1.0 4 4.6 4 6.3 5 3.0 6 1.9 6 2.6 6 1.9 7 1.0 7 1.0 1 1.0 3 1.0 3 1.0 3 1.0 3 1.0 4 1.0 5 1.0 6 1.0 6 1.0 7 1.0 8 1.0
1 2 3 4 4 5 5 6 6 7 7 8 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9	W 2.1 N 3.2 N 1.6 SW 2.2 W 4.6 W 4.5 WSW 6.8 WSW 1.7 O.0 W 0.9 SSW 1.4 SW 0.6 N 1.1 SW 0.6 WSW 2.2 W 3.2 W 3.2 W 3.2 W 3.2 W 3.2 W 3.2	SW 0 N 1 N 1 WSW 3 WSW 3 WSW 3 SW 2 SW 0 WNW 0 SSW 1 SSW 0 N 0 SSW 1 SSW 0 SW 3 WNW 5 SSW 3 WNW 5 SE 1	.6 NNW .1 NNW .1 NNW .1 SW .6 WNW .2 SW .2 SW .4 NW .5 NW .5 SSW .1 WSW .1 WSW .1 WSW .1 WSW .1 WSW .2 SSE .2 SSE .3 SSW .1 WSW .1 WSW .2 SSW .3 SSW .1 WSW .1 WSW .2 SSW .3 SSW .4 SSW .5 SSW .5 SSW .5 SSW .6 SSW .6 SSW .7 SSW .7 SSW .7 SSW .8 SSW .8 SSW .9 SSE .9 SSE .9 SSSW .1 WSW .2 SSW .2 SSW .3 SSW .3 SSW .3 SSW .4 SSW .5 SSW	2.1 6.8 0.4 NN 3.5 4.0 5.2 WS 4.0 NN 5.2 1.3 5.0.7 8.0.6 1.9 0.6 1.9 0.6 0.6 1.9 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6	X 1.8 X 6.2 W 3.6 W 4.2 W 4.2 W 1.9 W 0.5 E 0.8 N 1.5 E 0.8 N 1.5 W 2.5 W 2.5 W 2.5 W 2.5 W 3.6 W 4.1 W 3.6 W 4.2 W 4.1 W 3.6 W 3.6	N 2.6 N 7.2 NNW 1.1 SW 3.5 W 4.1 SSE 1.2 WSW 0.9 SSW 1.0 NNE 1.4 ESE 1.6 SSW 1.0 VNW 2.4 SSW 0.8 VNW 2.4 SSW 0.8 VNW 4.1 SSW 0.8	NNE 1. NNE 5. NNW 0. WSW 5. WSW 6. WNW 4. WNW 4. WSW 1. NNE 2. SSE 1. SSW 1. SW 0. N 2. SW 0. N 2. SW 3.	7 NE 2 NNE 2 NNW 8 WSW 8 WSW 9 WNW 9 WNW 9 WNW 1 WSW 1 WSW 1 WSW 1 SSW 1 SSW 5 SSW 9 SSW	3.1 NNB 5.1 NNB 9 WNW 7.2 WSW 6.1 WNW WSW 4.5 WSW 4.5 WSW 4.5 WSW 4.5 SW 8.6 WSW 2.1 NNB 6.6 WSW 2.1 NNB 6.6 WSW 2.2 NNB 6.6 NNB 6.6 WSW 2.2 NNB 6.6 N	6 2.6 V 5.0 W 7 7 6.1 W 7 7.6 W 7 7 6 W 7 7 6 W 7 7 6 W 7 7 7 7 7 7	N 2.5 NE 2.9 W 0.6 SW 6.5 SW 5.5 SW 3.0 W 2.77 SW 2.7 SW 2.7 SW 2.7 SW 2.7 SW 2.7 SW 2.7 SW 2.7 SW 2.7 SW 2.7 SW 6.7 SW 6.7	NNE 1. WSW 0. WSW 6. WNW 5. WSW 6. WSW 2. WSW 2. WSW 2. WSW 1 0. SW 1 0. SW 1. NNW 0. SW 1. WNW 4. WSW 1.	N 2. N 2. N 2. N 3. N 3	N 2. 2 WSW 1. 2 WSW 5. 5 WSW 6. 5 WSW 6. 5 WSW 6. 5 WSW 6. 6 WSW 1. 1 SSW 0. 2 WSW 1. 1 SSW 0. 2 WSW 1. 5 SSW 3. 5 WSW 3	3 2. 6 4. 9 1. 4 4. 4 6. 5 3. 6 1. 7 1. 7 1. 1 1. 1 1. 1 1. 1 1. 1 1. 1

			aj I	irekte Ablest	angen			
	Luftdruc	k auf o' reduz	ert in Millim.	== 700** +	L	ufttempera	tur nach Cele	ius
Tag	19t	24	94	Tagesmittel	191	211	94	Tagesmitte
			89	1 1		•	0	1 .
1	39.4	38.3	37.9	38.53	2.4	7.6	4.3	4.77
2	34.8	32.6	35.2	34.20	7.0	10.3	7.7	8.33
3	40.3	43.2	46.3	43.27	7.0	11.0	6.6	8.20
4	48.9	45.2	47 - 4	48.17	2.6	13.3	6.1	6.33
5	42.0	39.2	33.9	38,67	6.5	13.3	11.5	10.53
6	14.0	37.0	39.5	36.83	11.8	13.1	10.0	11.63
7	42.0	40.8	40.8	41.20	2.8	8.6	8.4	6.60
7 8	40,2	49.7	41.4	40.77	7.9	9.3	6.9	8.03
9	37.8	36.4	39.5	37.90	5 - 4	8.3	4.4	6,03
10	40.1	42.3	43.9	42.10	4.9	4.6	4.0	4.50
11	44.0	42.6	39.5	42.03	4.0	4.9	3.4	4.10
12	32.1	31.7	32.7	32.17	1.9	3.6	1.5	2.33
13	29.0	27.2	26.5	27.57	2.1	5-3	5.0	4.13
14	25.4	27.2 25.1	26.9	25.80	4.4	3.5	1.2	3.03
15	29.9	32.6	34.8	32.43	2.8	4.4	0.3	2.50
16	33.6	32.9	36.7	34.40	0.1	1.2	1.1	0.50
17		46.2	50.4	46.53	1.1	2.6	1.9	1.87
18	43.0 53.4	53.1	51.5	52.67	- 1.1	2.1	- 0.3	0.23
01	44.7	40.1	34.7	39.83	0.4	3 - 2	2.6	2.07
20	39.3	42.0	46.9	42.93	4.9	7.9	5.8	6.20
21	50.7	50.7	50.8	50.73	3.1	6.8	2.8	4.23
22	49.5	49.7	51.2	50.13	2.6	5.6	2.2	3.47
23	50.2	46.7	42.9	46.60	1.6	2.4	1.4	1.50
24	36.3	38.5	40.2	38.33	1.4	5.4	1.9	3.57
25	42.9	44.6	45.9	44.47	3.7	5.8	2.6	4.03
26	44.6	42.7	40.7	42.67	-0.5	4.1	4.8	2.80
	38.9	38.6	41.1	39-53	- 0.5	10.6	6.8	0.40
27	42.8	42.5	41.0	42.40	3.0	6.7	1.4	3.70
29	40.5	42.3	45.1	42.63	1.2	2.2	1.8	1.73
30	48.3	50.3	52.1	50.23	0.8	1.2	1.2	1.07
Mittel	40.65	40.65	41.28	40.86	3.25	6.20	4.05	4.50

Tag	Dun	stdruck	in Millim	etern	Rel	ative F	euchtig	keit	Rich	tung	u, Ståi [Skaia: e	ke d	es Wine	de
	19 <sup>t</sup>	34	94	Tages- mittel	19h	28	9 <sup>k</sup>	Tages-	196		26		98	
	5-4	6.1	5.8	1 53	98	79	-	90	N	_	N			0
	6.7	6.0	6.1	6.3	89	79 64	93 77	77	SE		SE	2	SW	3
1	6.0	6.1	5.9	6.0	79	62	81	74	SW	2	SW			2
4	5.1	6.3		5.7	93	67	81	80	SW	ī	E	2	ESE	ì
5	6.3	8,0	5.7	7.6	87	71	81	80	ENE	i	SE	2	ESE	i
6	7.7	8.0	5.6	7.1	7.5	72	61	69	8		w	2	W	
7	5.1	6.3	7.0	6,1	91	76	86	84			NE.	i	ENR	3
7 8	7-3	6.7	6.4	6.8	92	76	86	85	***	0	SW	3	***	è
9	6.5	6.9	5.8	6.4	97	86	93	92	NW	2	NE	ï	NW	3
10	5.1	5.2	5.1	5.1	78	82	84	81	W	3	W	2	W	- 3
11	4.9	5.1	5.1	5.0	80	78	87	82	W		WNW			
12	4.5	4.3	4.4	4.4	86	73	85	St	ESE		SE	1		
13	4.8	5.6	5.8	5.4	89	85	89	88	E		SE		SE	1
14	6.0	5.2	4.9	5.4	97	88	98	94	N	1	NNE	2	N	3
15	4.4	4.0	3-7	4.0	77	63	78	73	W	3	W	2		4
16	3.4	3.8	3.9	3.7	73	75	79	76	***	0	N	3	WNW	
17	3.9	3.2	3.8	3.6	77	75 88	7.3	69	SW	1	WNW	2	W	1
18	3.4	3.4	3.6	3.5	8a	64	81	75		0	SE	t	SE	1
19	4.0	4.7	5.1	4.6	85	Sı	93	86	Е	2	ENE	2	E	- 1
20	5-5	6.4	6.4	6.1	84	81	93	86	M.	3	WSW	1	SSW	-
21	5-3	6.1	5.6	5-7	93	82	100	92	***	0	NE	1		-
22	5.4	6.0	5-3	5.6	98	88	98	95	W	1	***	0	WSW	
23	5.0	5.1	4.4	4.8	96	93	87	92	WSW	1	W	1	SW	2
24	4.8	5.0	4.8	4.9	94	75	78	82	SSW	2	W	3	WNW	3
25	4.6	4.1	4.6	4.4	77	60	82	73	W	2	W	3	SW	3
26	3.9	4.5	4.8	4.4	88	74	74	79	S	1	SSW	1	SSW	2
27	4-4	6.1	5.9	5-5	84	64	80	76	8	2	SW	2	SW	2
28	4.5	4.5	4.4	4-5	79	61	87	76	WSW	2	SW	2	SW	
29	4.5	4.7	4.8	4-7	91	87	91	90	***	0	N	1	NNW	0
30	4-3	4-5	4-4	4-4	89	91	89	90	NNW	1	N		naw	2
Mittel	5.1	5.4	5.2	5.2	87	75	84	82		1.2		1.6		

## NOVEMBER

Tag	Be	wõlkung	(Skala: e	ke n z u	er, 10 :	= trūb]	Nieder- schiag in	Bemerkungen
	194		24		94	Tagesmittel	Milli- metern	
1 2 3 4 5	S 10 FS 5 HS 10 HS 3 S 10	FHS FHS	8 10 8 7 10	FS	10 ··· 6 ··· 10 ··· 3 ··· 10 ···	7.0 9.3 4.3	2.5	Morgens =, △, mittags =, abends =, △. Morgens =, △, mittags Dunst, 4½ ♠, 6²u.8² ♠ Morgens =, abends =, △. Morgens =, △, mittags Dunst, abends =, △. Morgens =, △, abends =, △.
6 7 8 9	FHS 10 FHS 6 HS 10 S 10	FHS HS	10 SW 9 E 10 10	HS S S	10 ··· 10 ··· 10 ··· 10 ···	8.3 10.0 10.0	10.3 *8.9	Morgens dunstig, $\triangle$ , 61 Tropfen.  Morgens $\Longrightarrow$ , $\triangle$ , abends $\Longrightarrow$ , $z_3$ 1 $\longrightarrow$ $0$ 1 Morgens $\Longrightarrow$ , vorm. u. nachm $\bigcirc$ , $\longrightarrow$ m. Unterby.  Vormittags u. nachts $\bigcirc$
11 12 13 14	S 10 S 10 S 10 FHS 10	HS HS HS	10 10 SE 10 N 6 NW	FHS	10 10 SW 10 10 3	10.0 10.0 10.0 10.0 10.0 6.3	0.8	Abends =,, abends =,, Morgens =,, ole1+ O., nachts O. Norg. =, vormit u. nachmit regner, 9 * u. O. Abends =,, 10 Nordicht.
16 17 18 19	HS 10 S 3 HS 10 FHS 10 W	- HS FHS	10 ···· 8 S 10 ···· 10 W	FS S	10 10 3 10	10.0	  	Morgens ==,, abends ==,
21 22 23 24 25	FHS 6 S 10 S 10 S 10 FHS 10 W	FHS S HS	6 4 10 10 W 7 W	S	10 ··· 10 ··· 10 ··· 5 ··· 2 ···		1.1 1.4	Morgens =, mittage dunstig, abende =, Morg. =,, mitt. dunstig, abends =,, 4½ =, Morg. =,, mitt. u. abends =,, achts ±. Morgons =, ⊕, vormittags regnerisch.
26 27 28 29 30	FHS 7 FHS 9 W FS 2 HS 10 S 10	FH FH	10 7 W 3 10	HS FS S	10 ··· 10 ··· 2 ··· 10 ··· 10 ···	9.0 8.7 2.3 10.0		Morgens =, mittags und abends dunstig. Morgens Dunst, Eis. Morgens Dunst, abends =, am Hor., Morgens =, mittags w. abends =, Morgens und mittags =, abends Dunst.
Mittel	8.7		8.8		8.5	8.7	S. 30.9	
-					b Au	tographische	Aufzei	chnungen

						b Aut	ograpl	ische	Aufze	ichnus	ngen				
	1				Luft	druck	auf o	reduzier	t in Mil	limeters	1 = 700°	" +			
Tag	124	14 <sup>h</sup>	16%	18h	20h	22h	Op	2 <sup>h</sup>	44	6r	8tı	10h	Tages- mittel	Max.	Min
1	30.0	39.0	39.0	39.3	39.5	39.8	39.4	38.3	37.8	37.9	38.1	37.9	38.75	39.8	37.
2	37.1	36.4	35.7	35.0	34.0	34.5	33.6	32.6	13.2	33.0	34.4	30.3	34.64	37.3	32.
3	37.3	38.3	39.0	39.8	41.0	42.3	43.1	43.2	44.0	45.0	45.9	46,6	42.13	47.4	37-
4	47.4	47.9	48.4	45.8	49.3	49.5	48.8	48.2	48.1	47.8	47.5	47.2	48.24	49.5	46.
5	46.4	45.3	44.3	43-1	42.9	42,1	41.0	39.2	38.3	16.9	35.2	33.2	40.66	46.4	32.
6	32.0	31.4	31.9	33.3	34.7	16.1	16.4	37.0	37 - 4	18.7	39.2	40.0	35.68	40.5	31.
7	40.5	40.0	41.4	41.8	42.0	42.2	42.0	40.8	40.6	40.8	40.8	40.7	41.21	42.2	40.
8	40.0	40.8	40.4	40.1	40.3	40.6	40,9	40.7	41.2	41.4	41.5	41.3	40.84	41.5	40,
9	41.1	40.8	40.0	15.8	37.4	37.2	36.5	36.4	37.1	38.2	39.1	39.6	38.52	41.1	36.
10	39-5	39.6	39.7	39.7	40.4	41.3	41.7	42.3	43.7	43.2	43.7	44.0	41.48	44.0	39.
11	44.0	44.3	44.0	43.9	43.8	44.0	43.6	42.6	41.8	41.1	39.9	38.8	42.63	44.8	37-
12	37.0	35.3	33.6	32.2	32.4	32.3	31.8	31.7	32.0	32.3	32.6	33.0	13.01	37.0	31.
13	32.4	31.4	30.5	29.3	28.7	28.2	27.4	27.2	26.8	26,5	26.3	26.5	28.43	32.4	26.
14	26.3	25.9	25.8	25.5	25.4	25.3	25.2	25.1	25.6	26.4	26.6	27.3	25.86	27.5	25.
15	27.5	28.1	28.7	29.5	30.6	31.8	32.2	32.6	33.1	33 - 7	34-7	34.8	31.44	34.8	27.
16	34.5	34.3	34.0	33.4	33.8	33.7	33.4	32.9	33.7	35.1	36.2	37.3	34.36	38.3	32.
17	38.3	19.2	40.4	42.1	43.8	44-7	45.6	46.2	47.3	48.5	49.6	51.0	44.73	51.9	38.
18	51.0	52.3	53.0	53.4	53.7	54.4	54.0	53.1	52.6	52.6	52.2	51.0	\$2.85	54.0	49.
19	49.9	47.8	46.1	44.8	42.9	42.3	41.5	40.1	38.9	37.0	35.4	34.2	41.74	49.9	34 -
20	34.7	35-7	36.8	38.6	39.7	40.7	41.7	42.6	43.8	45.4	46.2	47-3	41.10	47.8	34 -
21	47.8	48.5	49.3	50.3	50.7	50.7	50.7	50.7	50.7	51.0	50.0	50.7	50.17	51.0	47.
22	50.5	50.2	50.0	40.6	49.4	49.4	49.4	49.7	49.8	50.4	50.8	51.4	50.05	51.4	49.
23	51.3	51.0	50.3	50.3	50.3	49.5	48.1	46.7	45.6	44.8	43.6	41.7	47.70	51.2	40.
24	40.4	39.2	38.0	37.0	36.6	37.2	37.9	18.5	39.1	39.8	40.0	40.5	35,68	40.7	36.
25	40.7	41.3	41.8	42.5	43.2	44.2	44.5	44.6	45.0	45.3	45.7	45.9	43.73	45.9	40.
26	45.0	45.5	45.0	44.5	44.2	43.9	43.2	42.7	42.3	42.1	41.4	40.5	43.43	45.9	39.
27	39.9	39.3	39.1	18.8	39.3	18.9	18.7	18.6	39.0	19.8	40.7	41.6	39,48	41.9	18.
28	41.9	42.4	42.3	42.6	42.8	43.0	43.8	42.5	42.3	42.4	42.0	41.6	42.41	43.8	41.
29	41.1	40.6	40.4	40.4	40.9	41.5	42.1	42.3	43.1	43.9	44.7	45.4	42,20	46.3	40.4
30	46.3	47.1	47.1	48.0	49.0	50.1	50.3	50.3	50.8	51.6	51.8	52.1	49.54	52.2	46,
fittei	40.78	40.65	40,53	40.55	40.79	41.05	40.93	40.65	49.76	41.00	41.22	41.31	40.86	43.90	37 -

ag						L	ufttems	eratu	r nach C	cisius					
	12h	14 <sup>h</sup>	163	181	201	22h	Oy	2 <sup>h</sup>	4%	64	84	107	Tages- mittel	Max.	Min
	1.0	3.2	2.6	2.4	2.4	2.7	4.0	7.6	8.6	6.4	5.0	4.9	4.46	8.6	
1	5.6	5-7	6.1	6.5	6.5	8.2	9.3	10.3	9.8	5.6	8.0	7.2	7.05	10.4	
1	7.5	7.6	7.6	7.1	7.1	5.1	7.8	11.0	9.8	8.5	7.6 6.5	5.5	6.03	11.0	
	5.5	4.5	3.5 5.3	6,0	7.2	8.8	11.8	13.3	12.2	11.2	11.0	12.0	8.98	13.3	
Ś	12.1	11.3	11.1	11.1	11.2	12.3	13.8	13.1	11.8	11.1	10.3	9.4	11.55	13.8	
1	8.0	6.5	4.3	3.1	2.7	3.2	5.2 N.9	8.6	9.7	9.1	8.8	8.3	0.45	10.1	
	8.3	7-9	7.8	7.8	8.0	8.5		9.3	8.1	7.7	7-3	6.7	5.02	9.5	
1	6.5	4.3	5.2	5.0 4.6	5.6	6.6	5 1	8.3	7.1	4.2	4.9	4.3	4.55	8.3	
į			1			5.0									
	3.3	3.8	3.8	3.9	2.3	4.5	4.5 3.3	3.6	3.1	4.2	3.5	3.5	2.63	3.7	
1	1.5	1.6	2.2	2,2	2.3	3.2	4.8	5-3	5.0	4.9	5.0	4.9	3.58	5.3	
Į	4.5	4.5	4.4	4.4	4.5	4.2	3.6	3-5	2,6	2.0	1.4	1.3	3.41	4.6	
1	1.9	2.1	2.5	2.7	3.0	3.4	4-3	4 - 4	3.0	1.3	0.8	0.1	2.46	4-5	-
j	- 0.3	- 0.1	- 0.1	0.2	0.2	1.0	1.1	1.2	1.5	1.3	1.2	1.2	0.70	1.5	-
3	1.2	0.5	- 0.1	- 1.0	- 1.1	1.8	2.4	2.6	1.6	0.0	2.0	- 0.6	0.44	3.0	-
Ì	- 1.3	- 1.3	- 0.6	0.1	0.6	1.5	2.3	3.2	3.2	2.9	2.4	2.7	1.32	3.3	_
ì	2.7	2.9	3.8	4.7	5.3	6.3	7.0	7.9	7-5	6.7	6.1	5.6	5.54	7-9	
ı	5.0	5.4	4.6	3-4	2.9	3.8	5.4	6,8	6.0	4.5	3.3	2.4	4.46	6.8	
ł	2.2	2.3	2.3	2.5	2.8	3-3	4.4	5.6	4-3	3.6	2.7	1.9	3.16	5.6	
ı	1.7	1.9	1.6	1.6	1.5	3.2	1.6	2.4	2.3	4.7	1.3	3.8	1.67	2.4 5.5	
l	4.2	3.9	4.0	3-7	3.7	4.3	5.1	5.8	4.8	3-5	2.9	2.1	4.00	5.8	
ı	1.3	0.7	0.1	- 0.5	- 0.1	1.4	3.1	4.1	4.5	4.1	4.5	4.8	2.33	4.9	
ł	4.3	3.9	3.2	2.1	2.2	3.5	7.0	10.6	9.6	7-7	6.7	6.6	5.62	10.6	
1	6.7	4.9	3.8	3.4	2.9	4.3	5.6	6.7	5.4	3-3	2.1	1.0	4.19	6.7	
ł	1.4	1.3	0.7	0.9	0.8	0.9	1.3	1.2	1.3	1.4	1.9	1.6	1.46	2.2	
ļ							- 1				1				
1	3.80	3.52	3.36	3.20		4.16	5.28	6,20	5.75	4.83	4.27	3.91	4.30	6.44	1
-	12h	14	Rich	tung (i	R), Gest	chwindi 20h	gkeit (	G) des	Winde	s in 1 S	Sekunde i	in Meter	n St.	104	Ta
2	12h R G	H 14	Rich	tung (i	R), Gest	chwindi	gkeit (	G) des	Winde	s in 1 S	Sekunde	in Meter	8 <sup>1</sup> R G	Ioh R G	Ta mi
2	R G	H ENE	Rich G R	tung (i	R), Gest	chwindi	gkeit (	G) des	Winde	s in 1 S	Sekunde	in Meter	R G	R G	Ta m
-	R G ENE o	ENE ENE	Rich	tung (i	R), Gest	chwindi 20h R G	gkeit (	G) des	Winde	s in 1 S	Sekunde	in Metern	R G	R G	Ta m
-	ENE o. ENE o. SSW 2.	ENE ENE SSW SSW	Rich G R 0.5 ENI 0.5 ENI 2.8 SSV	6 G G G G G G G G G G G G G G G G G G G	R), Gest	Chwindi 20 <sup>k</sup> R G N 0.9 ESE 2.1	gkeit (	G) des	Winde  G R  1.2 A  3.0 KS  3.5 WS	s in 1 S	NNE 0.4 ENE 0.5 W 2.1 E 1.5	in Metern	8 NNW 0 SSW 1 SW 2	10h R G	Ta m
2	R G ENE o	ENE ENE SSW SSW	Rich G R 0.5 ENI 0.5 ENI 2.8 SSV	6 G G G G G G G G G G G G G G G G G G G	R), Gest	chwindi 20h R G	gkeit (  22 <sup>k</sup> R G  No. ESE 2. SSW 0.	G) des	Winde  G R  1.2 A  3.0 KS  3.5 WS	s in 1 S	NNE 0.4 ENE 0.5 W 2.1 E 1.5	in Metern	8 NNW 0 SSW 1 SW 2 SSW 1 SW 2 SSW 2	2 NNW 0. 3 SSW 3. 1 SSW 0. 1 ESE 1. 5 ESE 0.	Ta m
-	ENE o. ENE o. SSW 2.	ENE ENE SSW E ESE ESE	Rich  G R  0.5 ENI 0.5 ENI 2.8 SSV 0.5 SSV 0.5 SSV	tung (4 6 6 6 6 8 8 9 9 9 9 9 9 9 9 9 9 9 9 9	R), Gest 18k R G N 0.6 ENE 0.2 SSW 0.8 SSW 1.0 ESE 2.1	N 0.9 ESE 2.1 SSW 1.6 SSW 0.5 ESE 2.1	R O  No. ESE 2. SSW 1. SSW 0. B 1. WSW 2.	G) des	Winde:  G R  1.2 M 3.0 KS 3.5 WS 1.1 EM 2.7 ES	E 1.6 E 2.6 E 2.6 E 2.6 E 2.6 E 3.0	Sekunde R G NNE 0.4 ENE 0.5 W 2.1 E 1.5 ESE 2.9 W 1.8	in Metern  6b R G  NNW o. S o. W 3. SSE 1. ESE 2.	8 NNW 0 7 SSW 1 1 SSE 1 0 E 1 4 WNW 3	2 NNW 0. 3 SSW 3. 1 SSW 0. 1 ESE 1. 5 ESE 0.	Ta m
-	ENE 0 SSW 2 SW 1 ENE 2	ENE ENE ENE SSW SSW E	Rich  G R  0.5 ENI 0.5 ENI 0.5 SSV 0.5 SSV 0.5 SSV 0.5 SSV 0.5 SSV 0.6 SSV 0.7 SSV	60 G G G G G G G G G G G G G G G G G G G	R), Gest  18t R G  N 0.6 ENE 0.2 SSW 0.8 (SW 1.0 ESE 2.1 (SW 1.5	No.9 E G No.9 ESE 2.1 SSW 1.6 SSW 0.5 ESE 2.1 No.8 SW 0.5	gkeit (  22b R O  No. ESE 2. SSW 1. SSW 0. E 1. WSW 2. SSW 2.	G) des	Winde  G R  1.2 M 3.0 ES 3.5 WS 1.1 EN 2.7 ES 1.1 WS 1.1 WS 1.1 WS 0.8 SS'	E 1.6 E 2.6 E 2.6 E 2.4 E 3.0	NNE 0.4 ENE 0.5 W 2.1 E 1.5 ESE 2.9 W 1.8 ENE 1.7	in Metern  66 R G  NNW 0, S 0, W 3- SSE 1, ESE 2, WNW 3- ENE 0,	8 NNW 0 7 SSW 1 1 SW 2 3 ESE 1 4 WNW 3 8 ENE 2	10h R G 2 NNW 0. 3 SSW 3. 1 SSW 0. 1 ESE 1 5 ESE 0. 6 WNW 2.	Ta m
The second secon	12h R G ENE 0 SSW 2 SW 1 ENE 2 ESE 2 ESE 2	ENE ENE SSW SSW E	Rich  6 R  0.5 EN  0.5 EN  0.5 SSV  1.8 SSV  0.5 SSV  0.9 NN	tung (1 6 6 6 8 8 8 9 9 9 9 9 9 9 9 9 9 9 9 9	R), Gesel 18 <sup>h</sup> R G N 0.6 ENE 0.2 SSW 0.8 SSW 1.0 ESE 2.1 SSW 1.5 SSW 1.5	N 0.9 ESE 2.1 SSW 1.6 SSW 0.5 ESE 2.1 N 0.8 SW 0.5	gkeit (  22 <sup>k</sup> R G  N o. ESE 2. SSW o. E 1. WSW 2. SSW O. SW O. SW O.	G) des  R  SE SE SWSW  G ESE 2 NNE 2 NNE 5 NNE	Winde  G R  1.2 3.0 88 3.5 WS 1.1 EN 2.7 ES 1.1 WN 0.8 8S	s in 1 S G E 1.6 E 2.6 W 3.6 E 2.4 E 3.0 W 0.9 W 0.9 W 0.7	R G NNE 0.4 ENE 0.5 W 2.1.1 E 1.5 ESE 2.9 W 1.8 ENE 1.7 W 2.8	in Metern  Ob R G  NNW o. S o. W 3-SSE 1. ESE 2. WNW 3-ENE 0. WSW 1.	8 NNW 0 SSW 1 SW 2 SW 1 SW 2 SW 1 SW 2 SW 2 SW	10 <sup>h</sup> R G 2 NNW 0. 3 SSW 3. 1 SSW 0. 1 ESE 1. 5 ESE 0. 6 WNW 2. 1 ESE 1. 2 SW 0.	Ta m
The same of the last of the la	12h R G ENE 0 SSW 2 SW 1 ENE 2 ESE 2 ESE 2	ENE ENE SSW SSW E	Rich  G R  0.5 EN  0.5 EN  0.5 EN  0.5 SSV  1.8 V  0.5 SSV  0.4 V  0.9 NN	E 0.2 E 0.3 E 0.3 S V 0.1 S V 0.1 S V 0.8 W 0.8 W 1.8 S V 0.8 W 1.8 S V 0.8 W 1.8 S V 0.8 W 1.1 S V 0.1 S	R), Gest 18 <sup>h</sup> R G N 0.6 ENE 0.2 SSW 0.8 SSW 1.0 ESE 2.1 SSW 1.5 (SW 1.0 NNE 0.4 N 1.0	20h K G N 0.9 ESE 2.1 SSW 1.6 SSW 0.5 ESE 2.1 N 0.8 SW 0.5 NE 0.4	gkeit (  22b R G  N o. ESE 2. SSW 1. SSW o. E 1. WSW 2. SSW o. NW O. NAE 4.	G) des  O R  S SE S WSW 6 ESE 2 NNE 7 SW 5 WSW 1 NNE	Winde  G R  1.2 A   3.0 BS 3.5 WS 1.1 EA   2.7 ES 1.4 WN 0.8 SS 3.0 WS	E 1.6 E 2.6 E 2.6 E 2.4 E 3.0 W 0.9 W 0.7 W 0.7 W 2.7	Sekunde :  #	66 R G  NNW 0. S 0. W 3. SSE 1. ESE 2. WNW 3. ENE 0. WSW 1. N 1.	8 NNW 0 7 SSW 1 1 SW 2 3 ESE 1 0 E 1 4 WAW 3 8 ENE 2 6 WSW 2 7 NAW 3	10h R G 3 SSW 3 3 SSW 0 1 SSW 0 1 ESE 1 8 ESE 0 6 WNW 2 4 ESE 1 2 SW 0 6 WNW 3	T: m
The same of the sa	R G  ENE 0 ENE 0 SW 1 ENE 2 ENE 2 ESE 2 O E 2 WNW 4	ENE ENE SSW SSW E ESE W N W N W N W N W N W N W N W N W N W	Rich  G R  0.5 ENI 0.5 ENI 2.8 SSV 0.5 SSV 1.8 SV 0.9 NNI 2.7 V 2.7 V	6 G E 0.2 E 0.3 E 0.3 S V 0.1 S E 2.7 I V 1.8 W V 1.8	R), Gess R G N 0.6 ENE 0.2 SSW 0.8 SSW 1.0 ESE 2.1 SSW 1.0 ESE 2.1 SSW 1.0 N 0.4 N 3.9 N 3.1	20h R G SW 0.5 ESE 2.1 NO.8 SW 0.5 NNE 0.4 N 3.5 WNW 4.4	22b   R   G     N   0.     ESE   2.     SSW   0.     SSW   0.     SSW   0.     N   0.     MAR   4.     WNW   3.	G) des    R	Winde  G R  1.2 A   3.0 BS 3.5 WS 1.1 EA   2.7 ES 1.4 WN 0.8 SS 3.0 WS 4.8 NA 4.8 NA	E 1.6 E 2.6 W 2.6 E 2.4 E 3.0 W 0.9 W 0.7 W 0.7 W 2.7 W 5.0	Sekunde :  #	66 R G  NNW 0. S 0. W 3- SSE 1. ESE 2. WNW 3- ENE 0. WSW 1. N 1. WNW 4-	8 NNW 0 7 SSW 1 1 SW 2 3 ESE 1 0 E 1 4 WNW 3 8 ENE 2 6 WSW 2 7 NNW 3 0 WNW 4	10 <sup>h</sup> R G 2 NNW 0 3 SSW 3 3 SSW 3 1 ESE 1 6 WNW 2 1 ESE 2 5 W 0 6 WNW 3 5 W 2	3 0 5 4 6 5 5 6 6
The same of the sa	12h   R   G	ENE ENE SSW E E W N N W NW S S W NW S S W NW S S W N W N	Rich  G R  0.5 EN  0.5 EN  0.5 SSV  1.8  0.4 NN  0.9 NN  0.9 V  2.7 V  2.0 V  0.0 SSV	66 G E 0.2 E 0.3 E 0.3 S V 0.3 S V 0.1 S V 0.1 S V 0.1 S V 0.4 S V 0.8 W V 0.8	R), Gest R G N 0.6 ENE 0.2 SSW 0.8 SSW 1.0 ESE 2.1 SSW 1.5 SW 1.5 SW 1.5 SW 3.1 W 3.1 W 3.1 SSE 0.2	20h K G SSW 1.6 SSW 1.5 SSW 1.5 SSW 2.5 ESE 2.1 No.8 SW 0.5 SSW 0.5 SSW 0.5 SSW 0.5 WNW 4.4 WNW 1.9 ESE 1.1	gkeit (  22b R G  N 0, ESE 2, SSW 1, SSW 0, SSW 1,	G) des  R  S SE  WSW  6 ESE 2 NXE 7 SW NNE 5 WSW 1 NNE 5 WNW	Winde  G R  1.2 M 3.0 ES 3.5 WS 1.1 EN 2.7 ES 1.1 WN 0.8 SS 3.0 WS 4.8 NA 4.0 WN 2.8 WN	S in 1 S  46  E 1.6  E 2.6  W 3.6  E 2.4  E 3.0  W 0.7  W 2.7  E 2.9  W 5.0  V 5.1.4	R G  NNE 0.4 ENE 0.5 W 2.1 E 1.5 ESE 2.9 W 1.8 E NE 1.7 W 2.8 E 1.0 VNW 4.6 NSW 2.1 SSW 2.1	in Metern  6	8 NAW 0 87 SSW 1 1 SW 2 3 ESE 1 0 E 1 4 WAW 3 8 EAE 2 6 WSW 2 7 NAW 3 0 WAW 4 9 SW 1 5 SW 0	10 <sup>h</sup>   R   G   C   NNW 0   C   SSW 3   1   SSW 6   1   5   E   E   1   1   E   E   1   1   E   E	Ta m
The same of the sa	12h   R   G	ENE ENE SSW E E ESE W N W NW S W NW S S S S S S S S S S S S	Rich  G R  0.5 EN  0.5 EN  0.5 SSV  0.5 SSV  0.5 SSV  0.7 NN  0.9 NN  0.9 V  2.7 V  0.0 ES	tung (4 6 6 6 6 8 8 8 8 9 9 9 9 9 9 9 9 9 9 9 9 9	R), Gescond 18 <sup>th</sup> R G N 0.6 ENE 0.2 SSW 0.8 SSW 1.0 ESE 2.1 SSW 1.5 (SW 1.0 NNE 0.4 N 3.9 W 3.1 W 2.1 SSE 0.7 E 1.2 E 1.2	20h R G N 0.9 ESE 2.1 SSW 1.6 SSW 0.5 ESE 2.1 N 0.8 SW 0.5 NNE 0.4 WNW 4.4 WNW 4.4	226   R   O     N   O     ESE   2     SSW   O     SSW   O     NAE   4     WNW   3     SSW   1     ESE   2	G) des  R  S NS SE S WSW	Winde  G R  1.2 A 3.0 ES 3.5 WS 1.1 EA 2.7 ES 1.1 WN 0.8 SS 3.0 WS 4.8 NA 4.8 NA 4.8 WN 2.8 WN 1.3 3.0 S	s in 1 S  2b  46  E 1.6  E 2.6  W 3.6  E 2.4  W 0.9  W 0.7  W 2.7  E 2.7  W 5.0  W 1.5  S 1.4	8	6 R G  NNW 0, S 0, W 3, SSE 1, ESE 2, WNW 1, N 1, WNW 4, WSW 0, SSW 0, ESE 1, ESE 2,	8 NNW 0 0 7 SSW 1 1 SW 2 3 SSE 1 1 6 E 1 4 WAW 3 8 EAR 2 7 NNW 3 0 WAW 4 9 SW 1 5 SW 0 2 ESE 1 1 SSW 0 2 ESE 1 SSW	10 <sup>h</sup> R G 2 NNW 0.3 SSW 3.1 SSW 0.1 ESE 1.5 ESE 0.6 WNW 2.2 SW 0.6 WNW 3.5 W 2.5 SSW 0.2 SSW 0	Ta m
	12h   R   G	ENE ENE SSW E ESE WNW WNW SSW WNW SSW E SSW WNW SSW WNW SS SSW E ESE ESE WNW WNW SS SSW E E ESE WNW WNW SS SSW E E E	Rich  G R  0.5 ENI 0.5 ENI 0.5 SSV 0.5 SSV 0.6 SSV 0.9 NN 0.9 NN 0.9 NS 0.6 SSI	tung (4 6 6 E 0.2 E 0.3 E 0.3 S V 0.1 S V 0.1 S V 0.8 V 1.8 S V 0.8 N V 1.8 S V 0.8 S V 0	R), Gess 18 <sup>h</sup> R G N 0.6 ENE 0.2 SSW 0.8 SSW 1.0 ESE 2.1 SSW 1.5 SSW 1.5 SSW 1.5 SSW 1.5 SSW 1.5 SSW 2.1 SSE 0.7 E 1.2 N 0.6	No.9 SSW 1.6 SSW 1.6 SSW 0.5 SSW 0.5 SW 0.5	gkeit (  22k R G  N 0, ESE 2, SSW 1, SSW 0, E 1, WSW 2, SSW 0, NAE 4, WNW 3, W 2, SSW 1, ESE 2, NAE 2, NAE 2, NAE 2, NAE 3, W 2, SSW 1, ESE 2, NAE 2, NAE 3, NAE 3, NAE 4, NAE 3,	G) des  R  S N S SE S WS W 6 ESE 2 NNE 7 SWS 1 NNE 8 WNW 0 WNW 0 SSE 2 E	Winde  G R  1.2 AS 3.0 KS 3.5 WS 1.1 EA 2.7 ES 4.1 WN 0.8 SS' 3.0 WS 4.0 WN 2.8 WN 1.3 3.0 S	S in 1 S  25  45  E 1.6  E 2.6  E 2.6  E 2.4  E 3.0  W 0.7  W 2.7  E 5.0  W 1.5  V 5.0  W 1.5  V 5.1  E 1.4  E 2.0  N 3.4	R G NNE 0.4 ENE 0.5 W 2.1 E 1.5 ESE 2.9 W 1.8 E 1.0 W 2.8 W 2.8 W 2.8 W 2.8 W 3.8 W 4.0 W 3.8 W 4.0 W 3.8 W 5.8 W	in Metern  66  R G  NNW 0.  S 0.  W 3.  SSE 1.  ESE 2.  WNW 3.  ENE 0.  WSW 1.  N 1.  WSW 0.  SSW 0.  ESE 1.	8 NAW 0 7 SSW 1 1 SW 2 2 3 ESE 1 0 WAW 3 8 EAE 2 6 WAW 3 7 NAW 3 6 WAW 4 9 SW 1 5 SW 0 7 ESE 1 1 SW 0 7 ESE 1 0 N 5 SW 0 7 ESE 1 0 N 5 SW	10 <sup>h</sup> R G 2 NNW 0.3 SSW 3.1 SSW 0.1 ESE 1.8 ESE 0.6 WNW 2.1 ESE 1.2 SW 0.6 WNW 3.5 W 2.2 SSW 0.2 SSW 0.0 ESE 1.3 NNW 5.3 NNW 5	Ta m
	12h   R   G	ENE ENE SSW SSW WNW WNW SSW WNW SSW WNW SSW WNW SSW WNW SSSW WNW S	Rich  G R  0.5 EN0.3  0.5 EN0.3  0.5 SSV  1.8 SV  1.8	E 0.2 E 0.3 E 0.3 E 0.3 F 0.3	R), Gescond R), Ge	20b R G N 0.9 ESE 2.1 SSW 0.5 SSW 0.5 SSW 0.5 N NE 0.4 N 3.5 WNW 4.9 ESE 1.1 E 1.6 WNW 1.9 ESE 1.5 WNW 3.5	gkeit (  22b R G  N 0, ESE 2, SSW 1, SSW 0, SSW 0, NAE 4, WNW 3, W 2, SSW 1, ESE 2, AME 2, WNW 4,	G) des  R  S	Winde  G R  1.2 85 3.0 85 3.5 WS 1.1 EA 2.7 ES 3.0 WS 4.0 WA	S in 1 S  25  46  E 2.6  W 0.9  W 0.7  W 2.7  W 2.7  W 5.5  V W 1.5  S 1.4  W 3.5	R G  NNE 0.4 ENE 0.5 W 2.1 E 1.5 ESE 2.9 W 1.8 E 1.0 WNSW 1.0 SSW 2.1 ESE 2.2 N 3.4 NW 2.9	NXW 0, S 0, W 3, SSE 1, ESE 2, WSW 1, N 1, WSW 0, ESE 1, N 1,	8 NAW 0 7 SSW 1 1 SW 2 1 SW 2 1 SW 2 0 W 1 8 ENE 2 6 WSW 2 7 NAW 3 8 ENE 2 6 WSW 2 7 NAW 4 9 SW 1 5 SW 0 7 ESE 1 9 N 5 5 NAE 0	10 <sup>k</sup> R G 2 MW 0 3 SSW 3 1 SSW 0 1 ESE 1 SE 1 SE 1 SE 1 SE 1 SE 1 SE 1 S	Ta m
	12h   R   G	ENE ENE SSW E E ESE WNW SSW E E ESE WNW SSW WNW SS SSW WNW SS SSW WNW SS SSW WNW WN	Rich  G R  0.5 ENI 2.8 SSV 1.8 SV 0.9 NNI 0.9 NNI 0.9 SV 1.0 KS 1.0 KS 1.0 NNI 0.2 NNI 0.3 NNI 0.3 NNI 0.4 NNI 0.4 NNI 0.5 NNI	tung (1 6 G E 0.2 E 0.3 S E 0.3 S V 0.3 S V 0.8 W V 0.8 W	R), Gesell R G N 0.6 ENE 0.2 SSW 1.0 ESE 2.1 SSW 1.5 CSW 1.0 VNE 0.4 N 3.1 W 2.1 W 2.1 W 2.1 NSE 0.7 E 1.2 NE 1.4 W 5.1 NNE 2.0	20b R G N 0.9 ESE 2.1 SSW 0.5 SSW 0.5 SSW 0.5 NNE 0.4 NN 0.5 NNE 0.4 NN 0.5 NNE 0.4 NN 0.5 NN 0.5	gkeit (  22b R G  N 0. ESE 2. SSW 1. SSW 0. NW 0. AAE 4. WNW 3. W 2. SSW 1. ESE 2. AME 2. WNW 4. NNE 1.	G) des  R  S	Winde  G R  1.2 M 3.0 BS 3.5 WS 1.1 EN 2.7 ES 1.1 WN 0.8 SS 4.8 NA 4.0 WN 2.8 WN 1.3 3.0 WS 4.0 WN 2.8 WN 1.3 3.0 WS	S in 1 S  24  45  E 1.6  E 2.4  E 3.6  E 2.4  E 3.0  W 0.7  W 2.7  W 5.0  W 1.5  V 3.4  W 5.6  E 2.4	R G  NNE 0.4 ENE 0.5 W 2.1 E 1.5 ESE 2.9 W 1.8 ENE 1.7 W 2.8 ENE 1.7 W 2.9 N 3.4 NW 2.9 NWE 2.6	in Meters  6 R G  NNW 0,  8 0,  W 3,  SSE 1,  ESE 2,  WNW 3,  ENE 0,  WSW 1,  WNW 4,  WSW 0,  SNW 0,  ESE 1,  N 4,  NNW 2,  N 1,	R G  R NNW o  S NNW o  S SW 1  S W 2  S SW 1  S W 2  S EXE 2  W NW 3  W NW 4  S W 0  S W 1  S W 0  S EXE 2  NNW 5  W NW 4  S W 0  S W 1  S W 0	10 <sup>k</sup> R G 2 MW 0 3 SSW 3 1 SSW 0 1 ESE 1 SSE 1 6 WW 2 2 SW 0 0 SSW 0 2 SSW 0 0 ESE 1 3 NW 5 5 6 WW 3 0 GW W 3	Ta m
	12h   R   G	ENE ENE SSW E ESE WNW SSW E ESE WNW SSW WNW SSW WNW SSW WNW WNW WNW WNW	Rich  G R  0.5 ENI 0.5 ENI 0.5 ENI 0.5 SSV 0.5 SSV 0.6 V 0.9 NN 0	E 0.2 E 0.3 E 0.3 S V 0.3 S V 0.3 S V 0.3 S V 0.4 I V 2.9 E 0.6 E 2.0 V 4.1 E 0.4 F V 2.9 E 0.4 F V	R), Geseller R G N 0.6 ENE 0.2 SNW 0.8 SNW 1.0 ESE 2.1 SNW 1.5 SNW 1.5 SNW 1.5 SNW 1.5 SNW 2.1 W 2.1 W 2.1 NNE 0.2 NNE 0.4 W 1.0 SNW 0.8	20b R G SSW 1.6 SSW 1.6 SSW 0.5 SSW 0.5 SW 0.5 NNE 0.4 WNW 4.4 WNW 4.4 WNW 1.3 SW 1.6 NNE 0.5 NNE 0.5	22 <sup>b</sup>   R G     N 0.     ESE 2.     SSW 0.     E 1.     SSW 0.     N 8W 2.     SSW 0.     SW 0.     SW 0.     SW 0.     SW 0.     SW 0.     N 0.     SW 0.     N 0.     SW 0.     SSW 1.     ESE 2.     SSW 1.     ESE 2.     SSW 1.     ESE 2.     SSW 1.     SSW 1.     SSW 2.     SSW 3.     SSW 1.     SSW 5.     SSW 5.	G) des  R 5	Winde  G R  1.7 3.0 85 3.5 WS 1.1 EN 2.7 ES 1.1 WN 0.8 SS' 3.0 WS 4.8 NA 4.0 WN 1.3 3.0 WS 3.0 WS 2.8 WN 1.3 3.0 WS 3.0 WN 2.9 WN 2.9 WN 2.9 WN 2.9 WN 2.9 WN	S in 1 S  26  18 1.6  18 2.6  18 2.4  18 2.4  18 2.4  18 2.4  18 2.4  18 2.7	R G  NNE 0.4 ENE 0.5 W 2.1 E 1.5 ESE 2.9 W 1.8 ENE 1.7 W 2.8 E 1.0 V 3.4 NW 2.9 NNE 2.5 ENE 2.7 NNE 2.8 ENE 2.7 NNE 2.8 ENE 2.7 NNE 2.8 ENE 2.7	Metern	8 NNW 0 7 SSW 1 1 SW 2 2 3 ESE 1 0 E 1 4 WAW 3 8 ENE 2 6 WSW 2 7 NAW 3 0 WSW 4 4 9 SW 1 5 SW 0 7 ESE 1 9 N 5 SNE 0 4 NAW 1 1 W 2 5 SE 2 SE 2 SE 2 SE 2 SE 2	10 <sup>h</sup> R G   2 NNW 0 3 SSW 3 1 SSW 0 1 ESE 1 2 SW 0 6 WNW 2 5 SSW 0 ESE 1 3 NNW 5 5 W 2 5 SSW 0 ESE 1 3 NNW 5 5 SSW 0 ESE 1 5 SSW 0 ESE 2 9 WNW 2 9 ESE 2 9 WNW 2 5 SSW 0 5 S	Ta m 3 4 6 6 5 5 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6
	12h   R   G	ENE ENE ENE SSW SSW E ENE SSW WNW WNW WNW WNW WNW WNW WNW WNW WNW	Rich  G R  0.5 EN  0.5 EN  0.5 EN  0.5 SSV  0.6 SSV  0.7 NN  0.9 V  2.0 SSI  0.6 ESI  1.0 NN  2.4 WNV  1.5 WNV  1.5 WNV  1.5 WNV  1.5 WNV	6 G E 0.2 E 0.3 S E 0.3 S E 0.3 S V 0.1 S E 2.7 S V 1.8 W V 1.8 W V 1.8 W V 1.9 E 1.1 E 0.6 V V 1.1 S E 0.4 M	18 <sup>1</sup> R G No.6 ENE 0.2 SSW 0.2 SSW 1.0 ENE 0.2 SSW 1.0 ENE 2.1 N 3.9 W 3.1 W 2.1 W 2.1 W 5.1 NNE 2.0 W 1.0 SSE 0.7 E 1.2 W 5.1 NNE 2.0 W 1.0 SSW 1.6 ENE 0.2 ENE 0.2 E	20h R G No.9 R SE 2:1.1 SSW 1.6 SSW 0.5 ESE 2:1.1 NO.3 SSW 0.5 NNE 0.4 N 3.5 NNE 0.4 WNW 1.9 ESE 1.6 WNW 3.6 NNE 1.5 WNW 3.6 NNE 1.5 WNW 3.6 NNE 1.5 WNW 3.6 NNE 1.5 WNW 3.6 NNE 1.6 ESE 1.6 R S.6 WNW 3.6 NNE 1.6 ESE 1.6 R S.6 WNW 3.6 ESE 1.6 ESE 1	22b   R   G     N   0, ESE   2, SSW   1, SSW   0, SSW   0, SSW   0, SSW   0, SSW   1, ESE   2, WNW   3, W   2, SSW   1, ESE   2, WNW   4, WNW   2, SSW   1, ESE   2, SSW   1	6) des  R  S  S  S  S  S  S  S  S  S  S  S  S	Winde  G R  1.2 AS 3.0 KS 3.5 KS 3.5 KS 3.6 KS 3.0	S in 1 S  2 b  G	R G R G R G R G R G R G R G R G R G R G	0 Metern	R G  R G  S NNW o  7 SSW 11  1 SW 2  3 ESE 1  6 1  4 WAW 3  8 EAR 2  6 WSW 2  7 NNW 3  0 WNW 4  9 SW 1  5 SW 0  7 ESE 1  9 N5  5 NNE 0  4 NNW 1  1 W 2  5 SE 2  6 ESE 2  6 ESE 2  6 ESE 2  6 ESE 3	10 <sup>h</sup>   R   G   S   S   W   3   S   W   3   S   W   3   S   W   0   C   S   W   2   S   W   0   S   W   2   S   W   0   S   W   2   S   W   0   S   S   W   0   S   S   W   0   S   S   W   0   S   S   W   0   S   S   W   0   S   S   W   0   S   S   W   0   S   S   W   0   S   S   W   0   S   S   W   0   S   S   W   0   S   S   W   0   S   S   W   0   S   S   S   W   0   S   S   S   W   0   S   S   S   W   0   S   S   S   S   W   0   S   S   S   S   S   S   S   S   S	Ta m 3 4 4 6 3 5 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6
	12h   R   G	ENE ENE SSW SSW E ESE W N W N W N W N W N W N W N W N W N W	Rich  G R  0.5 EN  0.5 SN  0.5 SSV  0.5 SSV  0.5 SSV  0.9 NN  0.9 NN  1.0 N  2.0 SSV  2.1 N  3.0 WN  3.1 SWN  3	6 G E 0.2 E 0.3 S V 0.1 S E 2.7 S V 1.8 W V 1.8 W V 1.8 W V 1.8 W V 1.9 E 0.6	18 <sup>1</sup> R G N	Chwindi  20b  R G  N 0.9  ESE 2.1  SSW 1.6  SSW 0.5  SSW 0.5  SW 0.5  NNE 0.4  NNW 1.9  ESE 1.1  E 1.6  NNE 1.5  NNE 0.5	22b   R   G     N   0.     ESE 2.     SSW 0.     SSW 1.     ESE 2.     SSW 2.     SSW 2.     SSW 2.     SSW 2.     SSW 2.     SSW 3.     SSW 3.     SSW 4.     SSW 4.     SSW 4.     SSW 5.     SSW 5.     SSW 5.     SSW 6.     SSW 6.     SSW 7.     SSW 8.     SSW 9.     SSW	6) des    R	Winde  G R  1.2 A 3.0 KS 3.5 WS 1.1 EA 2.7 ES 1.1 WS 0.8 SA 4.8 WA 4.0 WA 2.8 WA 1.3 A 3.0 WS 2.4 ES 2.4 ES	E 1.6 EE 2.6 EE 3.4 EE 3.4 EE 3.0 WE 2.7 W 5.0 W 5.0 W 5.1 W 5.0 W 5.0 W 6.1 W	R G  R G  NNE 0.4 ENE 0.5 W 2.11 E 1.5 ESE 2.9 W 1.8 ENE 1.7 W 2.8 ENE 1.7 W 2.8 ENE 1.7 W 2.8 ENE 1.7 W 3.8 ENE 2.1 E 1.0 WSW 1.0 SSW 2.1 ESE 2.2 N 3.4 NW 2.9 NSE 2.5 ENE 2.1 ENE 2.1 ENE 2.1 ENE 2.1 ENE 2.1 ENE 2.1 ENE 3.2 W 1.3	66 R G NNW 0. S 0.	R G   R   R   G   R   R   G   R   R	10 <sup>h</sup>   R   G   SSW 3   3   SSW 3   1   SSW 0   1   ESE 1   5   ESE 0   0   SSW 0   2   SSW 0   0   ESE 1   3   SSW 0   0   ESE 1   3   SSW 0   0   ESE 1   3   SSW 0   0   ESE 2   5   SSW 0   0   ESE 2   SSW 0   SSW	Ta m 3 0 1 4 4 5 5 5 6 6 0 0 0 5 5 6 0 0 1 7 7 1 5 5
	BY B	ENE	Rich  G R  O.5 ENI C.5 SSV O.5 SSV O.5 SSV O.9 NN O.6 SSI O.6 SSI O.6 SSV O.9 NN O.6 SSI O.7 V O.6 SSI O.6 SSI O.7 V O.6 SSI O.6 SSI O.7 V O.7 V O.7 V O.8 V O.8 V O.9 V O.8 V O.9	6 G G G G G G G G G G G G G G G G G G G	18 <sup>k</sup> R G ENE 0.25 SW 0.8 SW 1.0 SW 1.0 SW 1.0 SW 1.0 SW 1.0 W 2.1 SSE 0.7 E 1.2 W 2.1 SSE 0.5 W 1.0 SSE 0.5 W 1.0 SSE 3.2 SW 1.6 SW 1.6 SSE 3.2 SW 1.6 SW 1.6 S	20h R G No.98 SSE 2.1. No.8 SSW 0.5 SSE 2.1 No.8 SSW 0.6 No.8 SSW 0.5 WNW 4.4 WNW 1.9 EXE 1.1 No.2 SSW 0.9 WNW 3.6 No.2 SSW 0.9 WSW 1.6 WSW 1.6 WSW 4.4 WSW 4.	gkeit (  22b R O No. ESE 2. SSW 1. SSW 0. SSW 0. AAE 4. WNW 3. W 2. SSW 1. ESE 2. ANE 2. WNW 4. NNE 1. WNW 2. SSW 1. ESE 2. SSW 3. SSW 0. SSW 1. ESE 2. SSW 3. SSW 3. SSW 3. SSW 3. SSW 3. SSW 4.	R   SEE	Winde  G R  1.2 A 3.0 BS 3.5 WS 1.1 EA 2.7 ES 1.1 WN 0.8 SS 4.8 NA 4.0 WN 2.8 WN 1.3 S 3.0 WS 4.0 WN 2.9 WN 2.9 WN 2.9 WN 2.9 WN 2.9 WN 3.0 NN 2.9 WN 3.0 NN	E 1.6 E 2.6 E 3.6 W 3.5 W 4.5 W 4.5 W 3.5 E 2.6 E 3.0 W 3.5 E 2.6 E 3.0 W 3.5 E 2.6 E 3.0 W 3.5 E 2.6 E 2.8 W 3.5	Sekunde :  4	ob R G  NXW 0. 8 0. W 3. SSE 1. ESE 2. ENE 0. SWW 1. N 1.	R G  NNW 0  S NNW 0  S SW 1  S W 2  S SW 2  S SW 3  E E 1  WAW 3  S E NE 2  NNW 4  S W 1  S W 0  N N W 4  N N W 1  W W 2  S E NE 3  N N W 1  W E NE 1  E	10 <sup>8</sup>   R   G   G   S   W   M   W   G   S   W   G   G   W   W   Z   S   W   G   G   W   W   Z   S   W   G   G   G   W   W   Z   S   W   G   G   G   W   W   Z   S   W   G   G   G   G   G   W   W   G   G	Ta m: 3 0 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1
	12h   R   G	ENE ENE SSW SSW SSW SSW SSW SSW SSW SSW SSW SS	Rich  G R  O.5 ENI O.5 ENI O.5 SSV O.5 SSV O.9 NN O	6 G  6 G  E 0.2 E 0.3 E V 0.3 S V 0.1	R), Gest R G N 0.6 ENE 0.2 SSW 0.8 SSW 1.0 ESE 2.1 SSW 1.0 W 3.1 W 2.1 SSE 0.7 E 1.2 NE 1.4 W 5.1 NNE 2.0 W 1.0 SSW 1.0 S	Chwindi  20b  R 0  SSE 2:1  SSW 1.6  SSW 0.5  SSW 0.5  SW 0.5  SW 0.5  NNE 0.4  WNW 1.9  EXE 1:1  E 1.6  NNE 0.9  WNW 1.3  SSW 1.3  SSW 1.3  SSW 1.4  WNW 4.4  WNW 4.4  WNW 5.5  NNE 0.5  SSW 1.6  SSW 1.	gkeit (  22b R O No. ESE 2. SSW 1. SSW 0. SSW 0. AAE 4. WNW 3. W 2. SSW 1. ESE 2. ANE 2. WNW 4. NNE 1. WNW 2. SSW 1. ESE 2. SSW 3. SSW 0. SSW 1. ESE 2. SSW 3. SSW 3. SSW 3. SSW 3. SSW 3. SSW 4.	R   SEE	Winde  G R  1.2 A 3.0 BS 3.5 WS 1.1 EA 2.7 ES 1.1 WN 0.8 SS 4.8 NA 4.0 WN 2.8 WN 1.3 S 3.0 WS 4.0 WN 2.9 WN 2.9 WN 2.9 WN 2.9 WN 2.9 WN 3.0 NN 2.9 WN 3.0 NN	E 1.6 E 2.6 E 3.6 W 3.5 W 4.5 W 4.5 W 3.5 E 2.6 E 3.0 W 3.5 E 2.6 E 3.0 W 3.5 E 2.6 E 3.0 W 3.5 E 2.6 E 2.8 W 3.5	4 G G G G G G G G G G G G G G G G G G G	ob R G S S S S S S S S S S S S S S S S S S	R G G NNW 6 NNW 1	10 <sup>h</sup>   R   G   S   W   W   W   W   W   W   W   W   W	Ta m 3 4 6 3 5 5 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6
	12h   R   G	ENE	Rich  67 R  0.5 ENI 0.5 ENI 0.5 SSV 0.4 SSV 0.4 SSV 0.4 SSV 0.4 SSV 0.6 SSV 0.6 SSV 0.6 SSV 0.6 SSV 0.7 SSV 0.8 SSV 0.8 SSV 0.9 NN 0.9 NN 0.1 SV 0.1 SSV 0.1 SSV 0.1 SSV 0.2 SSV 0.2 SSV 0.3 SSV 0.5 SSV 0.6 SSV 0.7 SSV 0.9 SSV	trong (4)  60 G  6	R), Gest  188  R G  N 0.6 ENE 0.2 SSW 0.8 SSW 1.0 SSW 1.0 VXE 0.4 N 3.1 W 2.1 VXE 0.4 W 5.1 W 5.1 W 5.1 SSE 0.7 E 1.2 VX 1.0 SSW 1.6 SSW 1.5 SSW 1.6 SSW 1.6 SSW 1.6 SSW 1.6 SSW 1.6 SSW 1.8 SSW 1.8 SSW 1.6	20% R G  N 0.9 ESE 2.1 SSW 1.6 SSW 0.5 ESE 2.1 SW 0.5 SW 0.5 NNE 0.5 NNE 0.5 NNE 1.9 ESE 1.6 NNE 1.5 WNW 1.3 SSW 1.3 S	gkeit (  22b R O No. ESE 2. SSW 1. SSW 0. SSW 0. AAE 4. WNW 3. W 2. SSW 1. ESE 2. ANE 2. WNW 4. NNE 1. WNW 2. SSW 1. ESE 2. SSW 3. SSW 0. SSW 1. ESE 2. SSW 3. SSW 3. SSW 3. SSW 3. SSW 3. SSW 4.	R   SEE	Winde  G R  1.2 A 3.0 BS 3.5 WS 1.1 EA 2.7 ES 1.1 WN 0.8 SS 4.8 NA 4.0 WN 2.8 WN 1.3 S 3.0 WS 4.0 WN 2.9 WN 2.9 WN 2.9 WN 2.9 WN 2.9 WN 3.0 NN 2.9 WN 3.0 NN	E 1.6 E 2.6 E 3.6 W 3.5 W 4.5 W 4.5 W 3.5 E 2.6 E 3.1 W 3.5 E 2.6 W 3.5 E 2.6 E 2.9 W 3.5 E 2.6 E 2.8 W 3.5 E 2.6 E 2.8 W 3.5 E 2.6 W 4.8 E 2.6 E 2.8	# G G G G G G G G G G G G G G G G G G G	on Metern  ob  R	8	10 <sup>8</sup> R G G S S W 3 S S W 3 S S W 3 S S W 3 S S W 3 S S W 3 S S W 3 S S W 5 S S W 5	Tame 3 4 6 5 5 6 6 0 0 0 5 5 0 0 0 1 1 77 1 5 5 2 0 0 1 1 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
	12h   R   G	ENE	Rich  G R  O.5 EN  O.5 EN  O.5 EN  O.5 SSV  O.6 SSI  O.6 SSV  O.6 SSI  O.6 SSI  O.6 SSV  O.6	trong (4)  60 G  6	R), Gest R G N 0.6 ENE 0.2 SSW 0.8 SSW 1.0 ESE 2.1 SSW 1.0 W 3.1 W 2.1 SSE 0.7 E 1.2 NE 1.4 W 5.1 NNE 2.0 W 1.0 SSW 1.0 S	200 N 0.9 ESE 2.1 N 0.8 SW 1.6 SSW 0.5 NNE 0.4 NNE 0.4 NNE 1.9 ESE 1.1 NNE 0.4 NNE 1.9 ESE 1.1 NNE 0.4 NNE 1.9 ESE 1.1 NNE 0.5	gkeit (  22b  R	5 NE SEE SEE SEE SEE SEE SEE SEE SEE SEE	Winde  G R  1.7 3 3.0 85 3.5 WS 1.1 E3 2.7 E5 1.1 E3 3.0 WN 1.3 3.0 WN 3	E 1.6 E 2.6 E 3.6 W 3.5 W 4.5 W 4.5 W 3.5 E 2.6 E 3.1 W 3.5 E 2.6 W 3.5 E 2.6 E 2.9 W 3.5 E 2.6 E 2.8 W 3.5 E 2.6 E 2.8 W 3.5 E 2.6 W 4.8 E 2.6 E 2.8	4 G G G G G G G G G G G G G G G G G G G	ob R G R G R W 0. S 0. W 3. SSE 1. ESE 2. WNW 3. ESE 2. WNW 4. WNW 4. WNW 4. NNW 2. NNW 2. WNW 2. ESE 1. N 1. WNW 2. ESE 2. ESE 2. ESE 2. ESE 2. ESE 2. W 0. ESE 1. WNW 0.	8	10 <sup>h</sup>   R G G   S W 3	Tam m 3 0 5 4 6 6 6 6 6 6 6 6 6 6 7 1 1 7 1 1 5 5 7 6 1 1 0 2 2
The state of the s	R G  ENE O., ENE O., SSW 1. ENE 2. WN 1. ENE 2. WN 4. W2. SSW 0. WN 3. WNW 3. WNW 3. WNW 3. WNW 3. WNW 3. WNW 3. SSW 1. SSW 3.	14'   E   E   E   E   E   E   E   E   E	Rich  6 R  8 R  0.5 ENIM  0.5 ENIM  0.5 SSW  1.8 SSW  0.5	66 6 8 0.2 8 0.3 8 8 0.3 8 8 2.7 1 8 2 2.7 1 8	R), Gest  R G  N 0.6  N 1.5  N	R G N 0.9 ESE 2.1 SW 0.5 ESE 2.1 SW 0.5 ESE 2.1 SW 0.5 NNE 0.4 WNW 1.9 ESE 1.1 NNE 0.5 WNW 1.3 SSW 1.6 WSW 1.0 SSW 2.7 W 2.5 SSW 1.6 SSW 2.5 S	22k   R   O   N   O   O   N   O   O   O   O   O	R	Winde  G R  1.2 5 5 3.5 WS 2.7 ES 1.1 EA 2.7 ES 4.8 MN 1.3 5 3.0 WS 4.8 MN 2.8 WN 2.8 WN 1.3 5 3.0 WS 4.8 MN 2.8 WN 2.8 WN 4.8 MN 4.8	E 1.6 (2.6 (2.6 (2.6 (2.6 (2.6 (2.6 (2.6 (2	R G  NNE 0.4 ENE 0.5 W 2.1 E 1.5 ESE 2.9 W 1.8 E 2.6 E 2.0 VNW 4.0 WSW 1.0 SSW 1.0 SSW 2.1 E 1.5 W 2.5 W 1.0 SSW 2.0	Metern	8	10 <sup>8</sup> R G G S S W 0 0 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	Ta m 30 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1
	12 <sup>k</sup> R G ENE 0. ENE 0. SSW 2. SW 1. SSW 2. SW 1. SSW 2. SW 1. SSW 0. E 1. ANM 5. SSW 0. SSW 1. SSW 2. SSW	14'   R     ENE     ENE     SSW     ESE     SSW     SW     N     N     N     WN     SSE	Rich  G R  R R  0.5 ENN  0.5 ENN  0.5 ENN  0.5 SSV  0.5 SSV  0.5 SSV  0.5 SSV  0.6 SSV  0.6 SSV  0.7 V  2.0 V  0.6 SSV  0.6 SSV  0.7 V  0.7 V  0.6 SSV  0.7 V  0.7 V  0.7 V  0.7 V  0.8 SV  0.8 SSV  0.9 SSV  0.9 SSV  0.9 SSV  0.6 SSV  0.7 V  0.7 V  0.7 V  0.7 V  0.8 SSV  0.8 SSV  0.9 SSV  0.6 SSV  0.7 V  0.7 V  0.7 V  0.7 SSV  0.7 SSV  0.7 SSV  0.7 SSV	tung (1 6 6 6 7 7 8 1 8 1 8 1 8 1 8 1 8 1 8 1 8 1 8 1	R), Gesch R G N 0.6 ENE 0.2 SSW 0.8 SSW 0.8 ENE 2.1 SSW 1.0 ENE 2.1 SSW 1.5 SSW 1.0 NNE 0.4 N 3.9 W 3.1 W 2.1 NNE 0.4 N 3.9 W 3.1 W 2.1 NNE 0.4 N 3.9 W 3.1 N 2.1 NNE 0.4 N 3.9 W 3.1 N 3.1 N 4.5 SSE 0.7 E 1.2 SSW 1.0 SSW 1.0 E 1.2 SSW 1.0 SSW 1.0 S	Chwindi  R 00  ESC 2.1  SSW 1.6  SSW 0.5  ESC 2.1  N 0.5  SSW 0.5  ESC 2.1  N 0.5  NNC 0.4  NNW 1.5  NNW 1.5  NNE 1.5  NNW 0.3  SSW 1.6  E 1.6  NNW 0.3  SSW 1.6  SSW 2.7  WSW 2.7  W 2.5  SSW 2.7	226   N	0 des	G R 1.2 5 3.0 8 8 3.5 WS 1.1 E 8 1.1 WN 0.8 8 5 3 0.0 WS 4.8 8 3.3 0.0 WS 4.0 0.0	E 1.6 E 2.6 E 3.0 O 10 0.7 E 2.7 E 3.0 O 10 0.7 W 2.7 W 2.7 W 2.7 W 3.0 W 3.7 W 3.7 W 3.7 W 4.8 W 4.8	R 67  NNE 0.4 ENE 0.5 W 2.1 E 1.5 ESE 2.9 W 1.8 EAL 1.7 W 2.8 E 1.0 O SSW 2.1 ESE 2.2 N 3.4 NW 2.1 ENE 2.2 W 1.3 ESE 2.2 W 1.3 ESE 2.1 ENE 2.1 SSW 2.5 SSW 2.0 SSW 2.0	Motorn   M	R G   R G	10 <sup>h</sup>   R   G   G   S   S   M   3   S	Ta m 3.0 th 4.6 5.5 th 6.0 th th
The state of the s	12 <sup>k</sup>   R   G	ENE   ENE   SSW   WNW   WNW   S	Rich  6 R  7 R  8 R  8 R  8 R  9 R  9 R  9 R  9 R  9	66 6 8 0.2 8 0.3 8 8 0.3 8 8 0.3 8 8 0.3 8 8 2.7 1 8 8 0.5 8 8 2.7 1 8 8 0.5 8	RD, Gesting RD, Ge	Chwindi  20h R G SW 0.9 ESE 2.1 SSW 0.5 ESE 2.1 SW 0.5 ESE 2.1 ESE 2.	22k   R   O   N   O   O   N   O   O   O   O   O	R   R   R   R   R   R   R   R   R   R	G R 1.2 A 3.0 KS 3.0 KS 1.1 EA 8 KN 1.1 EA	E1.6 (2.6 (2.6 (2.6 (2.6 (2.6 (2.6 (2.6 (2	NNE 0.4 NNE 0.	R 6 6 8 6 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8	8 NNW 0 0 7 SW 1 1 SW 3 SW 3	10h   R   G   G   G   G   G   G   G   G   G	Ta min a de la companya de la compan
	12 <sup>k</sup> R G ENE 0. ENE 0. SSW 2. SW 1. SSW 2. SW 1. SSW 2. SW 1. SSW 0. E 1. ANM 5. SSW 0. SSW 1. SSW 2. SSW	ENE ENE SSW E ESE SSW W E ESE	Rich Rich Rich Rich Rich Rich Rich Rich	66 6 8 0.2 E 0.2 8 0.3 S 8 0.3	RD, Gesting RD, Ge	Chwindi  R 00  ESC 2.1  SSW 1.6  SSW 0.5  ESC 2.1  N 0.5  SSW 0.5  ESC 2.1  N 0.5  NNC 0.4  NNW 1.5  NNW 1.5  NNE 1.5  NNW 0.3  SSW 1.6  E 1.6  NNW 0.3  SSW 1.6  SSW 2.7  WSW 2.7  W 2.5  SSW 2.7	Record   R	0   des     0	G R 1.2 A 3.0 KS 3.5 WS 1.1 B 2.5 W 1.3 A 0.0 W 1.3 A	E 1.6 E 2.6 E 3.0 O 10 0.7 E 2.7 E 3.0 O 10 0.7 W 2.7 W 2.7 W 2.7 W 3.0 W 3.7 W 3.7 W 3.7 W 4.8 W 4.8	R 67  NNE 0.4 ENE 0.5 W 2.1 E 1.5 ESE 2.9 W 1.8 EAL 1.7 W 2.8 E 1.0 O SSW 2.1 ESE 2.2 N 3.4 NW 2.1 ENE 2.2 W 1.3 ESE 2.2 W 1.3 ESE 2.1 ENE 2.1 SSW 2.5 SSW 2.0 SSW 2.0	Motors   M	8	10h   R   G   G   G   G   G   G   G   G   G	Ta m: 300.400 : 500.000 : 500.000 : 500.000

						DEZEMBEI	(				190
						ekte Ables	ingen				
_	Luft	druck a	uf o° redu	ziert in M	illim. =	700° +		Luf	ttemperati	or nach Celsiu	S
Tag	19 <sup>k</sup>		21	94		Tagesmittel	19		2 <sup>h</sup>	91	Tagesmitt
1	52.4		53.2	54.5	1	53-37	,		3.8	2.6	2.47
2	\$0.5		57.0	57.9	- 1	57.23		6	1.0	0.3	0.63
3	56.6 52.2		56.3	49.8	- 6	55.97	- 0	.3	- 0.1	2.7	2.97
5	48.7		45.5	45.1	- 1	48.43		.0	3.1	2.7	2.40
6	46.7		47.0	48.1		47.27		2	2.3	3.2	2.23
7	50.9		51.0	50.8	- 6	50.90		.0	10.1	5.1	3,90
	51.9	1	51.3	50.8		51.37	7	5 8		9.0	8.87
9	48.8 53.5	19	49.2	60.1	- 1	49.00 57.00	9	.8	7.1 5.4	3.4	7.80 3.93
11			57.2	64.8							2.80
12	62.5 64.3		64.1	61.5		63.80	- 1	.6	3.9	1.5	0.07
13	(8.4		54.1	52.1		54.87	0	9	3.4	2.8	2.37
14	50.0		50.8	52.8	- 1	51.20	4	.0	5.0	5.2	4.73
15	52.3	1	51.5	50.9	- 1	51.57		.8	7.2		6.00
16	49.5	- 1	47.0	46.9	- 1	48.10 52.13	5	1	5.6	- 0.7	5.17
17	55.3	1.4	52.5	53.9 56.3	1	55.31	- 2	.8	- 0.3	- 3.6	- 2.23
19	55.3	- 1	53.7	53.2	- 1	54.07	5	9	- 1.3	- 3.4	- 3.53
20	53.2		53.9	54.3	- 5	53.80	- 2		1.6	2.4	0.40
21	54.4		54.4	54.3	- 1	54.37		.6	3.6	3.1	3.10
22 23	53.6 52.5		55.6	53.1	- 1	53.27	3	9	5.8	4.8	4.60 5.30
24	54.3		55.9	56.4	8	55-53	3	4	2.8	2.7	2.97
25	55.0	- 1	53.4	51.5	ij	53.30		.2	1.9	0.9	1.67
26	49.4		49.1	49.1		49.20	0	.1	2.6	2.7	1.80
27 28	47.0 41.3		44.3	43.0 39.1		44.77		2	4.1 1.2	0.5	0.60
29	16.1	1	33.5	30.8		33.47	0	1	1.4	2.3	1.27
30	28.8			44.8	- 1	36.80	4	9	0.5	- 1.6 - 6.2	0.60
31 Mittel	53.6		55-7	57.4		55-57	- 4		- 3. i		- 4.50
antel	51.40										
	31.4	•	51.63	51.75		51.61	1	79	3.09	2.05	2.31
Tag			in Millin		1	51.61 Relative Fe				2.05 z u, Stärke d [Skala: 0 — 10	les Winde
					1					u. Starke d	les Winde
Tag	Dun 19h	stdruck 2h	in Millin	Tages- mittel	194	Relative Fe	uchtig 9 <sup>h</sup>	Tages- mittel	Richtung 19h	y u, Stärke d [Skala: 0 — 10	les Winde
Tag t	Dun 19h	2h 5-2 4.6	9h	Tages- mittel	19 <sup>b</sup>	2 87 92	uchtig 9h	Tages- mittel	Richtung	z u. Stārke d [Skala: o - 10	les Winde
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Tag	Dun 19h	2h 5-2 4.6	9h	Tages- mittel	19 <sup>b</sup> 87 92 94	2 87 92	uchtig 9h	Tages- mittel	Richtung	z u, Stärke d [Skala: o = 10 ] NE I NW I NB I	NNE 1 E 2 S E 2 S E 3
Tag	Dun 19 <sup>h</sup> 4-3 4-4 4-2 4-5 4-8 3-9	2h 2h 5.2 4.6 4.5 4.6 4.2 3.9	9h 5.0 4.3 4.1 4.3 4.1 4.8	Tages-mittel **  4.8 4.4 4.3 4.5 4.4 4.2	87 92 94 85 91	87 92 98 76 73 72	9h 91 92 84 77 77 83	Tages- mittel  88 92 92 79 80	Richtung  19 <sup>b</sup> N 1  N 1  E 2  E 1  SW 1	yu, Stārke d [Skafa: o - 10 2h NE 1 NB 1 NB 1 SE 1 o	NNE 1 E 2 E 3 SE 2 SW 3
Tag	Dun 19 <sup>h</sup> 4-3 4-4 4-2 4-5 4-8 3-9	2h 2h 5.2 4.6 4.5 4.6 4.2 3.9	9h 5.0 4.3 4.1 4.3 4.1 4.8 5.8	Tages-mittel  ****  ****  ****  ***  ***  ***  *	87 92 94 85 91 77	87 92 98 76 73 72 81	9h 91 92 84 77 77 83 80	Tages- mittel  88 92 92 79 80 77 86	N 1 N 1 E 2 E 1 SW 1 S 1	Su. Starke d [Skala: 0 - 10] NE I NW I NE I NE I NW I NE I NW I NE I NW I NE I NW I	NNE 1 E 3 SE 3 SW 2 SW 2
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Tag	Dun 19 <sup>h</sup> 4-3 4-4 4-5 4-8 3-9 4-7 6-6	2h 2h 5.2 4.6 4.5 4.6 4.2 3.9	9h 5.0 4.3 4.1 4.3 4.1 4.8 5.8	Tages-mittel  ****  ****  ****  ***  ***  ***  *	87 92 94 85 91 77 89 86 84 88	87 92 98 76 73 72 81	9h 91 92 84 77 77 83 80	Reit Tages-mittel  88 92 92 79 80 77 86 85 90 80	Richtung	y u, Stärke d [Skala: 0 — 10 NE 1 NW 1 NE 1 SE 1 0 WSW 2 SW 2 SW 2 NNE 1 NNW 1	Ics Wind  9h  NNE 1 E 2 E 3 SE 2 S 1 SW 2 SW 2 SW 2 NN 2
Tag	Dun  19h  4-3  4-4  4-5  4-8  3-9  4-7  4-7	2h 5.2 4.6 4.5 4.5 4.2 3.9 5.1 7.6 7.1	9h 5.0 4.3 4.1 4.8 5.8 7.4 6.7 4.1	Tages- mittel 100 4.8 4.8 4.4 4.3 4.5 4.4 4.2 5.2 7.2 7.1 4.8	87 92 94 85 91 77 89 86 84 88 83	87 92 98 70 73 73 81 82 94 69 72	9h 91 92 84 77 77 83 89 87 93 82 80	Reit Tages-mittel  88 92 92 97 80 77 86 85 90 80 78	Richtung   19h	Z u, Stárke č [Skala: o - 10]  NE I NW I NE I NE I NW I NE I NW I NE I NW I NW 2 NW 2 NW 2 NW 2 NW 1 NW I	90   NNE 1   E 2   SE 3   SW 2   SW 2   NNW 1   NNW 1
Tag	Dua 19 <sup>h</sup> 4.3 4.4 4.2 4.5 4.8 3.9 4.7 6.6 5.0 4.7 3.8	2h 5-2 4.6 4.5 4.6 4.2 3.9 5.1 4.6 4.4 4.4 4.6 4.3 4.6 4.3 4.6 4.4 3.9 5.1 4.0 5.1 4.0	9h 5.0 4.3 4.1 4.5 4.8 5.8 7.4 8 4.1 4.1	Tages- mittel see 4.8 4.8 4.4 4.3 4.5 4.4 4.2 5.2 7.1 7.1 4.8 4.4	87 92 94 85 91 77 89 86 84 88 83 94	87 92 98 76 73 72 81 82 94 69 72 75	9h 91 92 84 77 77 83 89 87 93 82 80	Reit Tages-mittel  88 92 92 97 80 77 86 85 90 80 78	Richtung  19 <sup>b</sup> N 1 N 1 E 2 SW 1 SW 1 SW 3 SW 4 N 1 NNW 1	Z u, Stårke d [Skala: 0 - 10] 26 NE 1 NW 1 NB 1 SE 1 0 WSW 2 SW 2 SW 2 NYE 1 NYW 1 NYW 1	9   NNE   1   E   2   3   SE   2   SW   2   SW   2   SW   2   NNW   1   SSW   1   SS
Tag	Dun  19h  4-3  4-4  4-5  4-8  3-9  4-7  4-7	2h 5-2 4.6 4.5 4.6 4.2 3.9 5.1 7.1 4.6 4.4 3.9 4.2 5.3	9h 9h 5.0 4.3 4.1 4.3 5.8 7.4 6.7 4.8 4.1 4.1 4.1	Tages- mittel 4.8 4.4 4.3 4.5 4.4 4.2 5.2 7.1 4.8 4.4 4.3 4.5 4.4 4.2 5.2 7.1 4.8	87 92 94 85 91 77 89 86 84 88 83 94 88	87 92 98 70 73 73 81 82 94 69 72	9h 91 92 84 77 77 83 89 87 93 82 80	Reit Tages-mittel  88 92 79 80 77 86 85 90 78 85 78	Richtung	Z u, Stårke d [Skala: 0 - 10] 26 NE 1 NW 1 NB 1 SE 1 0 WSW 2 SW 2 SW 2 NNE 1 NW 1 NW 1 NW 1 NW 1	SW 2 SW
Tag  1 2 3 4 5 6 7 8 9 10 11 12 13 14 15	Dun  10h  4.3  4.4  4.2  4.5  4.8  3.9  4.7  6.6  7.6  5.0  4.7  3.8  4.1	2h 5-2 4.6 4.5 4.6 4.2 3.9 5.1 4.6 4.4 4.4 4.6 4.3 4.6 4.3 4.6 4.4 3.9 5.1 4.0 5.1 4.0	9h 5.0 4.3 4.1 4.5 4.8 5.8 7.4 8 4.1 4.1	Tages- mittel see 4.8 4.8 4.4 4.3 4.5 4.4 4.2 5.2 7.1 7.1 4.8 4.4	87 92 94 85 91 77 89 86 84 88 83 94	87 92 98 70 73 73 81 82 94 69 72 75 71	9h 91 92 84 77 77 83 89 87 93 82 80	Reit Tages-mittel  88 92 92 97 80 77 86 85 90 80 78	Richtung  19b  N 1  N 1  E 2  E 1  SW 1  SW 3  SW 4  NW 1  SW 1  WW 1  WSW 1  W 3	Z u, Starke d [Skala: 0 - 10 24 NE 1 NW 1 NE 1 SE 1 0 WSW 2 SW 3	9h   NNE 1   E 2   S 1   SW 2   SW 2   SW 2   NNW 1   SSW 1   SW 1   SW 2   WSW 2
Tag  1 2 3 4 5 5 6 7 8 9 10 11 12 13 14 15 16	Dun  10h  4.3 4.4 4.2 4.5 4.8 3.9 4.7 6.6 7.6 4.7 3.8 4.1 4.6 5.4 4.9	2h 5.2 4.6 4.5 4.6 4.2 3.9 5.1 4.6 4.4 3.9 5.1 4.6 4.4 3.9 4.9	9h 5.0 4.3 4.1 4.8 5.8 7.4 4.1 4.1 4.1 5.4 5.5 5.0	Tages-mittel  **********************************	87 92 94 85 91 77 89 86 84 88 83 94 84 75 84	Relative Fe	9h 91 92 84 77 77 83 80 87 93 82 80 87 77 87	Reit Tages-mittel  88 92 92 79 80 77 86 85 90 78 85 90 78 87 79 79	Richtun;  19 <sup>5</sup> N 1 N 2 E 3 E 1 SW 1 SW 3 SW 3 SW 4 N 1 WW 1 WW 1 WW 1 WW 3 W 3 W 3	NE   NE   NE   NE   NE   NE   NE   NE	9h   NNE 1   E 2   E 3   SE 2   SW 3   SW 2   SW 2   SW 2   SW 3   SW 2   SW 4   SSW 4   SSW 4   W 4   W 5
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Tag  1 2 3 4 5 5 6 7 8 9 9 10 11 12 12 13 14 15 16 17 18	Dun  19h  4.3 4.4 4.2 4.5 4.8 3.9 4.7 6.6 7.6 5.0 4.7 3.8 4.1 4.1 4.1 4.3 4.3 4.3 4.3 4.3 4.3 4.3 4.3 4.3 4.3	2h 5.2 4.6 4.5 4.6 4.6 7.1 4.6 4.2 5.3 5.9 5.3 5.9 3.2 3.5 3.5	9h 5.0 4.3 4.1 4.3 4.1 4.1 4.1 5.4 5.0 4.2 2.6	Tages-mittel 4.8 4.4 4.3 4.5 4.4 4.2 7.2 7.1 4.8 4.4 8 4.4 5.4 6.2 7.1 6.8 6.6 6.6 6.6 6.6 6.6 6.6 6.6 6.6 6.6	87 92 94 85 91 77 89 86 84 88 83 94 84 75 64 75	Relative Fe  2h  87  92  98  73  72  81  82  94  69  72  73  81  77  73  68	9h 91 92 84 77 77 83 89 87 82 80 87 72 81 75 75 76 87 88	Reit Tages-mittel  SS 92 79 80 77 86 85 90 85 78 85 76 79 75 74 86 85 80	Richtung	y u, Starke of Skala: o - 10 (Skala:	9   9   1   1   1   1   1   1   1   1
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Tag  1 2 3 4 5 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25	Dun  19h  4.4 4.2 4.5 4.8 3.9 4.7 6.7 6 7.6 5.0 4.7 3.8 4.4 4.9 3.4 3.3 3.2 5.6 6.7 6.7 6.7 6.7 6.7 6.7 6.7 6.7 6.7 6	2h 5.2 4.6 4.5 4.2 3.9 7.6 7.6 7.6 4.6 4.4 3.9 4.6 4.6 4.9 3.9 3.5 5.3 5.9 3.7 4.6 5.3 5.9	9h 5.0 4.3 4.1 4.3 4.1 4.8 5.4 5.4 5.2 5.0 4.2 2.6 5.6 5.4	Tages-mittel  4.8 4.3 4.5 4.4 4.2 7.2 7.1 4.8 4.4 4.9 3.9 4.6 3.0 3.1 3.1 3.1 3.1 3.1 3.1 3.1 3.1	87 92 94 85 91 77 89 86 84 88 83 94 84 75 64 89 98 87 75 85 85 87 85 85 87	Relative Fe  21  87 02 05 70 73 72 81 82 94 69 75 77 77 78 77 78	9h 91 92 84 77 77 83 89 80 87 72 87 87 88 88 87 78 88 88 88	Tages-mittel  SS 02 92 79 80 77 86 85 90 80 77 86 85 90 80 80 85 86 86 86 86 86	Richtung   19\(^{\text{N}} \)	Substance of Skala: 0 - 1 - 2 - 2 - 2 - 2 - 2 - 2 - 2 - 2 - 2	9   9   1   1   1   1   1   1   1   1
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Tag  1 2 3 4 4 5 5 6 7 7 8 9 10 11 12 13 14 15 16 17 17 18 10 10 10 10 10 10 10 10 10 10 10 10 10	Dua 10h 4.3 4.4 4.2 4.5 4.8 3.9 4.7 6.6 7.6 5.4 8 4.1 4.2 4.2 4.2 4.2 4.2 4.3 4.6 4.7 6.6 5.4 4.7 6.6 5.4 6.7 6.6 5.4 6.7 6.6 5.4 6.7 6.7 6.7 6.7 6.7 6.7 6.7 6.7 6.7 6.7	2h 5.2 4.6 4.5 4.6 4.2 3.9 7.6 7.6 7.6 4.4 3.0 4.2 5.3 5.9 4.9 3.5 5.9 4.9 3.5 5.9 4.9 3.5 5.9 4.9 3.5 5.9 4.9 3.5 5.9 4.9 3.5 5.9 4.9 4.9 3.6 3.7 4.5 5.4 5.5 3.9 4.9	5.0 Millin Millin 5.4 4.3 4.1 4.1 5.4 5.6 5.6 5.6 5.6 5.6 5.6 5.6 5.6 5.6 6.7 4.8 4.0 4.0 4.0 4.0 4.0 4.0 4.0 4.0 4.0 4.0	Tages-mittel	19 <sup>4</sup> 87 92 94 85 91 77 78 86 86 84 88 83 94 84 84 85 87 75 86 87 87 86 87 89 92	Relative Fe  24  857  92  98  70  73  84  97  77  77  81  77  77  81  81  77  77  81  81	9h 91 92 84 77 83 89 87 72 85 87 78 87 78 88 87 78 88 87 78 88 87 88 88	Reit Tages-mittel  88 92 92 79 80 77 86 85 90 80 78 85 85 86 87 89 80 80 80 80 80 80 80 80 80 80 80 80 80	Richtun;  195  N 1 N 2 E 2 E 3 S 1 S 1 S 1 S 1 S 1 S 1 S 1 S 3 S 3 S 4 S 3 S 4 S 5 S 1 S 5 S 1 S 5 S 1 S 5 S 1 S 5 S 1 S 5 S 5 S 5 S 5 S 5 S 5 S 5 S 5 S 5 S 5	SU, Starke & (Skala: 0 - 10 (Skala: 0 - 10 )  ME   ME   ME   ME   ME   ME   ME   ME	
Tag  1 2 3 4 5 6 7 8 8 9 9 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 27 27 28 29 30 0	Dun  10 <sup>h</sup> 4.3 4.4 4.5 4.8 3.9 6.6 5.0 4.7 3.8 4.6 4.7 3.8 3.4 3.3 3.6 4.2 5.2 3.6 4.2 5.6 4.2 5.6 4.2 5.6 4.2 5.6 4.2 5.6 4.2 5.6 4.2 5.6 6.6 4.3	2h  5.2 4.6 4.6 4.0 4.0 7.6 7.6 7.1 4.6 4.4 3.0 4.2 5.3 5.9 4.5 5.5 5.4 5.5 5.4 5.5 5.5 4.5 3.9 4.5 3.9 4.5	5.0 Millin Millin 5.4 4.3 4.1 4.1 5.4 5.6 5.6 5.6 5.6 5.6 5.6 5.6 5.6 5.6 6.7 4.8 4.0 4.0 4.0 4.0 4.0 4.0 4.0 4.0 4.0 4.0	Tagesmittel	87 92 94 85 91 77 89 86 84 88 83 34 94 84 84 85 87 75 86 87 79 88 87 75 85 85 87 79 92 85 85 86 87	Relative Fe  24  87  92  98  79  79  79  79  79  70  70  71  71  71  71  72  83  84  99  79  79  85  86  99  79  79  87  87  87  88  89  99  79  7	9h 91 92 93 87 77 83 89 89 87 81 85 86 87 96 87 98 87 98 91 91 92 91	Reit  Tages- mittel  88 92 92 98 80 77 86 80 80 87 79 75 85 80 86 87 87 87 87 88 88 88 88 88 88 88 88 88	Richtung  19th  N 1 E 2 E 3 K 1 SW 1 SW 3 SW 3 SW 3 SW 3 SW 1	Starke   S	98   NNE   1
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17	III IIS FS	7 N	#	4 N	FS FS	3		3.3		Mora	ene dune	tin	nittaes dus	stir aben	de me
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25 26 27	FHS S	o SW	us	10	HS S	10	10	0.0	0,6	Morg Morg	s.=_,, ens =_,	22h K, 22 mittags	dunstig.	abends =	itt.dunst.
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ı	52.2	52.3	52.0	52.1	52.5	53.3	53-4	53.2	53.5	53.9	54.3	54.7	53.14	55.2	52.0
3	55.2	57.6	55-7 57-3	56.3	57.1	57.7	57.6	57.0	50.0	57-4	55.3	57.9	56.50	57.9 57.9	55.2 54.6
4	54.6	53-4	52.0	52.3	52.0	52.1	52.6	50.5	50.2	49.9	49.9	49.7	51.68	54.6	49.7
5	50.1	49.7	49.1	48.6	48.9	49.2	49.5	48.5	48.7	45.7	45.3	48.1	48.95	50.1	47.6
6	47.6	47.1	47.0	46.5 50.6	46.7 51.3	47.2 51.8	47.2 51.5	47.0 51.0	46.9 50.7	47.0 50.5	47.6	48.6 50.9	47.20	49.2	46.5
7	51.0	51.3	51.4	51.8	52.2	52.4	52.8	51.4	51.3	51.1	51.0	50.9	51.55	52.8	50.7
9	50.7	50.5	49.9	49.2 53.0	48.7	49.0	49.5	49.2	48.9	49.1	48.9	49.4 60.5	49.42	50.7	48.9
11	61.2	61.6	62.1	62.4	61.1	64.1	64.2	64.1	64.1	64.4	64.7	64.9	63.41	64.9	61.3
12	64.9	64.9	64.8	64.3	64.2	61.0	63.7	62.9	62.8	62.2	61.7	61.3	63.48	64.9	60,8
13	60.8	60.4	59.7	58.9	57-9	57-4	55.0	54.1	53.2	51.9	52.2	51.9	56.12	60.8	51.3
14	51.3	50.4	49.9	50.0	50.1	50.4	51.1	50.8	51.4	51.8	52.7	52.9	51.07	52.9	50.5
16	50.8	40.3	50.2	49.6	49.3	49.3	48.4	47.9	47.2	47.3	47.2	46.7	48.68	50.8	46.5
17	46.5	47.4	48.6	49.2	50.4	31-7	52.2	52.5	52,6	53.1	53.7	54.0	50.49	54.5	46.5
18	54-5	\$6.4	54.7	55.1	55.6	56.2	56.4	55.9	55.9	55.0	56.1	55.5	55.60	56.5 56.5	54.5
20	53.5	53.6	53.7	55.5	55.3	55.6	54.9	53.7	\$3.5	54.1	54.2	54.3	53.50	54.3	53.2
21	54.2	54.5	54.4	54.4	54.4	55.0	55.0	54.4	54.4	54-3	54.3	54.2	54.46	55.0	54.0
22	54.0	53.9	53.8	\$3.7	53.6	53.9	53.6	53.1	53.1	53.1	53.1	53.0	53.49	54.0	52.9
23	52.9	52.8	52.6	54.1	53.1	54.3	55.1	55.6	55.1	54.6	54.1	\$3.0 \$6.8	53.89	55.6	52.5
25	56.7	56.3	55.9	55.1	54.9	55.0	54.4	53.4	52.6	52.2	31.9	51.3	54.14	56.7	50.7
26	50.7	50.0	49.7	49.3	49.5	49.6	49.6	49.1	49.4	49.4	49.3	48.9	49-54	50.3	48.3
27 28	48.3	48.2	47.7	46.9	47.0	46.7	44.8	44.3	43.6	43.4	13.0	42.8	45.56	48.3	42.7 38.5
29	35.8	37.8	37 - 1	16. €	35.7	35.3	34.7	33-5	33.0	32.2	31.2	30.6	34.70	38.8	30.2
30	30.2	30.2	25.9	28.7 52.7	29.1 54.1	30.9	33.7 55.6	36.8	39.3 56.4	41.2 57.0	43.3	45.7 57.4	34.83	47.2 57.5	28.7
Mittel	51.64	51.56	51.50	-	51.60	52.05	51.99			51.66	51.74	51.80	51.68	53.97	49.42

DEZEMBER

ag						L	uittem	peratu	r nach	Celsius					
	124	143	164	184	20h	221	Op	2 <sup>h</sup>	44	64	84	10,	Tages- mittei	Max.	Min.
1 2	1.1	1.0	1.0	1.0		2.1	3.0	3.8	4.1	3.9	3.6	3.2 0.0	2.33	4.1 1.3	- 0,
3	- 0.1	- 0.2	- 0.1	- 0.3	- 0.1	0.0	0.1	- 0.1	0.6	0.8	0.9	1.2	0.22	1.2	— 0,
5	2.4	2.3	1.6	2.0	3.4	2.5	3.5	3.1	2.8	3.6	3.2	2.2	2.65	4,6 3.1	- 1:
6	2.1	1.9	1,6	1.2		1.8	2.1	2.3	2.9	3-3	3.3	3.0	2.22	3.3	1.
8	5.7	6.7	7.0	7.3	7.8	8.5	9.6	10.1	9.9	9.2	9.1	5.3	3.45 8.37	5.7	5
9	9.4	9.5	9.6	9.7		3.8	8.2	7·1 5·4	6.8	6.6	3.6	6.0	8.28	10.4	5
	2.7	3.3	3.4	3.0	3.1	3.4	3.7	3.9	3.2	2.5	1.7	1.1	2.92	3.9	- °
3	0.3	- 0.2	- 0.9	- 1.5		- 0.6	3.0	3.4	3.0	2.4	2.4	0,6 3.1	2.12	3.6	- i
4	3-5	3-7	3.8	4.0	4.2	4.8	4.5	5.0	5.1	5.3	1 5.3	5.2	4.53	5.3	3
5	5.6	5.0	5.3	5.1	4.9	5.6	6.9	7.2	6.1	5.1	6.0	5.9	5.62	5.7	4
1	5.0	3.3	1.9	2.3	1.4	1.5	5.3	2.1	1.2	0.1	- 0.4	- 1.0	1.63	5.0	1
5	- 1.2	- 1.4 - 5.3	- 2.0 - 5.6	- 2.7 - 5.8	- 2.6 - 5.7	- 5.1	- 0.9	- 0.3 - 1.3	- 1.1	- 1.9	- 2.9 - 2.9	- 3.8 - 3.6	- 1.87 - 3.82	- 0.3	- 4 - 5
1	- 4.4	- 5.0	- 4.0	- 3.1	- 2.4	- 1.5	0.0	1.6	1.9	2.0	2.4	2.3	- o.85	2,6	- 5
	3.4	3.5	3.6	3.5	4.2	4.6	3.3	5.1	5.8	3.4 5.2	3.5	3.1	2,98 4.51	3.6 5.8	3
	4.5	4.9	3.9	3.5	5.4	5-5	5.8	5.8	5.7	5.1	2.7	4.6	3.24	5.8	4
1	2.5	2.5	2.4	2.3	2.1	1.9	1.8	1.9	1.8	0.8	1.2	0.5	1.51	2.5	- 0
	- 0.2	0.2	0.1	0.1	0.8	1.7	2.1	2.6	2.9	3.1	2.8	2.6	1.57	3.1	- 0
ı	0.5	0.3	0.5	0.3	0.2	0.3	9.6	1.2	3.6	0.7	0.3	0.2	0.52	1.2	0
1	2.7	3.3	- 0.1 4.3	4.7	5.1	4.9	2.3	0.5	- 0.3	- 1.7	- 2.4	- 4.2	1.67	2.7 5.1	- 0 - 4
ı	- 4.6	- 4.2	- 4.2	- 4-4	- 4.0	- 4.2	- 3.5	- 3.1	- 4.0	- 5.2	- 6.1	- 6.3	- 4.48	- 3.0	- 6
ı.	2.02	1.94													
۰		1.94	1.85	1.7	8 1.89	2.25	2.73	3.09	2.95	2.5	3 2.23	1.97	2.27	3.81	0.
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g	124		Ric	-	(R), Ges	chwind	igkcit		Wind	es in 1	Sekunde	in Meter		3.81	Tag
g		1 14	Ric	htung	1	1	igkeit	(G) des	Winde	-	-		n	104	Tag
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-	R 6	6 N 6 ENE	Ric.	htung	(R), Ges 18 <sup>b</sup> R G No.8 NNE 0.9	chwind 20h R G	igkeit	(G) des	Winds	es in 1	Sekunde  R G  NE 1.8 WSW 0.4	in Meter	R 6	R G	Tag
100	R 6	6 N 6 ENE 2 ESE	Ric 6 A	N 1.1 NE 0.6 NE 1.2 SE 2.5	(R), Ges 18 <sup>b</sup> R G N 0.8 NNE 0.9 ESE 1.2 SE 2.6	chwind 205 R G X 1.1 NE 1.6 ESE 1.6 ESE 2.1	R NNE NNE NE CESE :	(G) des	Winds	es in 1  24  KE 1.7  (W 0.5  NE 3.0  SE 2.0	Sekunde R G NE 1.8 WSW 0.4 E 3.0 S 1.6	in Meter  6 R G  NNE 1. SW 0. ESE 2. SSE 1.	8	1 NNW 0. 5 ENE 1. 6 ESE 3.	Tag
-	N O NAW O NAE 1 ESE 3 SSW 1	6 N 6 ENE 2 NNE 2 ESE 1 SSE	Ric 6 6	N 1.1 NE 0.6 NE 1.2 SE 2.5 SE 1.2	18 <sup>b</sup> R G  N 0.8 NNE 0.9 ESE 1.2 SE 2.6 S 1.0	203 R G NE 1.0 ESE 1.0 ESE 2.1 SSW 1.1	R NNE NE ESE ESE SW	(G) des	Winds G 1 1.4 E 0.0 NN 3.4 E 2.8 E 1.2 SS	es in 1  24  K G  NE 1.7 (W 0.5 NE 3.0 SE 2.0 SW 1.4	Sekunde R G NE 1.8 WSW 0.4 E 3.0 S 1.5 SSW 0.6	in Meter  6 R G  NNE 1. SW 0. ESE 2. SSE 1. SSW 0.	8	1 NNW 0 5 ENE 1. 6 ESE 3 4 SE 2	Tag
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the same of the same of	N 0 NNW 0 NNW 0 NNW 0 NNW 1 ESE 3 SSW 1 SSW 1 SSW 1 SSW 1 WSW 1 WS	6 N 6 ENE 2 NNE 2 ESE 1 SSE 3 WSW 9 WSW	Ric 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6	htung   16h   17   16h   17   17   17   17   17   17   17   1	(R), Ges 18 <sup>b</sup> R G N 0.8 NNE 0.9 ESE 1.2 SE 2.6 S 1.0 SW 2.1 NSW 1.5 SW 3.6 SW 2.5	20 <sup>3</sup> R G  N 1.1 NE 1.6 ESE 1.6 ESE 2.6 SSW 1.1 SW 1.2 SW 3.5 WSW 4.3	Igkeit  22h R NE ( NE ( ESE : ESE : SW ( WSW ( W	(G) des	Winds  G 1  1.4 E  0.9 NN  3.4 E  2.8 E  1.2 SS  3.2 WS  2.2 WS  3.9 S	es in 1  24  G  NE 1.7  (W 0.5)  SE 2.0  SW 1.4  SW 2.5  SW 2.5  NE 2.2	Sekunde  # G  NE 1.8 WSW 0.4 E 3.0 S 1.5 SSW 0.6 SSW 1.9 SSW 1.6 SW 3.0 N 1.0	in Meter  6 R G  NNE 1. SW 0. ESE 2. SSE 1. SSW 0. SSW 2. SSW 1. WSW 2. N 0.	8 R 6 NNE 1. 8 ESE 1. 6 ESE 3. 4 SE 1. 6 SW 2. 8 SW 1. 5 SW 2. 4 No. 4 No. 4 No. 4 No. 6 No. 5 N	104 R 6	Ta;
	12 <sup>h</sup> R 6 NNW 0 NNE 1 ESE 3 SSW 1 SSW 1 SW 4 SSW 1 NNE 2	6 N 6 ENE 2 NNE 2 ESE 1 SSE 2 SS 1 SSW 9 WSW 9 SW 3 N	Ric.  6 A  0.9  0.8  1.3 E  1.9 S  0.6 S  1.6 SS  3.0 WS  2.4 WS	N 1.1 NE 0.6 NE 2.5 SE 1.2 NW 1.1 NW 1.5 NW 1.3 NW 1.3 NW 1.3	18 <sup>b</sup> R G  N 0.8 NNE 0.9 ESE 1.2 SE 2.6 S 2.6 S W 2.1 NSW 1.5 SW 3.6 SW 2.5 N 1.3	20 <sup>5</sup> R G  N 1.1 NE 1.6 ESE 1.6 ESE 2.1 SW 1.1 SW 3.5 WSW 4.1 NW 1.6	Igkeit  22h R NE ( NE ( ESE : ESE : SW ( WSW ( WSW ( NSW ( N	(G) des	Winds  G I  1.4 E  0.9 NN  3.4 E  2.8 E  1.2 SS  3.2 WS  2.2 WS  3.7 NN  2.5 NN	es in 1  24  G  NE 1.7  (W 0.5)  SE 2.0  SW 1.4  SW 2.5  SW 2.5  SW 2.5  (W 2.0)	Sekunde  # G  NE 1.8 WSW 0.4 E 3.0 S 1.5 SSW 0.6 SSW 1.9 SSW 1.6 SW 3.0 N 1.6	in Meter  6' R G  NNE 1. SW 0. ESE 2. SSE 1. SSW 2. SSW 1. WSW 2. N 0. WNW 2.	8	7 R 6 4 NNW 0 5 ENE 1 6 ESE 3 4 SE 2 1 SSW 1 5 SSW 1 5 SSW 4 5 SSW 1 1 SW 2 3 NNE 2 1 NW 1	Tag mit 6 6 1 5 0 7 7 8 7 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8
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	12h   R   6   N   0   N   N   0   N   0   N   1   ESE   3   SSW   1   SSW   1   SSW   1   N   E   2   N   0   N   N   0   N   N   0   N   N	6 N 6 ENE 2 NNE 2 ESE 1 SSE 1 SSW 9 WSW 9 SW 3 N 8 NE 8 WSW 3 WSW 8 WSW 8 WSW	Rici 6 A 6 A 6 A 6 A 6 A 6 A 6 A 6 A 6 A 6	N 1.1 NE 0.6 NE 2.5 SE 1.2 W 1.1 W 3.9 W 1.3 W 1.3 W 1.4 W 0.3 W 1.4 W 0.3 W 1.4 W 0.3 W 1.4 W 0.3 W 1.4 W 0.3 W 1.5 W 0.3 W 0	(R), Ges R G N 0.8 NNE 0.9 ESE 1.2 SE 2.6 S 2.6 S W 2.1 NSW 1.5 S W 3.6 S W 2.5 N 1.3 NNW 3.1 S 0.6 S 2.6 S 3.6 S 2.6 S 3.6 S 2.6 S 3.6 S 2.6 S 3.6 S 3.6	Chwind  20h R G  N 1.1 NE 1.0 ESE 1.0 ESE 2.1 SW 1.7 SW 1.7 SW 3.9 WSW 4.1 NW 1.0 SSW 1.0 SSW 1.0 2.5 WXW 4.1 W 2.1	NNE 1 NE 0 ESE 2 ESE 3 SW 1 NSW 1 NS	(G) des	Winds  G J  1.4 E  0.9 NN 3-4 E  2.8 E  1.2 SS  3.2 WS 2.2 WS  3.7 NS  2.5 NS  1.5 WS  4.9 WN  3-3	24 G  NE 1.7 (W 0.5) NE 3.0 SW 1.4 SW 3.6 (W 2.5 (W 2.6) (W 1.4 NE 2.2 (W 1.4	Sekunde  A G  NE 1.8  WSW 0.4  E 3.0  S 1.5  SSW 0.6  SSW 1.6  SW 1.6  X 0.8  X 0.8  X 1.6  X 0.8  X 1.6  X 0.8  W 3.1  X 0.8  W 3.1	in Meter  6 R G  NNE 1. SW 0. ESE 2. SSE 1. SSW 0. SSW 2. SSW 1. WSW 2. N 0. WNW 2. NNE 1. SSW 0.	8	1 10 <sup>k</sup> R 6 6 1 NNW 0 5 ENE 1 6 ESE 3 4 SE 2 2 1 SSW 1 1 SW 2 1 NW 1 1	Tag mit  6 1. 5 0. 5 2 2. 1 2 3 1 6. 2 2 3 3 6. 1 1 1 1 8 1 1 1 8 1 1 3 2 3 4 1 5 3 3
	R 6  N 0  NNW 0  NNW 0  NNE 1  ESE 3  SSW 1  SSW 1  SW 4  SSW 1  SWW 1  NNW 2  NNW 1  NNW 2  NNW 2  NNW 2  NNW 4  NNW 4	R 6 NE 6 ENE 2 ESE 1 SSW 9 SW 3 N 8 NE 0 WSW 8 WSW 8 WSW 8 WSW 9 SW	Riccons	htung   164   16   16   16   16   16   16   1	(R), Ges 18 <sup>b</sup> R G No.8 NNE 0.9 ESE 1.2 SE 2.6 S 1.0 SW 2.1 NSW 1.5; SW 3.6 SW 2.1 NSW 1.5; SW 3.6 SW 2.5 SW 3.6 SW 2.5 SW 3.6 SW 2.5 SW 3.6 SW 3.	chwind  208 R 67 N 1.1 NE 1.0 ESE 1.0	Igkcit  R  NNE NE NE SE SE SW  WSW  NNW  WSW  WNW  WN	(G) des	Winds  G J  1.4 E  0.9 NA  3.4 E  1.2 SS  3.2 WS  2.2 WS  3.9 S  1.7 NS  2.5 NA  1.5 WS  4.0 WN  3.3 S	26 G NE 1.7 (W 0.5) NE 1.7 (W 0.5) NE 3.0 (W 1.4 (W 2.5) (W 2.5) (W 2.6 (W 1.8 (W 1.8 (W 2.5)	Sekunde  # 6  NE 1.8  WSW 0.4  E 3.0  S 1.5  SSW 1.0  S W 1.0  N 1.6  N 0.8  SW 1.0  W 1.5  W 3.1	in Meter  R G  NNE 1. SW 0. ESE 2. SSE 1. SSW 2. SSW 2. SSW 2. N 0. WSW 2. NNE 1. SSW 0. WNW 2. WNW 2. WNW 2. WNW 3.	R 66 NNE 1: 8 ESE 1: 6 ESE 3: 4 SE 1: 6 SW 2: 8 SW 1: 0 SW 2: 4 N 0: 0 NNW 1: 1 NNW 1: 8 SSW 1: 0 W 2: 4 WNW 4:	1 10 <sup>h</sup> R 6 1 NNW 0 5 ENE 1 6 ESE 3 4 SE 2 7 SSW 1 5 SSW 1 5 SSW 1 5 SSW 1 5 SSW 1 5 SSW 1 7 SSW 2 3 NN 2 3 NN 2 3 NN 2 4 SE 2 8 SSW 3 8 SS	Tag mit  6 1.65 0.55 2.21 0.02 0.03 0.02 0.03 0.04 1.11 1.81 1.83 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.85
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777773333333333333333333333333333333333	12 <sup>k</sup>   R   6   NAW   0   NAW   0   NAW   1   ESE   3   SSW   1   SSW   4   SSW   1   SSW   4   NAW   2   NAW   2   NAW   6   NAW   1   NAW   7   NAW   1   0   0   0   0   0   0   0   0   0	R   R   R   R   R   R   R   R   R   R	Ric	N 1.1 NE 0.6 NE 2.5 SE 2.5 NW 1.1 NW 1.3 N 1.4 NW 0.3 NW 1.4 NW 0.3 NW 1.4 NW 0.3 NW 1.4 NW 0.5 NW 2.2 NW 4.0 NW 2.2 NW 4.0 NW 3.0 NW 3	(R), Gen 18b R G NO.8 NNE 0.9 ESE 1.2 SE 2.6 S 1.0 S 1.0 S 1.0 S 1.0 S 1.0 S 2.6 NNW 1.5 S W 2.5 NNW 3.6 S 2.1 NNW 5.1 S 2.6 W 3.0 NNW 5.1 S W 2.5 NNW 5.1 S W 2.5 NNW 5.1 S W 3.0 S W 3	20 <sup>3</sup> R G  NE 1:c ESE 1:c ESE 2: SW 1:2 SW 1:2 SW 1:S SW 1:C SW 1	NNE 1	(G) des G R 1.9 NE 1.4 ESE 1.4 ESE 1.4 ESE 1.4 ESE 1.4 ESE 1.5 WSW 1.5 WSW	Winds  G J  1.4 E: 0.9 NX 3.4 E: 2.8 E: 1.2 SS 2.2 WS 3.2 WS 3.2 WS 3.2 SX 1.7 NI 2.5 NA 2.5	CE IN I  24  G  NE 1.7  (W 0.5)  NE 3.50  NE 3.50  NE 2.0  (W 3.6  (W 2.5)  (W 3.6  (W 2.5)  (W 1.8  (W 2.7  (W 1.8  (W 1.8  (W 3.8  (	Sekunde  # G  NE 1.5  WSW 0.4  E 3.0  SSW 1.6  SW 1.9  SSW 1.6  SW 3.0  N 1.6  SW 1.9  SW 1.9  SW 1.9  SW 1.9  SW 1.9  SW 1.9  1.1  2.0  SW 3.3  1.1  2.0  SW 3.3  3.1  SW 3.3  1.1  2.0  SW 3.3  3.1  SW 3.3  1.1  3.5  SW 3.3  3.1  SW 3.3  3.1  SW 3.3  3.1  SW 3.3  3.1  SW 3.3  3.3  SW 3.3  3.3  SW 3.3	in Meter  R G  NNE 1. SW 0. ESE 2. SSE 1. SSW 0. SSW 2. NO. WNW 2. NNE 1. SSW 0 2. WNW 1 1 1 1 1 1 1 2. WSW 1.	8	10°   R   6   1   10°   10°   10	Tag mit 6 6 1 0 5 5 2 2 3 3 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1
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<sup>&</sup>quot;) Der Windrichtungsnotograph fonktionlette am as, een ash on und vom 18, 26 bie as, o' nich



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K. U. K. HOFBUCHDRUCKEREI A. HAASE. — VERLAG DER K. K. STERNWARTE. 1906.